

PARKING

1. General

- A. A minimum physical clearance of 15 feet should be maintained between airplanes to give adequate turning clearances and protection from jet velocities and temperatures at taxi thrust and idle power.
- B. Based on the JT3C-4 installation for standard day condition, with 15 foot clearance between airplanee and at idle thrust, velocity at adjacent airplane would be approximately 18 to 20 mph and temperature would range between 75 to 85 degrees Fahrenheit.

2. Park Airplane

- A. Taxi or tow airplane into position designated for parking.
- B. Set parking brake by applying toe pressure on rudder pedals and then pull up on parking brake handle, located on throttle control stand.
- Place wheel chocks on forward and aft side of main gear wheels (two chocks per main gear).
- D. Disconnect and remove tow bar and tractor.
- E. Engage nose gear and both main gear ground down locks to prevent gear retraction.
 - NOTE: If airplane is towed to parking area, landing gear ground down looks shall be installed as soon as flight crew leaves airplane or before tow truck is attached. Recause of high gross weight of airplane, mooring provisions are not provided and should unusual—conditions warrant mooring, see 7-1-1, figure 202, for procedure.

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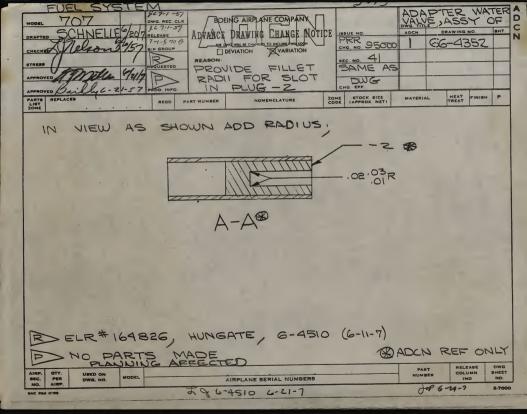
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RELEASE DWG AIRP QTY. PART USED ON MODEL COLUMN SHEET SEC. PER NUMBER DWG. NO. AIRPLANE SERIAL NUMBERS AIRP. NO. NO.

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POWER PER		-52		_		BLKH	1D FT	G-STA	62
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AIRPLANE SERIAL NUMBERS

AIRP. SEC. NO. BAC 924 C-R5

QTY.

PER

AIRP.

USED ON

DWG. NO.

MODEL

DWG SHEET NO. 2-700C

RELEASE

COLUMN

IND

PART

NUMBER

FUEL SYSTEM		4			6-70) =			
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ELR# 161071 MEGLING 6-4510 (6-8-7)

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FUEL SYSTEMS	4-	-69	E	LR#80562
MODEL 70 7 Willy DWG REC CLK 7 DRAFTED TIM TAYLOR RX 6/2+157 RELEASE	BOEING AIRPLANE COMPANY SEATTLE 14, WASHINGTON	ISSUE No.	PIT OVER	TING RBOARD DRAIN
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STRESS REQUESTED 6-4400	TO USE AVILLABLE	CHG. No. 95000	1	66-4312
APPROVED PROD INFO	MATERIAL,	APL		
APPROVED SHOP INFO		#1 \$#2		
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DUPONT WHITE NYLON

ALLOW MATERIAL CHG AS SHOWN

DO.P. ITEM.

-419 6/19

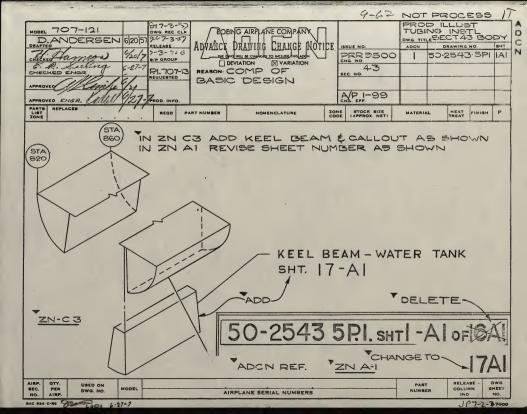
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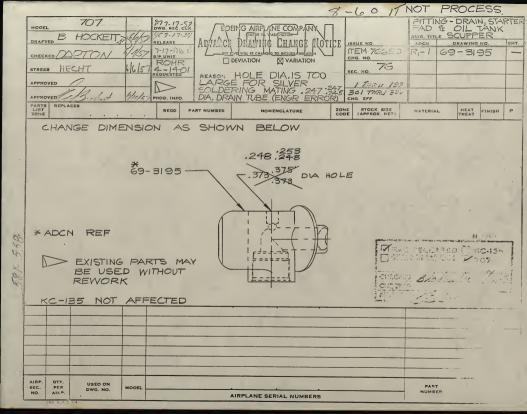
AIRP, OTY.
SEG. PER DWG, NO. AIRP.

AIRPLANE SERIAL NUMBERS

PART RELEASE DWG SHEET
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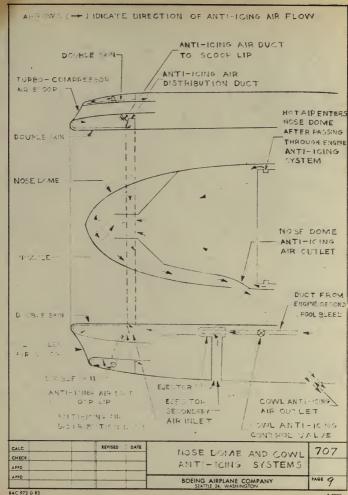
AIRPLANE SERIAL NUMBERS





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WING	2	.54 IT ELR 2390
ELR 2390 MODEL NO.	DWG. REC. CLK BOEING AIRPLANE COMPANY	SUPPORT ANGLE FUBL LINE WEL 315 DWG. TITLE
	RELEASE JIEM950	DOO ADCH DRAWING NO. SHT.
DRAFTED ()	B/F GROUP NO CHANGE REASON: TO ALLOW ENGIN FUEL BEC. NO. 1	2 30-3017
	TUBES (5-86584) TO ALIGN 1-1994	
APPROVED LABOUR 7.5-7	WITH ANGLE CHG. EFF.	
ORIGINATOR 2	PHONE PLAN	NING PHONE
REO WHITE	ENGINEERING LIAISON REQUEST	
DEPT. 6-2060 BOX NO. 8	Box No.	
PARTS REPLACES	Town Street	SIZE MATERIAL HEAT FINISH P
LIST	REQD. PART NUMBER NOMENCLATURE CODE (APPROX.	NUT) TREAT
*ADCN REF. ONLY	CHANGE ANGLE OF BEND 081*163 *	AH "ino!"
SEC PER DUG NO MODEL	AIRPLANE SERIAL NUMBERS	PART NUMBER
NO AIRP SHOULD ACCOUNT	ORD, REWORK EXISTING PARTS & INSTLY	3
STATUS OF TOOLS	DED) BEMORE EXPLINE TIME & WELL	STATUS OF COMPLETED
A/OR PLANNING		
Beatre 7-5-7		7-2-57 1



2-7000

- b. Jack point load limitations
 - Fuselage load limits
 - (a) forward body (b) aft body
 - (2) Landing gear
 - (a) main gear (b) nose gear
 - (3) Wing
 - (a) inboard wing
 - (b) outboard wing
- 5. Leveling and weighing
 - Leveling pad locations
 - (1) Center section
 - (2) Nose section
 - Leveling procedure b.
 - (1) Jacking
 - (2) Use of leveling equipment
 - (a) leveling provision scale
 - (b) use of engineers level
 - (3) Alignment
 - (a) location of points alignment procedure (b)
 - c. Weighing equipment and procedure
 - (1) Electronic weighing kit
 - (a) description
 - (b) operation
 - Weighing procedure (2)

Transport Service Training

- (1) Nose gear
 - (a) lock rod location
 - lock handle installation (b)
 - lock handle emergency release (c)
- (2) Main gear
 - (a) lock description and location
 - (b) lock installation
- b. Covers
 - (1) Pitot
 - (a) type
 - installation and removal (b)
 - (2) Engine
 - (a) intake
 - (b) tailpipe
 - (3) Vents and ducts
 - (a) types
 - (b) locations
 - (4) Surface covers
- 4. Jacking
 - Jack pad locations
 - (1) Station numbers
 - (a) fuselage jack points
 - landing gear jack points (b)
 - (2) Jack pad heights
 - (a) inboard wing
 - (b) forward body
 - (c) aft body
 - (d) outboard wing



- (a) temperatures
- (b) velocities
- (2) Danger areas
 - (a) inlet duct area
 - (b) exhaust area
- (3) Blast fences
 - (a) distances
 - (b) velocity and noise reduction
- (4) Engine noise levels
 - (a) decibel ratings
 - (b) suppressor effects

2. Towing

- a. Tow bar
 - (1) Description
 - (a) length
 - (b) load limits
 - (c) shear pin
- b. Attach points
 - (1) Main gear
 - (a) forward lugs
 - (b) aft lugs
 - (2) Nose gear
- c. Turning radii
 - (1) Nose gear
 - (a) steering angle
 - (b) swivel arrangement
- 3. Ground locks and covers
 - a. Locks

- d. Service area lighting
 - (1) Junction boxes
 - (2) Air conditioning compartments
 - (3) Tail cone
 - Wheel wells (4)
- Exterior lighting
 - (1) Landing lights
 - (a) inboard
 - (b) outboard
 - (2) Runway turn-off and taxi lights
 - (3) Position lights
 - (a) wing
 - (b) tail cone
 - Anti-collision beacons (4)
 - (a) upper
 - (b) lower
 - Wing illumination (5)
- M. Ground Handling

4 Hours 1, 2, 3, 6, 8

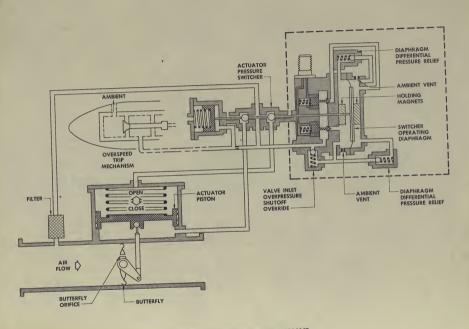
- 1. Parking
 - Typical parking
 - (1) Nose in
 - (2) Nose out
 - (3) Parallel
 - b. Engine ground run clearance
 - (1) Idle and taxi

Transport Service Training

- a, Crew compartment
 - General lighting
 - (a) dome lights
 - (b) emergency lights
 - (2) Special lights
 - (a) main instrument panel
 - (b) overhead switch panel
 - circuit breaker panels (c)
 - (d) radar panel
 - aisle stand aft panels (e)
 - engineer's station (f)
 - (g) navigator's station
 - (h) aisle stand
 - (i) map reading
 - brief case (i)
 - (k)
 - auxiliary panel standby magnetic compass (1)
- b, Passenger compartment
 - (1) General lighting
 - (a) dome
 - (b) cove
 - (c) lavatories
 - (2) Special lights
 - (a) reading
 - galley (b)
 - (c) entry
 - (d) lavatory mirror
 - (e) coat compartment (f)
 - passenger signs (g) emergency exit
- Cargo and lower forward compartments c.
 - (1) General lighting
 - forward cargo compartment (a)
 - (b) aft cargo compartment
 - (c) lower section 41

Transport Service Training

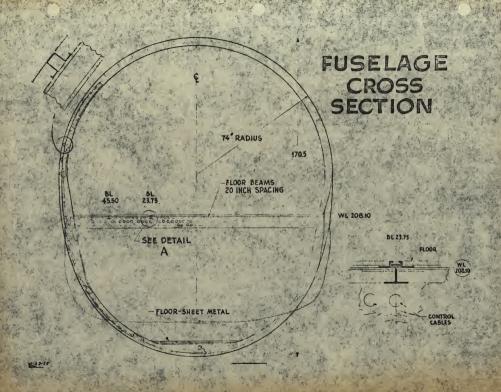
Art Order Number	SECTION 52	PAA-121 D6-1048	AA-123 D6-2757	CAL-124 D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	cua-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-2764	BOAC-L36	AII-437 D6-2762
52-1		CAUCEL						L.	L						
57-2	Cargo Compartment Doors - For- ward	×							L						
52-3	Fain Entry Door - Forward	×	K	X	X	N	Z		X	X	X	8		X	X
52 - lı	Operation of Main Entry Door From Inside	×	×	X	X	K	R	X	×	X	×	X	X	X	. 🗵
52-5	Operation of Main Entry Door From Outside	×	B	X	X	X	X	X	X	K	X	X	X	8	M
52-6	Forward Main Entry Door	K	×	N	K	X	×	Z	K	×	·	K	X	K	
52-7	Forward Main Entry Door Mechanism - Detail II	×	×	X	×		×		N	K	X	A	M	Z	K
52-8	Forward Main Entry Door Mechanism - Detail III	×	×	X	X	X	Z	X	×	X	K	×	K	K	D
52-9	Forward Main Entry Door Mechanism - Detail IV	M	X	X		X	X	X	X	K	×	Z	K	K	X
52-10	Forward Main Entry Door Mechanism - Detail V	X	×	×	K	. 🗵	X	K	K	K	K	K	X	X	
52-11	Forward Main Entry Door Mechanism - Detail VI	×	×	×.	X		X		X	X	X	×	E	K	



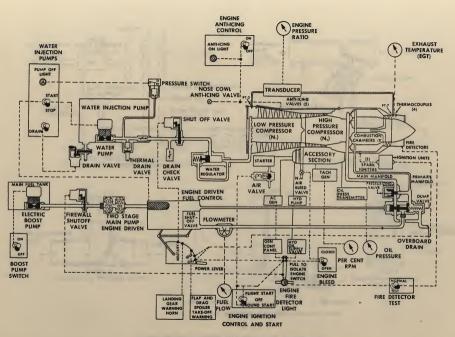
PRESSURE OVERRIDE SHUTOFF VALVE

REV 25 OCTOBER 1957 707-121 1 THRU 99

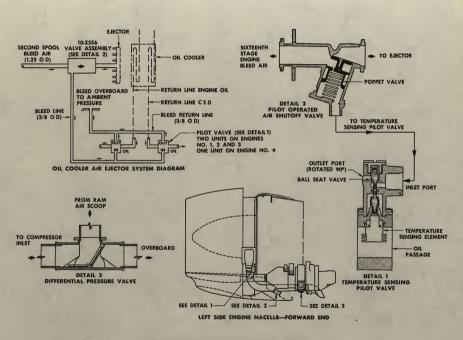
121-21-22 REV A



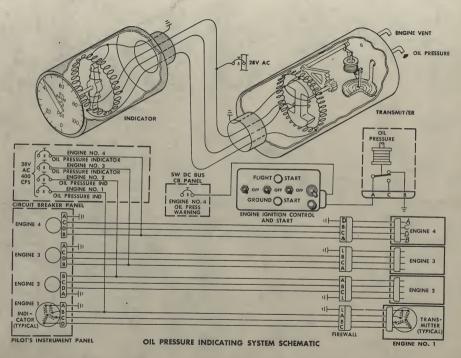
121-71-9 Eng front.



ENGINE OPERATION AND CONTROL DIAGRAM



ENGINE ACCESSORY COOLING DIAGRAM

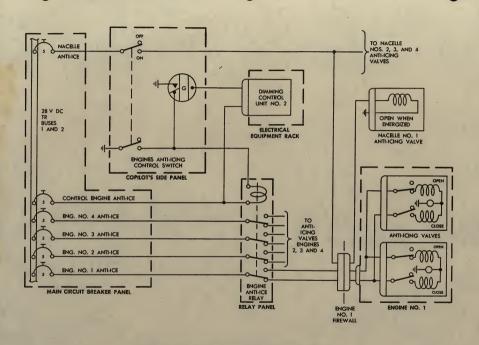


T-10.33

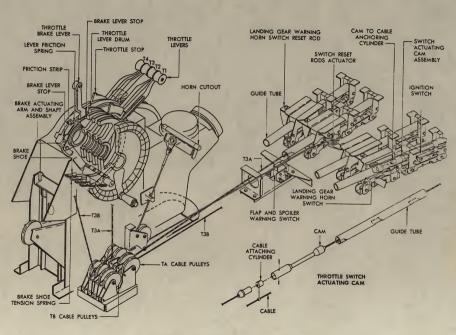
18 JUNE 1956

KC-135 3129 AND ON

5P2 SHT2



ENGINE AND NACELLE ANTI-ICE CONTROL CIRCUIT



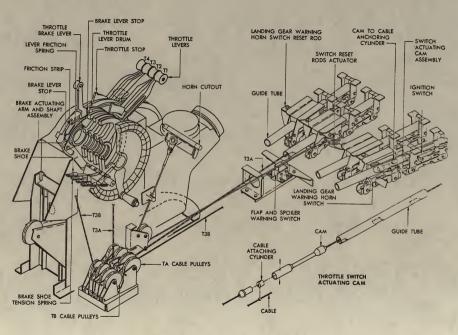
THROTTLE CONTROL LINKAGE - SECTION 41

T-10.16

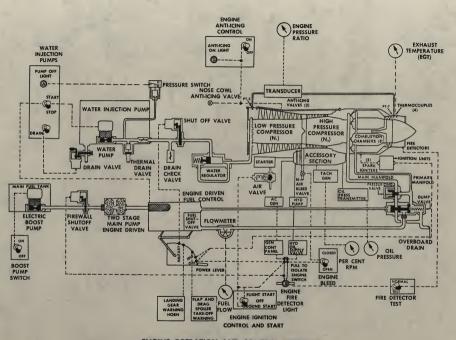
17 OCTOBER 1955

KC-135 55-3118 AND ON

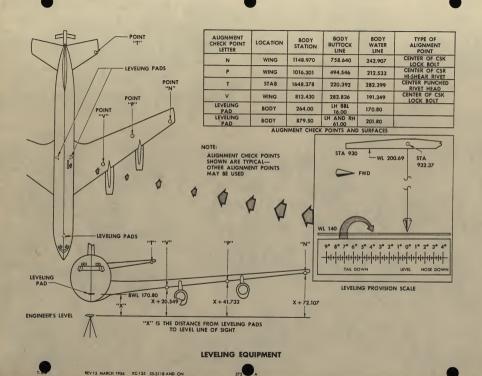
5P9

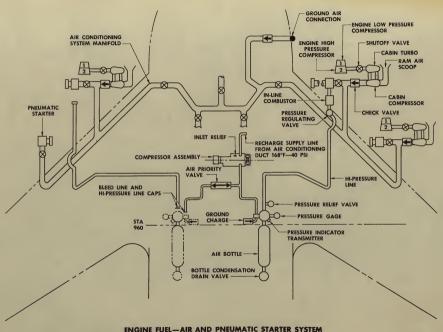


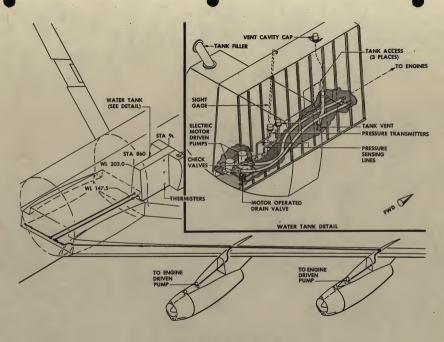
THROTTLE CONTROL LINKAGE - SECTION 41



ENGINE OPERATION AND CONTROL DIAGRAM





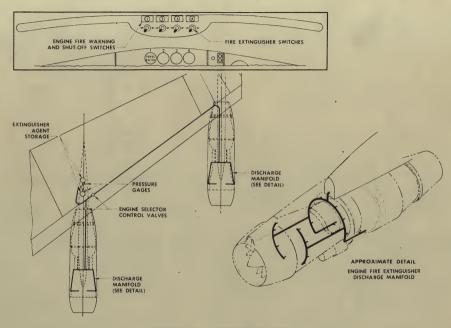


ENGINE WATER INJECTION SYSTEM

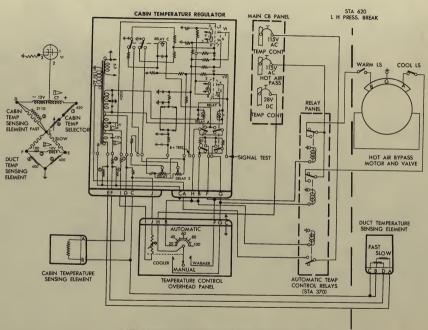
REV 25 JULY 1957

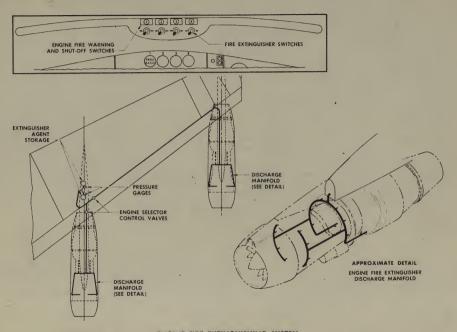
707-121 1 THRU 99

121-82-1 REV D



ENGINE FIRE EXTINGUISHING SYSTEM

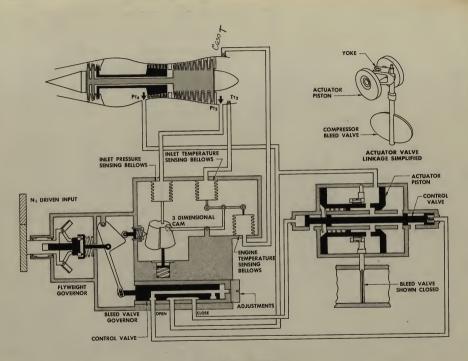




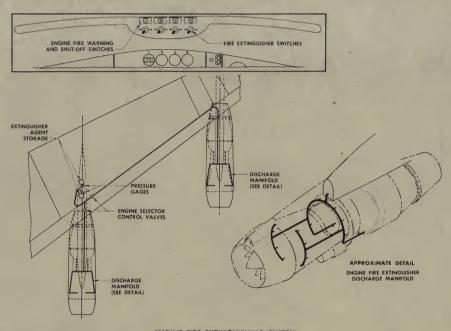
ENGINE FIRE EXTINGUISHING SYSTEM

REV 3 OCTOBER 1956 707-121 1 THRU 99

7P6 REV B



SURGE BLEED CONTROL



ENGINE FIRE EXTINGUISHING SYSTEM

REV. 3 OCTOBER 1956 707-121 | THRU 99

7P6 REV B

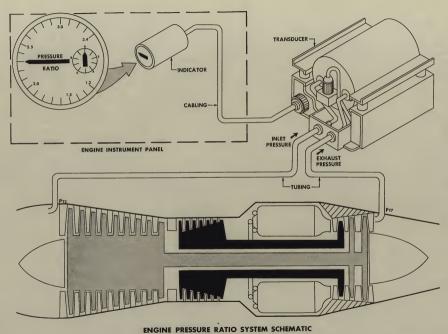
707 COMPANY TRAINING

COURSE NO. 707-002

GENERAL FAMILIARIZATION

CURRICULUM

DAY	SUBJECT	HOURS	INSTRUCTOR
Nov. 11 (Mon.)	Orientation Airplane General Description Structures Power_Plant	-la-la 2 5	Gumtow Allen Allen Monchil
Nov. 12 (Tues.)	Electrical Fower Fuel Systems Pneumatic System	3½ 3½ 1	Sorensen Schmidt Trimble
Nov. 13 (Wed.)	Air Conditioning and Pressurization Systems Ice Elimination, Defogging and Rain Protection Hydraulic (Power Supply) Landing Gear	3 1 1 3	Trimble Trimble Lyon Lyon
Nov. 14 (Thurs.)	Landing Gear (Con't) Flight Controls Autopilot Communication & Navigation Equipment Miscellaneous Systems	1 3 1 2	Lyon Cole Cole Norton Bain
Nov. 15 (Fri.)	Miscellaneous Systems (Con't) Ground Handling and Servicing Operation and Performance	3 2 3	Bain Monchil Rowland



ENGINE PRESSORE RATIO STATE

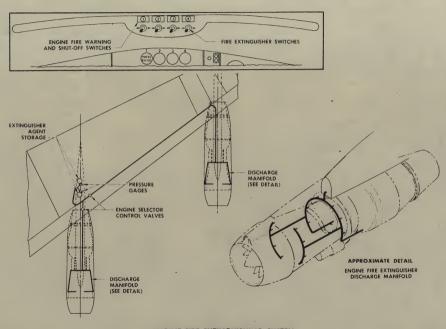
- (a) jack points used
- (b) electronic weighing cells
- 6. Hoisting and equipment
 - Hoisting slings and attach points
 - (1) Empennage attach points
 - (a) elevators
 - (b) stabilizer
 - (c) vertical fin
 - (2) Engine removal and installation equipment
 - (a) hoisting sling
 - hydraulic dolly (b)
 - Special tools (3)
- 7. Examination and review
- N. Servicing

8 Hours 1, 2, 3, 6, 8, 9, 10, 11

- Servicing equipment
 - Carts and trucks
 - (1) Fuel truck
 - (a) service locations
 - (b) pressure requirements
 - (c) flow rate
 - (2) Baggage and cargo
 - (a) type
 - service location (b)
 - (3) Galley cart
 - (a) type
 - (b) service location
 - (4) Water service cart

Transport Service Training

10:30 -	11:20	Engine General continue	d 25 mounting etc.
1225	1250	-Bleed systems	25
1250	0115	Oil Sys.	25
011.5 Break	0140	Water Injection	25
0200	0220	Fire Protection	15.
0220	0235	Engine Instruments	15
0235	0250	Engine Controls	15:
0300	0325	Fuel & Ignition	25
0325	0350	Start Sys.	25
0350	0400	Thrust Reverser	10



ENGINE FIRE EXTINGUISHING SYSTEM

REV 3 OCTOBER 1956 707 121 1 THRU 99

7PA REV B

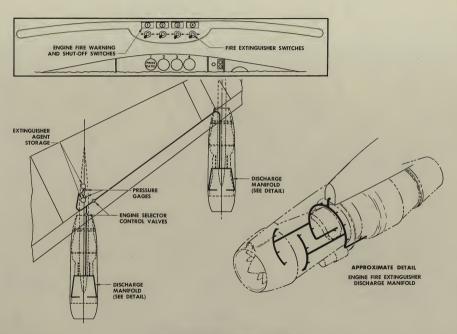
Call on thrust reverser Ken Farris

Tver Pollard - spares 2665

11(111

SUBJECT	TIME	INSTRUCTOR
Fuel Systems	8:00	LaViolette
	9:30	Da / Miche
Coffee Break	9:30	
•	9:50	
Fuel Systems (Con't)	9:50	LaViolette
	10:20	
Cabin Air Conditioning & Pressurization	10:20	Spicer
Systems	12:30	
Lunch	12:30	
	1:30	
Ice Elimination, Defogging and	1:30	Spicer
Rain Pretection	2;30	•
Hydraulics	2:30	Smith
	2:50	
Break	0.50	
an wan	2:50 3:00	
Landing Gear	3:00	Smith
	4:00	

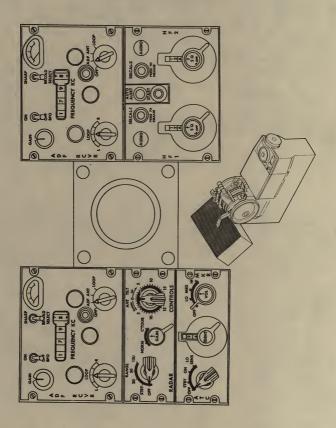
ATA 100 for use in setting up trouble shooting charts



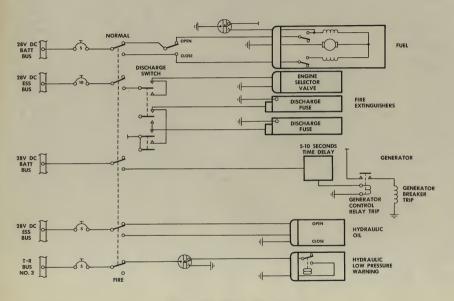
ENGINE FIRE EXTINGUISHING SYSTEM

121-26-2 new B

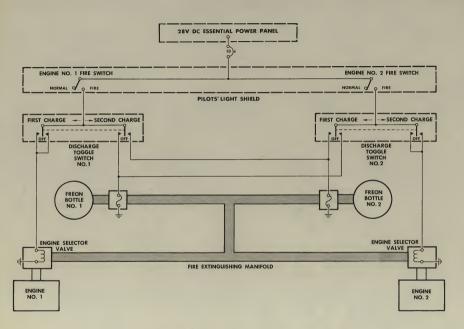




Forward Electronic Control Panel Figure 1

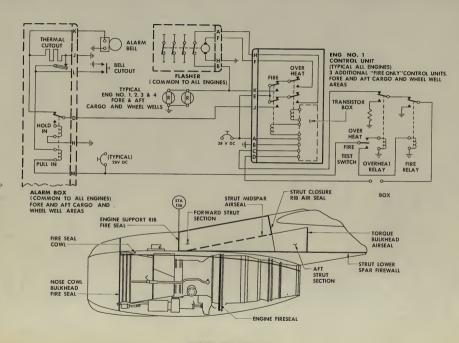


ENGINE FIRE SWITCH SCHEMATIC



ENGINE FIRE EXTINGUISHING SYSTEM CONTROL

9 JANUARY 1957 707-121 1 THRU 99



ENGINE FIRE DETECTOR

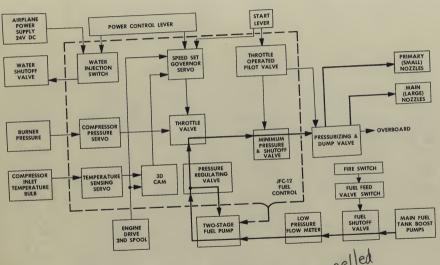
REV 21 MAY 1957 707-121 1 THRU 99

121-26-1 REV C

FRAME NO. B

BLACK PLATE OF 2

JA This anything interesting to ym? It was in garage, M. H.



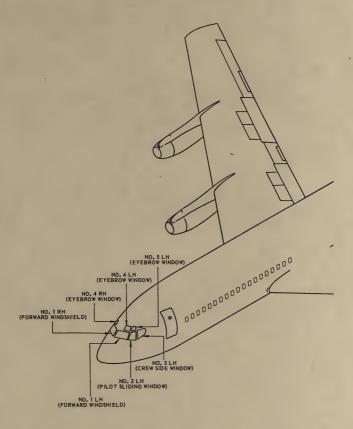
ENGINE FUEL SYSTEM BLOCK DIAGRAM CONCELLED

707-121 1 THRU 99 REV 27 SEPTEMBER 1956

121.73-2

X	APT ORDER WOLTEN THENSPARENCY RELEASED	-	WF-LA	TTI	ENTRI	ELE	ASE!	D		<u></u>	AIR	LINI	E	BRO SL	CH -	FOR	GIN/ R BI R SE ISOI	PCI	ASTI HUR CE	E-UP
ART. ORDER NUMBER	section 80 starting	PAA 121	AA 123	CAL 124	TWA 131	QEA 138	CUB 139	VARIG			BNF 227			PAA 321	AF 328	SAB 329	TWA	LUFT 430	BOAC 436	A11 437
80-1	Engine Fuel - Air And Pneumatic Starter System	PU B			L															
80-2	Engine Start Circuit	POA																		
80-3	Engine Pneumatic Starter Control System	POA						_							-					
- 80-4	Air Turbine Starter	X									h									
√ 80 - 5	Starter Clutch Schematic	A																		
-1.80-6	Combustion Starter Air Distrib- ution	X																		
1				10	li									-9						
-																				
-		h			h			1					6	74			5			
3.5						-			1					1				- 1		
	-13-57 H-26-59						-					-								1

X -	APT ORDER WOTTEN —TRANSPARENCY RELEASED		WR-LA	TES	ENTR	RT C	ASE	D .		F	AIR	LIN	Ē		CH -	FOF	RB	RVI	HUR	E-UP E
ART ORDER . NUMBER	SECTION 12 SERVICING	PAA I2i	A A 123	CAL 124	TWA 131	QEA 138	CUB	VARIG			BNF 227			PAA 321	AF 328	SAB 329	TWA 331	LUFT 430	BOAC 436	A11:
12-1 12-1-6 =16-202	- Typical Terminal Servicing Arrangement	PUC	PUB.	X	BROCH	BROCH			ŀ		X X			Á	BREE	BROCH	B SL B	X	X	Весен
12-2	Walkways, Access Doors and In- spection Openings - Top View	Bloca			BROWN	BROCH		7			-		L		BROCH	ВКОСН			PU X	ER OXH
12-3	Access Doors and Inspection Openings - Bottom View	B	h		BEOCA	BICOCH	i	L	L						BROCK	BROCH	L	L	X	BC OCH
12-4	Four Point Refueling Requirements	PUX SL X	X	SL	X	X		L	L		X			PU X SL	A A	X	A SL A	X	X	X
12-5	Cabin Temperature VS Time - Chrysler Air Temperature (22 Ton)	PUX SL X	X	X	SL X	X		L	L		X			X SL X	X SL X	X	X	X 3L	X . 5L X	X SL X
12-6	Cabin Temperature VS Time - GTCP 185 Pneumatic Cart	PUX SL X	X	X SL X	X St X	X X			-		X			X 54 X	X 5L X	X	SL X	X	X SL X	X SL X
12-7	The Park of the Pa					-			L					L	L	L				
12-8	Typical Terminal Service - Left Side	PUX	4			4		L				L				L				
1249	Typical Terminal Service - Right Side	PUX	L	L	-	4	L		L		4	-			L		L		L	
12-10	Tire De-Mounting Tool	4	4	-		-	-	-	-	L	-	-	-		PUX		-	X	X	X
		L	4	- 1		-	-		L	-	L	L				L		-	L	E
REV 11	15-57 13/12/37	/											_		-			-		



End 56-1-0 Page 2 Control Cabin Windows Location Diagram
Figure 1

£-4683

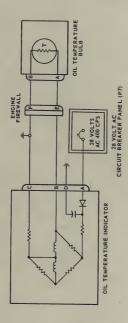
SE 495/

Ginter 363

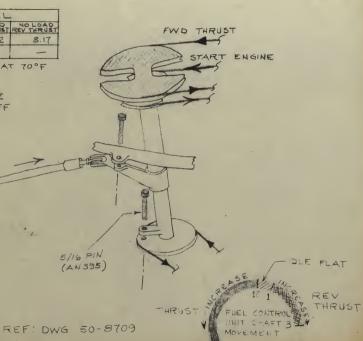
Scott Hinkley 2-3561

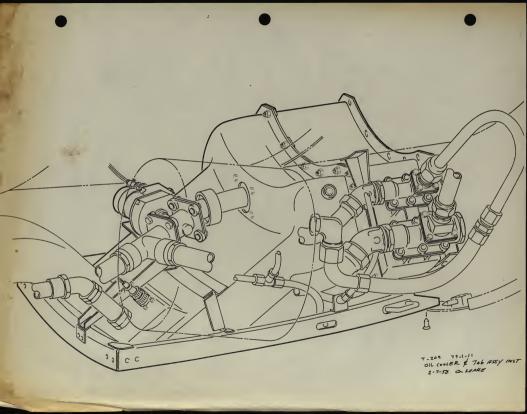
L.E. Buchart

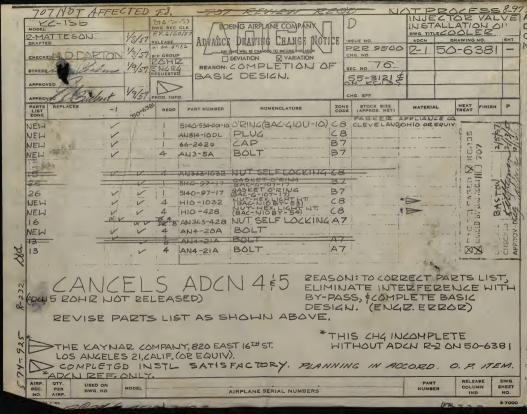
$$\frac{\frac{125}{2} 625}{\frac{625}{31250}}$$



	21-			
	CABLE	TRAVEL	•	
CABLE	NO LOAD	NO LOAD THRUST	REV THRUST	
THRUST	7.39	4.22	3.17	
START	2.27		_	
RIGGING I	DAO = 40	± 5 LB. A.	70°F	CA.
RIGGING	POSITIO	N		
	T LEVE			
		CUTOFF		1
			7	
		Bo		







DRAFTE	707 EARL RILEY	67/1	R 7	17-10 WG. REC 2/7-11 ELEASE -11-57C	ADVANC	DEING AIRPLANE COMPANY DRAWING CHANGE NOT	p	1 RR 107 4 7	DULT CAC DWG. TIT ADCN	SYSTE	MS	OUT BO	OARI SHT
APPROVI	Table also all	7-	R	IR CO!	UP TO	DEVIATION SVARIATION TO BRING DRAWING DATE	SE	74. 1-199 801-1999					
LIST ZONE	REPLACES	-1.	8252	REQD	PART NUMBER	NOMENCLATURE	ZONE	STOCK SIZE (APPROX. NET)	MATERIA	AL P	HEAT REAT	FINISH	P
43		1	1			DUGT-ASSY OF	C-6						-
	65-2016-7	V	V	1	65-2016-12	DUCT-ASSY OF	C6						

CHANGE P/L AS SHOWN ABOVE
IN TONETAG & C-6 CHANGE PICTURE CALL OUT FROM 65-2016-7 TO 65-2016-12 IN
BOTH VIEWS

WORK NUMBER REQD SLEEVE REOD ZONE SHT TUBING MIN TUBE WALL PRESS. MATERIAL IDENT-STOCK ZONE THICK TREAT TUBE ASSY END FITTINGS PER TUBE ASSY PSI CODE **IFICATION** LGTH

DISCUSSION

The reported structural defects are most concentrated in areas subject to high jet engine noise levels and jet buffeting, which are the lower surface and trailing edge of the wing. The inboard and outboard atlerons are located in line with the engines, and their control tabs are the most troublesome structural components. This is further substantiated by analyses of AFM 66-1 malfunction and man-hour expenditure rates per square foot of projected structure surface (references c and f). These analyses were based on data from the whole KC-135 fleet.

A previous summary and analysis of the reported structural defects on the 707-100 series airplanes (reference d) shows a marked contrast with the above observation in that no particular areas of malfunction concentration can be discerned. Very few reports of structural defects in areas of high jet engine noise levels were received on the 707, except for heneycomb delamination which will be discussed separately. However, it is felt that malfunctions similar to those reported on the KC-135 are occurring in these areas, but to an extent reduced by the less severe sonic environment on the 707 as follows:

- Engine noise is attenuated by sound suppressors. This lowers the sound pressure levels on the control surfaces by at least 6 db in the lower frequency ranges that are the most damaging to structure.
- Take-off and initial climb are usually made at lower EPR settings, and water injection is not so frequently used.
- Engine running time on the ground is less than on the KC-135 because of differences in procedures. KC-135s are subject to considerable dry and wet trimming and high powered ground engine running during practice elects.

In addition, many of the malfunctions experienced on the 707 have probably been attributed to normal wear and tear and are not reported after the warranty runs cut. It is noteworthy that nearly all of the structural malfunctions on the KC-135 are of a muisance type which are principally repaired during postflight and periodic inspections. Similarly such miner malfunctions on the 707 are not usually corrected on the flight line, and since they do not usually affect flight scheduling or flight safety are not brought to the attention of the Field Service Engineers and we do not hear of them.

Service experience of about 330,000 fleet hours on the KC-135 has shown that its basic structure, apaff from the main landing gear support structure, has been relatively free from major trouble. Initial problems, such as the cracking of splice plates, art body skin and tailcone, led to design changes or modifications early in the program, and were eliminated before serious hazard or maintenance man-hour expenditure developed. Minor nuisance malfunctions, which accounts for a good deal of the total maintenance man-hour expenditure, have been generally attributed to engine vibration, noise, and jet buffeting. The latter may be the most important contributor to structural malfunction in the jet wake as high speed films taken during the sonic fetigue test showed heavy racking and buffeting of the inboard ailerons. A decline in the reported honeycomb malfunctions which has been evident for some time is considered to be due to the introduction of nonperforated honeycomb.

Analysis of the 707 service experience (reference d) indicated a marked similarity in homeycomb malfunctions. Homeycomb sandwich construction, particularly the nonperforated type, has demonstrated good sonic fatigue resistance on the 707, on which some control surfaces are known to have exceeded 5,000 hours without malfunction. This is because of its good characteristics for dissipation of sonic energy and resistance to vibration, since it gives a structure with higher natural frequencies than conventional structure (reference h). It is therefore less susceptible to damage in the frequency range of the 150 to 600 cps duo-octave band, in which jet engines have a definite tendency to concentrate more power (reference g).

It should be noted that the effect of various modifications on the malfunction frequency is not separately reflected in the table and figures presented. They deal with the overall malfunctions reported since first delivery.

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DISCUSSION

The reported structural defects are most concentrated in areas subject to high jet engine noise levels and jet buffeting, which are the lower surface and trailing edge of the wing. The inboard and outboard allerons are located in line with the engines, and their control tabs are the most troublesome structural components. This is further substantiated by analyses of AFM 66-1 malfunction and man-hour expenditure rates per square foot of projected structure surface (references c and f). These analyses were based on data from the whole KC-135 fleet.

A previous summary and analysis of the reported structural defects on the 707-100 series airplanes (reference d) shows a marked contrast with the above observation in that no particular areas of malfunction concentration can be discerned. Very few reports of structural defects in areas of high jet engine noise levels were received on the 707, except for heneycomb delamination which will be discussed separately. However, it is felt that malfunctions similar to those reported on the KC-135 are occurring in these areas, but to an extent reduced by the less severe sonic environment on the 707 as follows:

- Engine noise is attenuated by sound suppressors. This lowers the sound pressure levels on the control surfaces by at least 6 db in the lower frequency ranges that ere the most damaging to structure.
- Take-off and initial climb are usually made at lower EPR settings, and water injection is not so frequently used.
- Engine running time on the ground is less than on the KC-135 because of differences in procedures. KC-135s are subject to considerable dry and wet trimming and high powered ground engine running during practice alerts.

In addition, many of the malfunctions experienced on the 707 have probably been attributed to normal wear and tear and are not reported after the warranty runs cut. It is neteworthy that nearly all of the structural malfunctions on the KC-135 are of a muisance type which are principally repaired during postflight and periodic inspections. Similarly such miner malfunctions on the 707 are not usually corrected on the flight line, and since they do not usually affect flight scheduling or flight safety are not brought to the attention of the Fleid Service Engineers and we do not hear of them.

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Analysis of the 707 service experience (reference d) indicated a marked similarity in honeycomb malfunctions. Honeycomb sandwich construction, particularly the nonperforated type, has demonstrated good sonic fatigue resistance on the 707, on which some control surfaces are known to have exceeded 5,000 hours without malfunction. This is because of its good characteristics for dissipation of sonic energy and resistance to vibration, since it gives a structure with higher natural frequencies than conventional structure (reference h). It is therefore less susceptible to damage in the frequency range of the 150 to 600 cps duo-octave band, in which jet engines have a definite tendency to concentrate more power (reference g).

It should be noted that the effect of various modifications on the malfunction frequency is not separately reflected in the table and figures presented. They deal with the overall malfunctions reported since first delivery.

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Coordination Sheet 61-5 Page Ten

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- (g) Boeing Document D-17130, Review of Testing and Information on Sonic Fatigue, dated March 7, 1957
- (h) Kazimi, M. I., Sandwich Cylinder, Part I State of the Art and Advantages of Sandwich Construction. Aerospace Engineering, Vol. 19, No. 8, August 1960, pp. 32-37

Attachments:

- I KC-135 In Service Action Items, October 1960, page 22, Lower Wing Skin Problem. A brochure prepared by the Military Service Unit for presentation to military personnel at SAC bases
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- IV KC-135 In Service Action Items, October 1960, page 36, Inboard Aileron Tab

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- (c) Service Analysis-Reliability Unit Coordination Sheet 60-160, dated November 9, 1960, NC-135 Analysis of AFM 66-1 Data for January through April 1960
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- (f) Service Analysis-Reliability Unit Coordination Sheet 60-23, dated April 11, 1960, KC-135 Analysis of AFM 66-1 Data from Castle and Offutt Air Force Bases
- (g) Boeing Document D-17130, Review of Testing and Information on Sonic Fatigue, dated March 7, 1957
- (h) Kazimi, M. I., Sandwich Cylinder, Part I State of the Art and Advantages of Sandwich Construction. Aerospace Engineering, Vol. 19, No. 8, August 1960, pp. 32-37

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- (c) Service Analysis-Reliability Unit Coordination Sheet 60-160, dated November 9, 1960, NC-135 Analysis of AFM 66-1 Data for January through April 1960
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- IV KC-135 In Service Action Items, October 1960, page 36, Inboard Aileron Tab

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- (b) Service Analysis-Reliability Unit Coordination Sheet 61-1, dated January 4, 1961, KC-135 Main Landing Gear Malfunction History to Assist in the 731-476L Design
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 - IV KC-135 In Service Action Items, October 1960, page 36, Inboard Aileron Tab

References:

- (a) Service Analysis-Reliability Unit Coordination Sheet 61-4, dated February 20, 1961, Analysis of XC-135 Aluminum Honeycomb Malfunctions Reported Prior to January 1, 1961
- (b) Service Analysis-Reliability Unit Coordination Sheet 61-1, dated January 4, 1961, KC-135 Main Landing Gear Malfunction History to Assist in the 731-476L Design
- (c) Service Analysis-Reliability Unit Coordination Sheet 60-160, dated November 9, 1960, KC-135 Analysis of AFM 66-1 Data for January through April 1960
- (d) Service Analysis-Reliability Unit Coordination Sheet 60-116, dated August 31, 1960, 707-100 Series Structural Malfunctions
- (e) Service Analysis-Reliability Unit Coordination Sheet 60-45, dated June 2, 1960, Malfunctions and Unscheduled Removals of Honeycomb Parts with Metallic Core in Nonpressurized Areas
- (f) Service Analysis-Reliability Unit Coordination Sheet 60-23, dated April 11, 1960, KC-135 Analysis of AFM 66-1 Data from Castle and Offutt Air Force Bases
- (g) Boeing Document D-17130, Review of Testing and Information on Sonic Fatigue, dated March 7, 1957
- (h) Kazimi, M. I., Sandwich Cylinder, Part I State of the Art and Advantages of Sandwich Construction. Aerospace Engineering, Vol. 19, No. 8, August 1960, pp. 32-37

- I KC-135 In Service Action Items, October 1960, page 22, Lower Wing Skin Problem. A brochure prepared by the Military Service Unit for presentation to military personnel at SAC bases
- II KC-135 In Service Action Items, December 1960, pp. 38 and 39, Aileron Tab Bearings
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 - IV KC-135 In Service Action Items, October 1960, page 36, Inboard Aileron Tab

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C. Distribution of Malfunctions as Related to Sound Pressure Level

Eight different malfunction types have been assigned symbols for identification as shown in the summary table.* Each primary structural malfunction has been indicated by the assigned symbol at its approximate location on Figures 1, 2 and 3 (page 12 and on) which respectively are diagrams of the KC-135 left wing, left stabilizer and vertical fin.

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Figures 4, 5 and 6 (page15 and on) show 25 by 25 inch matrices within the outlines of the wing, horizontal stabilizer and vertical fin, respectively, on which the number of malfunctions occurring in each unit area have been shown. Lines of constant sound pressure level, measured on a static KC-135 at full wet power, are shown on an isometric sketch of the KC-135 on Figure 7 (page 16) and have been superimposed on the matrices.

Figure 4 indicates that structural defects on the wing are heavily concentrated in areas behind the engines where control surfaces are subject to high jet engine noise levels and jet gas buffeting; frequency of occurrence increasing with noise intensity toward the trailing edge. Figures 8 and 9 (pp. 19 and 20) show lines of constant sowned pressure level at full wet and dry power, respectively, on the wing lower surface and the relative location of the various control surfaces. These figures show that the wing control surfaces experience approximately a 5 db higher sound pressure level than contigous wing structure at full dry or wet and presumably at all power settings. They also show that aileron tabs are always exposed to the highest sound pressure levels and are by far the most troublesome components of their structure type.

Figures 5 and 6 indicate a fairly constant sound pressure level for a given power setting on all of the empennage and further that structural defects are predominant on the tabs and trailing edges. These components on both empennage and wing are of necessity of light construction, which apparently does not give sufficient resistance to fatigue.

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Figures 5 and 6 indicate a fairly constant sound pressure level for a given power setting on all of the empennage and further that structural defects are predominant on the tabs and trailing edges. These components on both empennage and wing are of necessity of light construction, which apparently does not give sufficient resistance to fatigue.

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C. Distribution of Malfunctions as Related to Sound Pressure Level

Eight different malfunction types have been assigned symbols for identification as shown in the summary table.* Each primary structural malfunction has been indicated by the assigned symbol at its approximate location on Figures 1, 2 and 3 (page 12 and on) which respectively are diagrams of the KC-135 left wing, left stabilizer and vertical fin.

In a more detailed analysis, which is not included for brevity, the malfunctions on the left and right wing and stabilizers were separately plotted, but no significant difference was detected. About 95% of the surface malfunctions (skin cracks, delaminations and loose skin fasteners) occurred on the lower surface. Malfunctions on both left and right wings and horizontal stabilizers are shown on the left hand components on Figures 1 and 2, and no distinction is made between malfunctions occurring on the upper or lower surface; nor are those occurring on interior parts distinguished in any way.

Figures 4, 5 and 6 (page15 and on) show 25 by 25 inch matrices within the outlines of the wing, horizontal stabilizer and vertical fin, respectively, on which the number of malfunctions occurring in each unit area have been shown. Lines of constant sound pressure level, measured on a static KC-135 at full wet power, are shown on an isometric sketch of the KC-135 on Figure 7 (page 18) and have been superimposed on the matrices.

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To:

A. C. Larsen J. A. Wallen

cc:

See Page Nine

Subject:

KC-135 Structural Malfunctions and Their Relation to

Engine Noise, Vibration and Jet Buffet.

References:

See Page Ten

SUMMARY

During nearly four years and 330,000 hours flown by 430 KC-135 aircraft, major structural malfunctions (neglecting the landing gear and its support structure) have been few. They were:

- Cracking of lower wing to center section splice plates occasioned by rework
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- Cracking of the aft body skin found during the structure endurance test at
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- 3. Cracking of the forward boost pump support forging has been attributed to stress corrosion caused by residual stresses in the forging, and water acting on machined areas of the forging where the top coating was inadequate. All cracks have occurred at the forward pump position where more water tends to collect. No cracks have occurred on airplane 362 or later, on which the support forging has been given a sealant top coat.
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Coordination Sheet: 61-5 Date: March 14, 1961 Model: KC-135

To:

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cc:

See Page Nine

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J. A. Wallen

cc: See Page Nine

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Coordination Sheet: 61-5 Date: March 14, 1961 Model: KC-135

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Coordination Sheet: 61-5 Date: March 14, 1961 Model: KC-135

To: A. C. Larsen

cc: See Page Nine

J. A. Wallen

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cc:

See Page Nine

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To:

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cc:

See Page Nine

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- Cracking of the aft body skin found during the structure endurance test at full wet power, which was overcome by installing two inch wide external circumferential tear stopping and stabilizing bands.
- 3. Cracking of the forward boost pump support forging has been attributed to stress corrosion caused by residual stresses in the forging, and water acting on machined areas of the forging where the top coating was inadequate. All cracks have occurred at the forward pump position where more water tends to collect. No cracks have occurred on airplane 362 or later, on which the support forging has been given a sealant top coat.
- 4. Two cases of fatigue cracking of the lower wing skin inboard of number three nacelle which are still under investigation.

- Homeycomb delaminations caused principally by water freezing inside perforated core homeycomb, and which have been very much reduced by the introduction of nomperforated homeycomb.
- Control surface hinge year and cracking, which it is hoped will be evercome by the installation of teflon-lined spherical bearings.



Coordination Sheet: 61-5 Date: March 14, 1961 Model: KC-135

To: A. C. Larsen

J. A. Wallen

cc: See Page Nine

Subject: KC-135 Structural Malfunctions and Their Relation to

Engine Noise, Vibration and Jet Buffet.

References: See Page Ten

SUMMARY

During nearly four years and 330,000 hours flown by 430 KC-135 aircraft, major structural malfunctions (neglecting the landing gear and its support structure) have been few. They were:

- Cracking of lower wing to center section splice plates occasioned by rework
 and fit up stresses from distortion during heat treatment. The change from
 four to nine splice plates has so far been entirely effective.
- Cracking of the aft body skin found during the structure endurance test at
 full wet power, which was overcome by installing two inch wide external
 circumferential test stopping and stabilizing bends.
- 3. Cracking of the forward boost pump support forging has been attributed to stress corrosion caused by residual stresses in the forging, and water acting on machined areas of the forging where the top coating was inadequate. All cracks have occurred at the forward pump position where more water tends to collect. No cracks have occurred on airplane 362 or later, on which the support forging has been given a sealant top coat.
- 4. Two cases of fatigue cracking of the lower wing skin inboard of number three nacelle which are still under investigation.

- Roneycomb delaminations caused principally by water freezing inside perforated core honeycomb, and which have been very much reduced by the introduction of nonperforated honeycomb.
- Control surface hinge wear and cracking, which it is hoped will be evercome
 by the installation of teflon-lined spherical hearings.

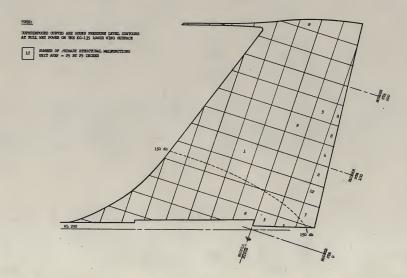


FIGURE 6 - DISPOSITION OF PRIMARY MALFUNCTIONS IN RELATION TO SOUND PRESSURE LEVELS ON KC-135 FIN AND HUDDER

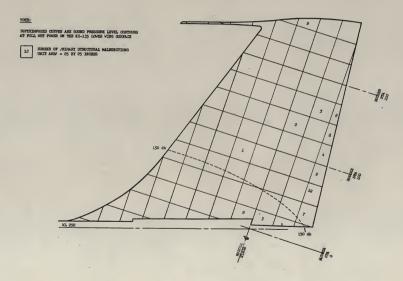


FIGURE 6 - DISPOSITION OF PRIMARY MALFUNCTIONS IN RELATION TO SOUND PRESSURE LEVELS ON KC-135 FIN AND RUPDER

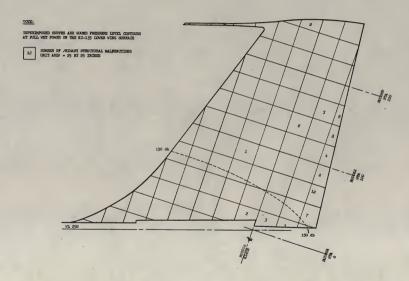


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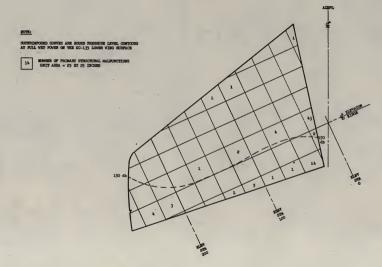


FIGURE 5 - DISPOSITION OF PRIMARY MALFUNCTIONS IN RELATION TO SOUND PRESSURE LEVELS ON KC-135 L & R HORIZONTAL STABILIZER AND ELEVATOR

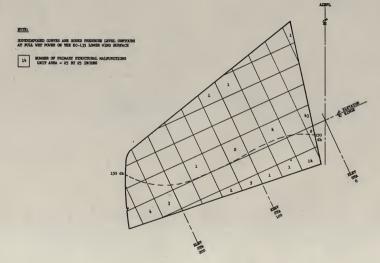


FIGURE 5 - DISPOSITION OF PRIMARY MALIFUNCTIONS IN RELATION TO SOUND PRESSURE LEVELS ON KC-135 L & R HORIZONTAL STABILIZER AND ELEVATOR

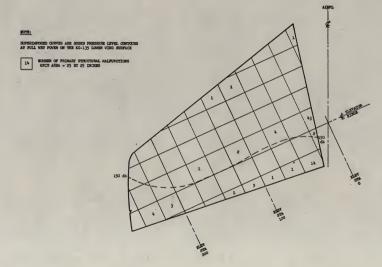


FIGURE 5 - DISPOSITION OF PRIMARY MALFUNCTIONS IN RELATION TO SOUND PRESSURE LEVELS ON KC-135 L & R HORIZONTAL STABILIZER AND KLEVATOR

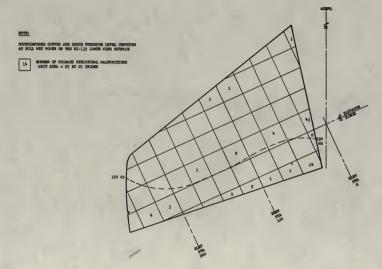


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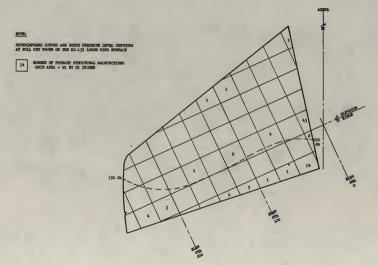


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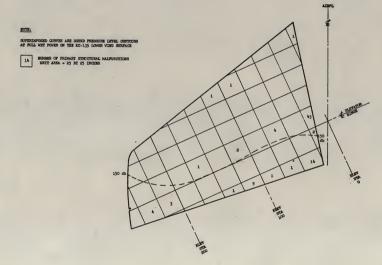


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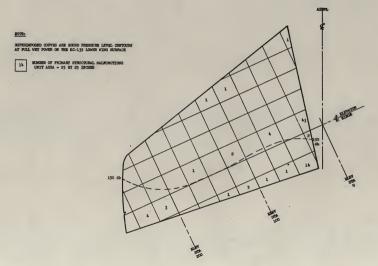


Figure 5 - Disposition of primary malfunctions in relation to sound pressure levels on kC-135 L & R Horizontal Stabilizer and klevator

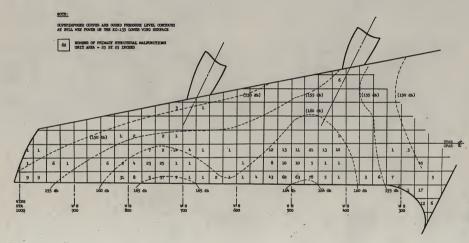


FIGURE 4 - DISPOSITION OF PRIMARY MALFUNCTIONS IN RELATION TO SOUND PRESSURE LEVELS ON KC-135 L & R WING AND CONTROL SURFACES

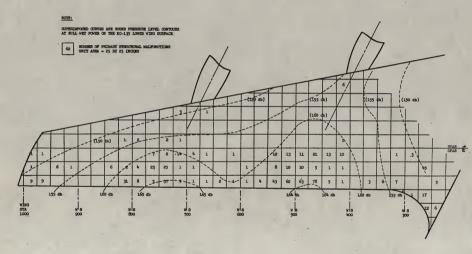


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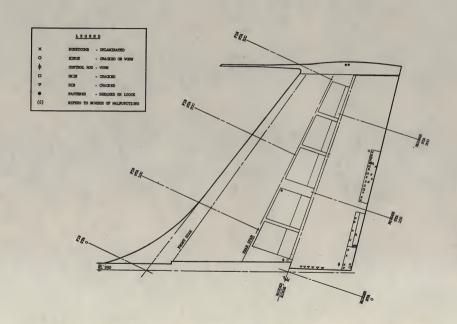


FIGURE 3 - PRIMARY MALFUNCTIONS OF KC-135 FIN AND RUDDER STRUCTURE

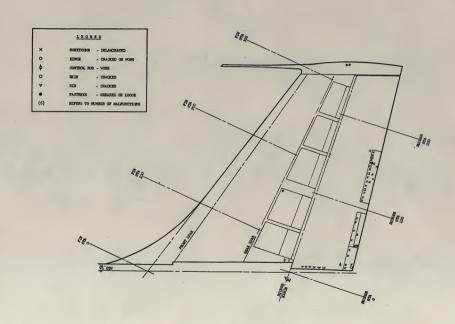


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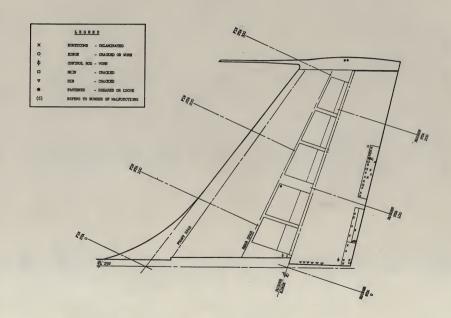


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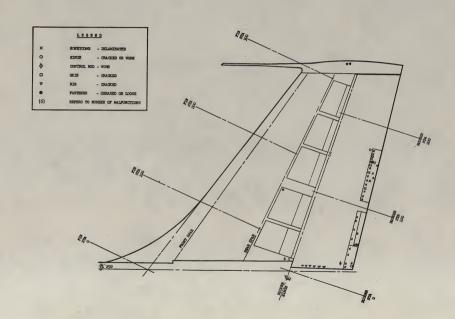


FIGURE 3 - PRIMARY MALFUNCTIONS OF KC-135 FIN AND RUDDER STRUCTURE

Coordination Sheet 61-5 Page Two

- Control push rod bearing wear, loose rivets and bending have caused considerable trouble. The only remedial action has been to increase the rivet size.
- 4. Cracking of skin, ribs and stiffeners has occurred predominantly in the wing trailing edge and balance bays. About 300 skin cracks reported in the wing leading edge of 50 sirplanes were attributed to overdriven rivets.
- Cracking of component mounting brackets and clamps has been widespread and
 is considered to be primarily due to engine vibration transmitted by the
 structure.
- Loosening of nuts, bolts and screws has been one of the most frequently
 occurring malfunctions on the KC-135.

CONCLUSIONS

Muisance structural malfunctions have shown a heavy predominance in control surfaces and their supports which are subject to high sound pressure levels and jet buffet (see Figure 4). Reported structural malfunctions on the 707 are generally less frequent than on the KC-135 and show more dispersion. This is attributed to the relatively greater influence of normal wear and tear in the less severe sonic environment of the 707.

RECOMMENDATIONS

It is recommended that in future designs the major problem of jet buffet and sonic damage should be avoided by mounting the engines so that the jet efflux and the highest SFL's are behind most of the airplane and particularly aft of the control surfaces. The 727 engine mounting seems to approach the ideal in this respect. If other considerations prohibit this, it is recommended that:

- Detail design of control surfaces and aft fuselage take account of exposure to jet blast and engine noise. Nemperforated honeycomb has given satisfactory service on the 707 and is considered to have good sonic fatigue resistance.
- 2. Designs of control surface structure be evaluated for sonic fatigue resistance; by full scale; tests.
- 3. Research into the mechanism of sonic fatigue be intensified.
- Laminated construction with viscoelastic inner layer be evaluated for its sonic energy dissipation and resistance to vibration damage.
- Methods of preventing engine vibration from passing into the airplane structure should be investigated.
- The design of component mounting brackets and clamps in jet aircraft be further stadied for improved vibrational load resistance.
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ANALYSIS

Basic airframe and flight controls malfunctions of a structural or a mechanical nature can be classified as:

- Primary structural malfunctions, which are considered within the responsibility of the manufacturer and may be of a design, quality control or manufacturing nature.
- Secondary structural malfunctions, which are those that occurred as a result of related component failure, installation or maintenance error, or foreign object damage.

This analysis covers the primary structural malfunctions reported on the KC-135 wing, rear fuselage and empennage prior to January 1, 1961, which involves about 330,000 flight hours. Secondary malfunctions and malfunctions of the forward and center fuselage, and the landing gear and its support structure are not included. The landing gear malfunctions are adequately covered by reference (b) and such structural malfunctions as occur in the center and forward fuselage appear to be of a random nature and not primarily related to sonic damage.

A. Major Structural Malfunctions

These malfunctions either compromised safety of flight or required extensive maintenance. The first three are not considered to be related to sonic damage.

1. Lower Wing to Center Section Splice Plate Cracking

The splice at BEL 70.5 was originally a four plate configuration. Distortion during processing made it almost impossible to obtain the desired contour in these long, relatively thin, high heat treat steel plates. In consequence, rework and fit up stresses semetimes caused cracking at the bend radius. Sixteen cracked splice plates of this configuration have been reported, the last in September 1960. A change to eight or nine smaller plates (PRR 457-5) alleviated manufacturing and assembly difficulties and was effective in airplane 134 and on. No failures have been reported in the modified splice plates, but 180. 10-135(NA-6 still calls for inspection at hourly postflight.

2. Lower Wing Skin Cracking

Two almost identical cracks have been reported in the lower wing skin, one in AF 58-040 at 655 flight hours (June 1960) and one in AF 57-1450 at 1159 flight hours (February 1961). The cracks were about thirteen inches long in a chordwise direction at approximately Wing Station 392, just inboard of the number three macelle. Cyclic loading caused the crack in AF 58-040, which is shown on Attachment I. It started at a rivet hole and progressed fore and aft stopping at rivets through the front spar, and stringer 15 respectively. First indications are that these were fatigue cracks caused by a stress concentration at the end rivet attaching the skin to the inboard dry bay doubler. A fleet wide inspection to examine affected rivet holes by means of a berescope or other method is under consideration.

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4. Aft Body Skin Cracking

The five hour sonic fatigue test at full wet power showed the susceptibility of the aft body skin to noise damage and skin cracks in the aft body were experienced early in service. To improve the resistance to sonic fatigue, two inch wide circumferential straps were installed on the outside aft body between Station 1150 and 1370 (T.O. 778). These straps, which act as tear stoppers and stabilizers, provide fail-safe structure and have eliminated this type of skin cracking.

5. Tailcone Cracking

Extensive cracking of the tailcome magnesium skin was experienced early in the KC-135 program. Redesigned tailcomes of fiberglas construction were installed on airplanes 216 and on by PRR 4372-1, and further modification of the tail light bracket and its supporting skin was later necessary because of cracking (PRR 4671-1). Limited information from Field Service and AFM 66-1 reporting indicate that the introduction of fiberglas cones, and repair of old configuration metal cones in accordance with PRR 4372 instructions, have virtually eliminated the basic problem

B. Nuisance Malfunctions

These malfunctions are not considered individually, but are analyzed in terms of their type, frequency of occurrence and location. The reported structural malfunctions are summarized by component and type in the table given on page 11. It is emphasized that these represent reported malfunctions only; what proportion they constitute of malfunctions which have actually occurred is not known. The malfunctions of left and right components have not been separated for this summary as no difference in frequency of occurrence could be discerned. Malfunctions fall into six types as follows:

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B. Nuisance Malfunctions

These malfunctions are not considered individually, but are analyzed in terms of their type, frequency of occurrence and location. The reported structural malfunctions are summarized by component and type in the table given on page 11. It is emphasized that these represent reported malfunctions only; what proportion they constitute of malfunctions which have actually occurred is not known. The malfunctions of left and right components have not been separated for this summary as no difference in frequency of occurrence could be discerned. Malfunctions fall into six types as follows:

1. Honeycomb Delamination

of honeycomb malfunctions including delaminations on the KC-135 and 707 is contained in references (a) and (e) respectively. The effect of sonic vibration on honeycomb delamination is evident although the magnitude of its contribution cannot be clearly established.

Honeycomb delaminations represent 14% of the total malfunctions but have shown a steady deciline in frequency of occurrence with the progressive introduction of nomperforated honeycomb. A good number of the delaminations were reported as the result of a special inspection (T.O. 703) particularly those on rudder and elevator tabs. Delaminations caused by water accumulating and freezing were virtually eliminated by the introduction of nonperforated cores in the machined edge panels on the trailing edges and tabs. This change was effective in production on airplane 235 and on for most tabs and trailing edges. Perforated honeycomb in these parts on earlier airplanes is being eliminated from the KC-135 fleet through attritien. It should be noted that crushed edge honeycomb panels still have perforated cores. However, crushed edge panels are not as susceptible to delaminations as machined edge panels because of better sealing.

2. Control Surface Hinge Wear and Cracking

The Table, pllshows that control surface hinges are the most troublesome item of the structure in that they experienced one third of the total structural malfunctions. Malfunctions of control surface hinges consist of excessive bearing wear, loose or sheared hinge and hinge retainer bolts, and loose or oracked fittings. Inboard aileron tab hinge malfunctions, which are characteristic of hinge problems are depicted in Attachment II. Teflon-lined spherical bearings for the three inboard aileron tab hinges and improved bolt terquing have been intreduced to alleviate these troubles. These spherical bearings distribute the load over a larger area which makes them superior to the ball or roller bearings in applications where there is constant vibrational pounding and relatively little rotation. The teflon lining also eliminates the necessity for lubrication.

Sonic vibration, aggravated by jet exhaust buffet, seems to be the underlying cause of these malfunctions and also of worm plano hinge lobes and pin retainers which allow the hinge pin to slide out and pierce the adjoining honeycomb panels. Outboard alleron hinge pin retention was completely revised by FRR 4724 and the aluminum hinge pin retainers on the other tabs were changed to steel.

3. Control Push Rod Wear and Bending

Worn bearings, loose rivets and loose or bent rod ends are the more recurrent problems on control rods and account for 12% of the total reported malfunctions. Actual seizure of eye end bearings and one case of complete rod fracture have been reported.

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4. Cracking of Skin, Ribs and Stiffeners

Cracked structural components such as skins, ribs and stiffeners represent about 25% of the 850 structural malfunctions reported. Skin and beam cracks in the wing trailing edge and cracks in the ribs of the balance bays and control surfaces are the most prevalent malfunctions of this type. In addition, approximately three hundred wing leading edge skin cracks have been found on about fifty airplanes during a special inspection of the whole fleet. These cracks mostly about 3/8 inch long emanated from rivet heles in a spanwise direction, and were attributed to overdriving the rivets during production. Once the prestress is relieved, further crack extension is not expected and stop drilling of cracks up to 3/4 inch long is permitted. The problem of leading edge skin cracking is further discussed in Attachment III.

5. Cracking of Brackets and Clamps

The relatively few malfunctions of brackets reported represent about 6% of the total structural malfunctions. They have mainly occurred on a brace that is located just above the aft hinge bracket of the outboard landing gear door assembly. Also, the bracket that extends from the aft rib at WEL 129.62 to support the lower wing trailing edge has frequently cracked. Both these brackets have been redesigned.

It should be noted that according to AFM 66-1 cracking of hydraulic tubing and component clamps and mounting brackets have been widespread. Component attachment brackets in most other systems have been similarly affected though to a lesser extent. The latter are considered to be caused primarily by engine vibrations transmitted by the structure. In the case of the hydraulic systems, pressure fluctuations are major contributors to such failures.

6. Sheared or Loose Fasteners

Sheared or loose fasteners occur very frequently, but are usually only reported by Field Service Engineers if they affect airplane safety or during special surveys. An example of the former is the backing out of the nose retention screws of the inboard aileres tab from their helicoil inserts. This has caused tab jamming, and is attributed to excessive vibration as described in Attachment IV. T.O. 915 calls for the application of resin cement to the threads of the aileron tab nose weight

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TO: BOEIN	G AIRPLANE COMPANY			4	SUMMARY
Attn:	Seattle Div. W. S. Supt. Sect.	Transport Div.	P. A	Division	Wichita Div. Eng. Serv. Sect.
SUBJECT	PAS AIR BOTTLE CONTE	OF AVEAS			/ H UNCLASSIFIED
-	REFERENCE: Boots	g ltr 6-7171-1-12	 1560 dtd 15 Jun	1960	CLASSIFIED
ROUTING					
ORIGINAL	Reference requests :	relative nervices	ility of two a	oufiguration	ne of the
CN WHO	The writer checked a sugine shop people to fishich reveal the parties the shop supervisor serits of the various	he are responsible tiquiar part mad did not care to d	e for this value, vendor, et	re. There	ere no records
OFFICE BASE FILE	It is regretted that but meither feet most	the writer cannot educated opinion	t supply the reparding the	equested in subject is	formation, available.
UEK UEK		-	Dick Ceist NG-133 Repr		
WHO !	7 DG/da				
FIELD SERVICE SUBJECT FILE					
FILE NO. 040701					
1			VAE	10701	
				35	-
NAME	Diek Goist	REPO	RT NO. GaS AFB	902-69F	DATE 27 June 1960
STATIONSUBJECT	Clinton-Shermen AFB FAS Air Bottle Control		TION Burns Fla	it, Oklahom	MODEL MG-135
REFERENCES_	As listed		LOSURES Rome		MODEL MALES
	FSR FSR	FSR FSR	FSR	FSR	FSR

August 26, 1960 6-7171-1-13217

To: All Field Service Engineers - Investigation

FAS Air Bottle Control Valve - KC-135

(a) Letter 6-7171-1-12560, June 15, 1960 Reference: (b) Letter 6-7171-1-12840, August 3, 1960

Reference (a) letter requested an investigation of the Part Number 38E13-8A (Bendix) versus the Part Number 840 891 (Kidde) and the Fart Number 38E13-3A (Bendix) subject valves. The Part Number 38E-13-8A is installed in production on sirplanes 59-1443 and on and is also supplied through spares.

Reference (b) summarized the results of the investigation which was inconclusive.

At the last weapon system phasing meeting, August 11, 1960, BAC was committed to further evaluation of the Part Number 38E13-8A (Bendix) valve. You are therefore requested to monitor the performance of these valves until further notice and report failure data i.e. part number and reason (if known) to this office. The difficulties of obtaining this type of information are fully realized and your efforts in obtaining this type of data will be appreciated.

File: 0106-01 040701

S

cc: W. B. Dalrymple

W. B. Kuse H. D. Cameron

C. A. Carlson

JCH/frs

June 13, 1960 6-7171-1-12559

To: W. J. Groseclose - Cklahoma City

Subject: FAS Air ottle Control valve, KC-135

Reference: T.O. 10-135(K)A-10, Figure 4-22, Item 25

Project has requested the following information on Ma Air Hottle Control Valves, part must re 38.13-44 (Hendix) Federal Stock Aumber 2995-766-0065, 38-13-34 (Hendix) Federal Stock Humber LELH-1650-512-1530, and 8091 (Hidde) Federal Stock Humber 1650-511-5266; returned to depot for overhaut.

- (1) Quantity of each valve returned for overhaul.
- (2) heason for return of each valve.

After acquiring above information please reply as soon as possible but no later than 27 June 1960.

ceibel

File OL0701

WCS/njh

oc: W. B. Dalrymple

W. il. Kuse

H. D. Cameron

FIELD SERVICE REPORT TO: BOEING AIRPLANE COMPANY Seattle Div. Transport Div. P. A. Division Eng. Serv. Sect. W. S. Supt. Sect. Field Service SUBJECT: FAS Air Bottle Control Valve, KC-135 UNCLASSIFIED X CLASSIFIED 6-7171-1-12560 dated June 15, 1960 Reference requested information on failures of the subject. Failures of the subject are not recorded by part number. It could be assumed, however, that almost all of the failures at this activity are of the old type valves. The following is a list of the work orders on the subject for the last six months. It is the only information available. No comment after the airplane number means that the valve was replaced. Remarks Tightened relief valve 1483 Replaced seals 1459 Replaced gage Adjusted "T" handle 1464 Adjusted "T" handle 1477 Adjusted "T" handle 1462 Adjusted "T" handle Adjusted "T" handle Tichtened relief valve

29 Dec 6 Jan 12 Jan 15 Jan 19 Jan 20 Jan 20 Jan 22 Jan 28 Jan 2 Feb Feb 4 Feb 10 March 1433 15 Harch 19 March 1483 March 1145 SERVICE 23 March 1428 SUBJECT FILE Replaced seals and packing 25 March 1153 Adjusted relief valve FILE NO. 26 April

28 April 1471 6 May

12 May 20 May 3658

Date

4 Dec

li Dec

20 Dec 28 Dec

Attn:

ROUTING

ORIGINAL

BASE FILE

- 35

Robert Brian REPORT NO. AAFB-96-276F DATE 22 June 60 Altus AFB, LOCATION. Oklahoma FAS Air Bottle Control Valve SUBJECT MODEL ENCLOSURES

FSR FSR FSR FSR FSR **FSR FSR**

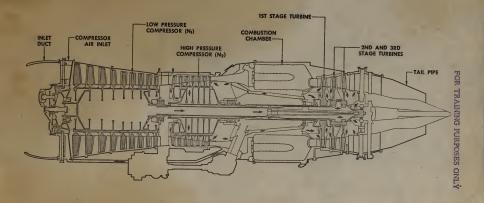
SUPPLEMENTARY SHEET

_D	ate	_ A/P	Remarks
	.lay June	14/3	Tightened B nut
12	June	1471	Replaced gage
	June	11,77	

TD:mm

Robert Brian





INTERNAL COOLING AIR

BOEING AIRPLANE COMPANY

TO: SEATTLE DIVISION

SERVICE SECTION

UNCLASSIFIED

ORIGINAL

BASE FILE

FAS Air Bootle Control Valve

Reference: 6-7171-1-12560, dated 15 June 1960

Information requested by reference letter, fallows:

- 1. There have been 5 of the subject valves replaced and routed through the pneumatic shop since 1 January 1960. Perhaps there have been other valves replaced during TBY operations and maybe several on the line that did not go through the FM shop. All 5 recorde d failures were Kidde, P/N 840891.
- 2. The two most frequent reasons for failure are the relief valve leaks and the gauge is inoperative.
- 3. There are only two of the Bendix 38E13-8A valves presently in service here and not enough available service experience to compare the relative service merits of the different valve configurations. The -8A valves have been on the aircraft only about two months.

R. S. Needy

File: 040701

R.S. Needy Ramey AFB FAS Air Bottle Control Valve Noted Above

REPORT NO ... LOCATION.

RAFB-72-98 Puerto R; co DATE _ 22# June 60 MODEL KC-135

FSR

FSR

FSR

FSR

FSR

FSR



CHAPTER 10

PARKING AND MOORING

TABLE OF CONTENTS

Subject	Subject No.
PARKING	 10-1-1

FIELD SERVICE REPORT BOEING AIRPLANE COMPANY PILOTLESS AIRCRAFT WICHITA DIVISION TRANSFORT DIVISION SEATTLE LIVISION SERVICE SECTION ENGINEERING ENGINEERING DIV. FIELD HH. SERVICE SECTION SERVICE SECTION OPERATIONS DEPT CLASSIFIED [SUBJECT: AS Air Bottle Control Valve KC-135. With reference to 6-7171-12560 6/15/60 and TWX 12863 the following is submitted: ROUTING: Supply records are not necessarily correct, as such, they indicate ORIGINAL (7) seven P/N 840891 valves and (1) one 38E13-8A valve consumed at BAFB. This record and opinion of flight line personnel indicate the improved valve is relatively trouble free compared to the earlier model Walter Kidde valve. John H. Pritt OFFICE BASE FILE Field Service Engineer SERVICE DEPT. 0407 FILE 2-1701 NO 135 REPORT NO. BAFB 913ARS-116F DATE 21 July 1960 John H. Pritt NAME STATION Barksdale AFB LOCATION Shreveport, Louisiana MODEL KC-135 SUBJECT FAS Air Bottle Control Valve, KC-135.

ENCLOSURES

FSR

FSR

FSR

FSR

REFERÊNCES_

BAC 1264-R3

FSR

FSR

FSR

6-700

TO: BOEING AIRPLANE COMPANY

Attn:	

Seattle Div. W. S. Supt. Sect.

FAS Bottle Control Valve

Transport Div. Eng. Serv. Sect.

P. A. Division Field Service

UNCLASSIFIED X CLASSIFIED

SUMMARY |

ROUTING

There are no records at this base that have the information correlating subject P/N's and failure data as desired in reference (a).

ORIGINAL WHD-

BASE FILE

A survey of the fleet here indicates that 75% of the valves installed now are the Kiddie valve P/N 840891 and 25% are the Bendix 38E 13-8A valve.

Hearsay information indicates that there were several failures last winter mostly on the Bendix valve (believed to be the -3A type). Usual cause for failure was forcing of "T" handle when frozen and resulted in leakage.

Spares that are received for replacements have been mostly Kiddie valves.

FIELD SERVICE SUBJECT FILE

Craig E. Field Service Engineer

FILE NO. 040701 CEM: jtm

£2256-1

=1LE 01/6701

			Planting of the same of the sa	
NAME	Craig E. McCreary	REPORT NO.	FAFB-92-125F	DATE 22 July 1960
ATION.	Fairchild AFB	LOCATION	Spokane, Washing	ton
SUBJECT	FAS Bottle Control Valve			MODEL KC-135
REFERENCES	(a) 67171-1-12560 dtd 15 Ju	ne 1960 ENCLOSURES	None	
			LEI	-1 110

FSR

FSR

FSR

FSR

FSR

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FSR

TO: BOEI	NG AIRPLANE	COMPANY				HH		OWWART _
Aitn	Seattle I		Transpo	ort Div.	P. A. Di			ichita Div.
SUBJECT:	FAS Air Bot			rv. Sect.	L_J Field Si	ervice		ICLASSIFIED
	٢			-Manu			Ol-	CLASSIFIED []
	Refere	nce: (a) 6	-7171-1-1	12560, de	ted June 1	15, 1960		
ROUTING		(b) 1	2863 (TW	K), recei	ved July 2	21, 1960		
ORIGINAL	sensus unreli cause Failure instand	of opinion of opinion of opinion of opinion of opinion of opinion of the second of the second of the second opinion of the second opinion of the second opinion of the second opinion opinion of the second opinion op	n is that rvice and cted main ure to op	AS air bot the val	uestioned ttle contr ves are co e rate of red upon a s remember	rol valve onsidered rejection	to be nons does	con- not not
OFFICE BASE FILE	The fol	llowing in ase Supply	formation:	n on valv	e consumpt	cion has	been obt	ained
7	38E13-3	Kidde (48 BA Bendix BA Bendix	(2995-63)	3-2239)	=	8 issu 2 issu 0 issu	ed	
FIELD	Supply No reco	records c	over the lure rece	past six	month per type could	iod only	ined.	
SERVICE SUBJECT FILE								
FILE NO. 0106-01 040701	- - -	· #=	v. •					
NAME	Peter F. Sa				SJAFB-911			July 1960
STATION	FAS Air Bot		ol Velve	LOCATION	Goldsboro	North	Carolina MODEL KC	
REFERENCES	Noted			ENCLOSUR	None	-		-133M
	FSR	FSR	FSR	FSR	FSR	FSR	FSR	

E2256 1

BOEING AIRPLANE COMPANY

SERVICE SECTION

SERVICE SECTION

ENGINEERING SERVICE SECTION

CLASSIFIED UNCLASSIFIED X

ROUTING: ORIGINAL FAS Air Bottle Control Valves

Ltr. 6-7171-4-12560 dated 6-15-60





It has been impossible to monitor the types and number of subject valve failures according to part number. However, the main failures have been with improperly indicating and/or loose gages and with valves relieving the air bottle down from 3000 psi. The gage has been the most frequent discrepancy. - The only information regarding service life is that the new type gage appears to be more reliable.

040701

Dm. Shake D. M. Shake

D. M. Shake WKAFB-6ARS-90F DATE_ 6-27-60 NAME Roswell, N.M. Walker AFB STATION MODEL KC-135 FAS Air Bottle Control Valves ENCLOSURES Noted Above

FSR

FSR

FSR

6-7000

20/2.10 FIELD SERVICE REPORT BOEING AIRPLANE COMPANY

TO: ENGINEERING SERVICE DEPARTMENT SEATTLE X WICHITA |

ROUTING-

ORIGINAL

OFFICE BASE FILE

SUBJECT: FAS Air Bottle Control Valve

> Please be referred to your letter 6-7171-1-12560 dated June 15. 1960.

The subject valves are listed under the following Federal Stock

Kidde, Part # 840891, Federal Stock # 1650-611-5286 Bendix, Part # 38E13-5A, Federal Stock # 1650-512-1530 Bendix, Part # 38E13-6A, Federal Stock # 1AFI-1650-633-2239

The following information is based on the above listed Federal Stock Rumbers. Since January 1, 1960 the following quantity of the subject valves were issued to maintain the fleet and any transient simplanes (KC-135)

Kidde, Part # 840891 Bendix, Part # 38E13-3A Bendix, Part # 38E13-8A

The reason for the predominance of the Kidde valves is that most the crew-chiefs will not request and accept theher of the Bendix valves as so much difficulties are experienced with them. The majority of the difficulties consist of the valve leaking. To a much lesser degree some trouble is also experienced with the solenoid.

This far the information may make sense, however, as these valves are not repairable at this station they are to be sent to OCAMA for overhaul whenever they fail. In order to determine how many of each of these failed since January 1, 1960 first Air Force personnel and then the writer (as he did not believe it) checked the lists of rep mirable material sent out of Castle since January 1, 1960. These lists show only two Kidde valves and none of either of the Bendix valves. Even if one assumes that some of the valves withdrawn from supply were taken on TDY sirplanes as spares and replaced while the sirplane was away from Castle this cannot explain the 19 apparently missing valves. The writer is not able to explain this discrepancy.

FILE 0110701

Paul Ribanvi

CLASSIFIED T

REPORT NO.__ DATE June 20,1960 NAME Paul Ribanyf CAFB-ORE-131F STATION Castle AFB LOCATION | Merced California FAS Air Bottle Control Valve REFERENCES 6-7171-1-12560- 6-15-1960 ENCLOSURES ! None

> FSR FSR FSR

DEPT. SUBJECT FILE

BOEING AIRPLANE COMPANY

TO: ENGINEERING SERVICE DEPARTMENT
SEATTLE WICHITA Renton X

BJECT: FAS Air Bottle Ground Cart

CLASSIFIED UNCLASSIFIED TO

ROUTING

ORIGINAL DRS GA UND IMI Per ref (b) and (c) the 5 enclosed photos are sent to amplify information in ref (a) and for possible use in BFSN. Note that a relief valve adjusted to relieve at 3125 psi is installed on manifold. This particular view cracks at 3125 and reseats at 3000. The four 3/8 inch T18 on the manifold were used as two 1/4 inch crosses were not available. The two crosses would simplify the manifold considerably.

Craig El McCreary
Field Service Engineer

FED

OFFICE BASE FILE

.

SERVICE DEPT. SUBJECT FILE

File: C4070I CEM: jtm

THE CHO OF

Peters we I Base

NAME Craig E. McCreary REPORT NO. FAFB-92-106F DATE 6-20-60
STATION Pairchild AFB LOCATION Spokane, Washington
SUBJECT FAS Air B ttle Ground Cart MODEL KC-135
REFERENCES (a) FAFB-92-97F dtd 5/25/60 ENCLOSURES five photos of Ground Cart (2 sets)
(b) FAFB-92-99F dtd 6/14/60 (c) Memo from D.R.Seibel dtd 6/13/60 / C 2/4/6

BOEING AIRPLANE COMPANY

TO: ENGINEERING SERVICE DEPARTMENT SUBJECT: FAS AIR BOTTLE CONTROL VALVE

WICHITA Transport Division

CLASSIFIED T UNCLASSIFIED X

ROUTING

Reference: Memo 6-7171-1-12560 dated 15 June 60

ORIGINAL A reliability survey of the subject revealed that 24 valve and gage assemblies have been replaced since January. Fleet hours accumulated during this time period are 3035. Available records do not indicate which valve failed (Kidde 840891 or Bendix 38E13-3A). Pneudraulic Shop personnel do recall one occasion where 3 of the Bendix valves were installed new and relieved at air pressures of 2500 PBI and lower. Pneudraulic personnel feet that the Kidde valve is more reliable than the Bendix valve. However, the Bendix gage is considered more reliable than the Kidde gage. Typical discrepancies against the valve and gage assembly are:

- (1) Gage sticking, erratic or wrong 5 cases:
- (2) Valve leak at T-Handle 10 cases:
- (3) Relieves early 3 cases:
- (4) Leaks at gage 1 case.

Undersigned knows of at least two instances where fuel air starter compressors were changed based on readings from improperly operating FAS air bottle gages. It is considered mandatory at this activity to check the bottle gage against MC-1 compressor gage when servicing the bottle from a ground oart.

UBJECT FILE Fila No.

BAC 1264-R2

0407

Field Service Engineer

REPORT NO. GAFB-41-135F LOCATION Rome, New York

FSR

DATE 6-24-60

STATION Griffias AFB 4039 Strat Wing SUBJECT FAS Air Bottle Control Valve REFERENCES Noted Above

MODEL KC-135

ENCLOSURES

FSR

NAME Robert &. Tucker/bs

FSR FSR FSR

FSR

BOEING AIRPLANE COMPANY

TRANSPORT DIVISION

	SERVICE SECTION	U OPERATIONS	DEPT.
SUBJECT:	FAS AIR BOTTL	REPLY VALVE	KC-
		7	

ENGINEERING SERVICE SECTION

ENGINEERING SERVICE SECTION

135

CLASSIFIED

OFFICE BASE FILE

ROUTING: ORIGINAL

TO. SEATTLE DIVISION

Reference (a) letter requested a survey of the service record of the Bendix 38KIS-8A subject valve versus the old types Bendix 38E13-3A and Kidde 840891. The -8A valve is installed on airplanes 59-1443 and on.

This activity has no 59 airplanes. A spot check of several planes by the undersigned indicates that only the old types are installed. The -6A valve does not appear to be in supply channels as yet, so no comparison as to serviceability is available.

A check of records shows that three valves were changed in the past six months, P/N unknown,; one for leakage and two for electrical malfunction (no details available).

The undersigned believes that in addition to the above, several valves have been changed by crew chiefs on the line, no records are kept of these changes and details are difficult to obtain.

In general, the concensus is that the valves do not present a problem and that consumption is reasonable.

JCH: 11f

SERVICE UBJECT FILE

REPORT NO. WAFB-4050-101F 24 Jun 60 J. Christopher Huebner DATE NAME Chicopee Falls, Mass. Westover AFB LOCATION FAS Air Bottle Control Valve MODEL SUBJECT Ref. (a) Letter 6-7171-1-12560 **ENCLOSURES**

FSR

JUPPLEMENTARY SHEET

- G. Aircraft on routine training mission.
- H Twenty minutes after take-off the number 4 engine fire warning light came on. Engine was throttled back and after approximately two minutes was shutdown. Fire switch was actuated but light remained on. No visible evidence of fire landing was accomplished without incident.
- J. Lead repaired and reinstalled. System checked satisfactorily.

CONTRACTOR'S REPLY

. . .

Reference TAX noted that the above unsatisfactory condition had been caused by damage inflicted during removal and installation of cowling and putting suggested providing a protective cover for this detector and connecting wire.

The existing fire detector installation provides protective covering for all wiring except approximately one inch at the detector ettaching point. However, reasonable care is still required during installation and removal of engine cowling to avoid damage to the fire detector and other installations. Subject UR is the only report to the Contractor of damage to the detector wiring from installation and removal or cowling. Modification to provide added protection is not considered warranted at this time.

The above is considered to complete the Contractor's action on this project.

REPORT T 00731 (4)

HIS AIN BALLE BOEING SET THE WASH

DMB 26 1

RR RJEDSQ RJESBA RJWFNK RJWXBR RJWZJM RJWZNF

DE RJWZDMB 46

R 202103Z

FM OCAMA REP OFC AFPR BOEING SEATTLE WASH

TO RJESBA/MOAMA BROOKLEY AFB ALA

INFO RJEDSQ/AMC ASC WPAFB OHIO

RJEDSQ/WADD WPAFB OHIO

RJWFNK/OCAMA TINKER AFB OKLA

RJWXBR/CINC SAC OFFUTT AFB NEBR

RJWZJM/93BW CASTLE AFB CALIF

RJWZNFOTIG USAF NORTON AFB CALIF

AF GRNC

BT

UNCLAS FROM OCNCSQ-5-1-114-E ACTION FOR MOAMAMONNSA.

INFO FOR AMC ASC/LMSJ, WADD/WWZSK, OCAMA/OCNC, OCNSI & WWDPESC,
SAC/DM4B2 AND OTIG/AFCDZ-2, 932/DCM.

OUR OFFICE HAS RECEIVED AN INFORMATION COPY OF SUBJECT IM PROBLEM UNSATISFACTORY REPORT, WHICH WAS SUBMITTED TO YOUR ORGANIZATION FOR INVESTIGATION AND NECESSARY ACTION IN ACCORDANCE WITH TO 20-35D-54, PAGE 2-5, PARA 2-36, DATED 1 APR 62. IF RESULTS OF YOUR PRELIMINARY INVESTIGATION INDICATE THAT THE MALFUNCTION WAS ATTRIBUTED TO, OR ASSOCIATED WITH, AN INSTALLATION PROBLEM,

PAGE TWO RJWZDMB 46

REQUEST THIS OFFICE BE NOTIFIED IN ORDER TO PROCURE EXHIBIT, IF
REQUIRED, AND TAKE NECESSARY ACTION TO RESOLVE UNSATISFACTORY
CONDITION. OCAMA REPRESENTATIVE OFFICE IS AVAILABLE TO ASSIST IN
ANY PROBLEM AREA ENCOUNTERED

BT

20/2118Z JAN RJWZDMB

NNNNO

74-22 14

AMC AERONAUTICAL SYSTEMS CENTER UNITED STATES AIR FORCE WRIGHT-PATTERSON AIR FORCE BASE. OHIO

FEB 1 1 10 PM '61

LUBJ-1-502/File: R&D 7-2-3

CONTRACT ADM.

Sontract AF33(600)-41979, Model MS-135 Airplane, Engine Tachometer -Generator, Type GEU-7/A, ARRIVO 61-8732

Sceing Airplane Company Transport Division Renton, Washington

TARU: Air Force Plant Representative Boeing Airplane Company Seattle 24, Washington

Reference is made to the following:

Spineense Date

To Tooling Airplane Co. om! AF Blant hep.

Loeing letter 3-7210-12403 dated 27 October 1960.

KC-135 FILE DISTRIBUTION

KG BAHRENBURG

ROUTING

EE DIE

DD MASON H3 HIATT

KG BAHRENBURG ACTION HH HOWELT. RM MCRGAN WE MORTLOCK

WB DALRYMPLE

A_J/ASJ letter LLSJ-9-921 dated 30 September 1960.

The reference a. letter recommends that the change from 13-6 to GII-7/A type tachcmeter-generator be made effective on an either/or basis on all 10-135's from (30) AF56-3591 and on. This Denter concurs in the recommendation and approves the change by miscellaneous ECP to the Lodel Specification 1-15441 as stated in paragraph 3 of the reference a. letter. It should be noted, however, that the ARENO 61-6732, GW-7/4 tachometer-generator is equally suitable for the first 29 MO-135's for spares purposes.

File DCH EMP RUST

PLB

LHH MES

SUT

DWO

JBR

3. The reference b. letter authorized the change to the GEU-7/A tachometer generator effective with the 493rd production KC-135. The Original toletter also stated that the Contractor was authorized to reject any GEN-7/A's manufactured by Globe Industries on the basis that they were never qualified. Since that time Globe has incorporated several minor Copies to: improvements in their article and has incorporated BOP R-1 which stakes the stator to keep it from rotating. Although the Globe unit is not get on the Qualified Products List the improvements and modifications are expected to provide an acceptable article. The previous instructions to reject Globe units are therefore rescinded. The Contractor may accept Clobe GDI-7/A's for KO-135 installation provided the units have had BOP R-1 accomplished either in production or by retrofit.

4. Globe GEU-7/A tachometer generators which have been modified in ACT accordance with DUP-N-1 can be identified by the small hole which was wrilled in the case forward of the smalti-pin connector for insertion of the ball bearing that stakes the stator. Production units also have marking on the packaging, both individual and external packaging containing several units, indicating that EOP R-1 was incorporated.

A13107

00674

155

5. It is expected that Boeing will not normally receive Globe units for FY 64 production airplanes. The units delivered will probably be new procurement from one of the three qualified sources. However, it is possible that production quantities may include some Globe units if existing supplies preclude the necessity for new procurement. Some Globe units may also be delivered as spares.

FOR THE COLLIAIDER:

Edward L. Brady
EDWARD L. 1924-18
Lt. Colonal U. 48
Chief. To hear V 5292
Literature of Structure Systems

Copies to: SAC (DLZT) B-52/KC-135 CES, Castle AFB, Calif NAMIA (NATTSE) OSATA (COMU)

BOEMS STATTES, WASH

BH AØ 26GS A4 29 ZCZCGS A89 8 ZCQQC 54 2

PP RJWZDMB

DE RJEBHB 2

P 272345Z ZEX

FM 4242 STRATWG K I SAWYER AFB

INFO RJWFNK /OCAMA TINKER AFB

RJWZNF/OTIG NORTON AFB

RJWZDMB/AFPR BOEING SEATTLE WA H

BT

UNCLAS FROM DCMQC 0193.

IMMEDIATE ACTION REQUIRED. SUBJECT: SEMERGENCY UNSATISFACTORY

REPORT. SPECIAL HANDLING REQUIRED IN ACCORDANCE WITH SECTION

II, T.O. 00-35D-54.

A. 4042SW 61-1. CRITICAL SARTY HAZARD.

B. 186059 SERIAL NUMBER

C. 330403-21 MANOFACTURERS PART NO.

D. AJA4 FUEL CONTROL (BENDIX)

E. KC-135A 59-1497

F. NONE

FILE ENGLES FOR MEMORITORS

1621

HH

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UH

PAGE TWO RJEBHB 2

1189

G. FUEL NCTED LEAKING IN VICINITY OF THETDTER RESET AND MAX. ;033\$ -\$'\$6,8,8 978,88. IT APPEARS THAT PISTON RING SEAL-81 OR PREFERMED PACKING -82 AND -24 ARE DISCREPANT ALLOWING BCDY FUEL TO LEAK FAST INTO THE WATER RESET HOUSING -101 DISCIPING THROUGH VENZ HOLES IN THE HOUSING AND ARCUND SCJEW ASSYS -42 AND -43 THRU TUBES -39. T.O. REF. 6J3-4-13-63, FIG 2-20

- H. REMOVE AND REPLACED WITH LIKE ITEM.
- I. FLEET INSPECTION IS BEING MADE THIS DATE, YOU WILL BE ADVISED.
- J. THREE (3)
- K. RECOMMEND BETTER QUALITY CONTROL AND BENCH CHECK PROCEDURES.
- L. 355:45 HCURS
- M. EXHIBIT BEING HELD FOR DISPOSITION INSTRUCTION.
- N. JACK E. WILLIAMSON, TSGT., USAF, AF 14333211, 2571/DI 69844.

28/8200Z JAN RJEBHB

NNNNJZCZCDMA692

FEB BH A99 1 GS A4Ø 72C ZCGS A8 72ZCWQ BE 18 PP RJWZDMB ZDK KAC718 PP RJWFNH RJWFNK RJWZDMB RJWZNF RJEDSQ DE RJWBKA 16C P 2722407 ZEX FM 4136 STRATWG MINOT AFB NDAK TO RJWFNH/SAAMA KELLY AFB TEX INFO RJWZDMB/AFPR BOEING AIRPLANE COMPANY SEATTLE WASH RIFDSO /WADD WRIGHT PATTERSON AND CHIC RJWFNK/OCAMA TINKER AFB OKLA RJWZNF/USAF DIG NORTON AFB CALIF RJEDSQ/AMC WRIGHT PATTERSON AFB CHIO BT UNCLAS. DCM 6158. IMMEDIATE ACTION REQUIRED. EUR SUBMITTED IAW T.O. 00-35D-54. ACTION FOR: DM4 SAC, SANSI SAAMA. INFO FOR: CONSI OCAMA, OORSTE AFPR, B-52/KC-135 OES, USAF DIG DIR SAFETY/AFSCA-3, DM4 ALL AIR FORCES AND AIR DIVISIONS DCM AND PIP CONTROL ALL BOMB WINGS, STRAT WINGS AND REFUELING WINGS. A. CRITICAL SAFETY HAZARD. B. 4136SW-61-4 - 27 JAN 61. C. PUMP ASSY - FUEL TO 1C-135(K)A-06 CODE 23215 CLASS 2915.

D. PART NUMBER 0 22594-02 -01 SERIAL NUMBERS PE 247., 543, 2345,

PAGE TWO RJWBKA 16

2055, 2193. T.O. 6J10-4-52-4.

- E. PESCO PRODUCTS INC., BEDFORD, OHIO.
- F. J57-P-59W ENGINES. KC-135A AIRCRAFT 58-691, -698 AND -120.
- G. FIVE (5) WORN EXCESSIVELY. 25 JAN 61 TO 27 JAN 61.
- H. FIVE (5) SPECIAL INSPECTION. 25 JAN 61 TO 27 JAN 61.
- I. FIVE (5) REMOVE AND REPLACE. 25 JAN 61 TO 27 JAN 61.
- J. FIVE (5).
- K. TWENTH (20) MANHOURS.
- L. DURING COMPLIANCE WITH T.O. 1C-135(K)A-1051, DATED 23 JAN 61, IN THE PROCESS OF MEASURING SPLINES FOR WEAR, IT WAS EVIDENT THAT ALL SPLINES SHOWED SIGNS OF WEAR AND DRIVE SHAFT SPLINE, PART NUMBER 02-10969, T.O. 6J10-4-52-4, FIGURE 2, INDEX 28, WAS REMOVED FOR MEASURING. IT WAS THEN NOTED THAT EROSION HAS TAKEN PALCE ON THE BEARING, FRONT COVER DRIVE, PART NUMBER 02-11786, FIGURE 2-23, AND BEARING BODY DRIVEN GEAR, PART NUMBER 02-12278, FIGURE 2-29, T.O. 6J10-4-52-4. THIS EROSION AREA WAS FAR BEYOND THE SPECIFIED LIMITS CONTAINED IN T.O. 6J10-4-52-3. OPERATING TIME OF DEFECTIVE PUMPS IS FIVE HUNDRED AND SEVEN (507) HOURS AVERAGE. ONE (1) DEFECTIVE PUMP SERIAL NUMBER PE 2470 IS BEING HELD AS UR EXHIBIT.

PHOTOS WILL FOLLOW BY SEPARATE MAILM AFM 66-1 DATA IS NOT APPLICABLE



PAGE THREE RJWBKA 16 IN THIS CASE.

M. DUE TO THE POSSIBLITY OF SHORT SUPPLY OF PUMPS FROM SUPPLY SOURCES, AIRCRAFT COULD BE GROUNDED BECAUSE OF NON-COMPLIANCE WITH T.O. 1C-135(K)A-1051.

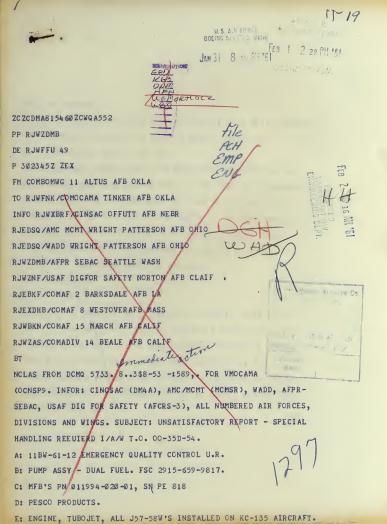
No RECOMMEND DISPOSITION INSTRUCTIONS BE FORWARDED ON EXHIBIT PUMP AND IMMEDIATE ACTION BE TAKEN TO PROVIDE A FIX.

O. KENNETH R SAMPLE, MSGT, 4136TH STRAT WING PIP CONTROL, EXT 5433 (DUTY) PA 7-3735 (NON DUTY).

BT

27/2240Z JAN RJWBKA

NNNN



PAGE TWO RJWFFU 49

F: SIX PUMPS RECEIVED FROM OCAMA THIS DATE WERE BEING INSPECTED FOR TOLERENCES OUTLINED IN INTERIM URGENT ACTION TOC 1C-135 (K)A-1051 DTD 23 JAN 61.

G: THE COUPLER, DRIVE SHAFT WAS MIKED AND INDECATED .9278.

T.O. 1C-135 (K)A-1051 STATES THAT IF THE COUPLING MEASUREMENT IS LESS THA .9355 INCH REPLACE THE PUMP ASSY. THE T.O.C. RECORD ON THE AF FORM 50B TAG ATTACHED TO THE PUMP INDICATED T.O.C.'S 1C-134(K)A-755 AND T.O.C. 1C-135(K)A-1051 WERE COMPLIED WITH. INSPECTOR'S NUMBER ON THE TAG WAS OMC 973.

DATE IN INSPECTION BLOCK 28 JAN 61.

H:OX IN ECTED 6

J: CDEFECTIVE 1

K: RECOMMEND THAT THE DEPOT FACILITY EVALUATE THEIR QUALITY CONTROL PROCEDURES AND TAKE THE NECESSARY CORRECTIVE ACTION TO PREVENT DEFECTIVE ITEMS FROM ENTERING SEVICEABLE STOCKS. FURTHER RECOMMEND THAT ALL SAC UNITS AFFECTED BY T.O.C. 1C-135(K)A-1051 COMPLETE THE INSPECTION REQUIRED BY SUBJECT T.O.C. REGARDLESS OF INFORMATION IN THE T.O.C. RECORD BLOCK OF THE AF FORM 50B.

PAGE THREE RJWFFU 49

L: NO OPERATING TIME SINCE OVERHAULED.

M: Preceve ITEM WILL BE HAND CARRIED TO OCAMA BY MAJOR JAY J.
BROWN 31 JAN 61.

N: DONALD L. RAYFIELD, TSGT, HQ 11BW, DUTY PHONE 351, HOME PHONE HE2-6238. .

BT

31/0030Z JAM RJWFFU

NNNNKZCZCDMA816

M

A

DE MOMENK 910

R 2021407

FM HO OCAMA TINKER AFB OKLA

TO AFPR BAC WICHITA KANS

P R 1007007

THE MAIRDIN WESTOVER AFE MASS TO EJESTA/HOAMA EROCKLEY AFE ALA

BITO RJEDSQ/AMC WPAFE OHIO

BJEDSOTVADD WPAFE OHIC

BJEFNK OCAMA TINKER AFE OKLA

TAMPKNIUSAF DIG FOR SAFETY HARCH AFE CALIF

EMCLAS 4050 DCMQ 0693 ACTION FOR MOUSA INFO FOR MOMT AND OCNSI OCAMA AFORS-3 USAF DIG FOR SAFETY BMA SAC BAF DMMI EUR SUBMITTED IAW TO

06+352-54 A MISSION FAILURE B 4050ARW 61-2 E FUEL AIR TARTLE KC-135/K/1-06/23411 D MFG

TW 541091F3 SH 240 E HAMILTON STANDARD F

KC-435 3636 & 10-IPEN SYSTEM WIRING 9-FAILURE TO

PERATE 5-IMPROPER OPERATION 3-1)893 1-INTERNAL

FAILURE 1-STALLS COMPRESSOR 1-NO OUTPUT 1-LOW

RESPONMENCE 2-MISFIRE 1-CRACKED DATA COLLECTED FROM



ENG

T Bosing Airplane Co. From: AF Flagt ... For: Act in Sent by Suspense Date

PAGE TWO LJWFNK 91C

JUN 60 THRE 15 JAN 61 H 33-BETWEEN FLTS - GROUND CREW 4-BOTWLEN FLTS. - AIRCREW - NO ABORT DATA COLLECTED FROM 1 JUN 60 THRU 15 JAN 61 I 23-REMOVED AND REPLACED 7-ADJUSTED ON AIRCRAFT 4-REPLACED SEAL GASKET OR PACKING 3 -SERVICED DATA COLLECTED FROM 1 JUN 60 THRU 15 JAN 61 J 37 K 138.0 L A TOTAL OF 23 UNITS WHICH FAILED REQUIRED REMOVAL AND REPLACEMENT OF THESE UNITS TEN HAD OPEN SYSTEM WIRING AND NINE FAILED TO SPERATE REFERENCE 4050 ARW UR 60-145 WHICH SHOWS BASIC TREMO OF FAILURES IN FUEL AIR STARTERS M PRECEDING INFORMATION AND REFERENCED UR PASED ON AIRCRAFT ON ALERT STATUS FAILING TO OPERATE PROPERLY AIRCRAFT 56-3636 WAS SUBJECT OF 40 50 ARW UR 60-145 FUEL AIR STARTER WHICH MALFUNCTIONED ON ALERT STATUS FUEL AIR STARTER WAS REPLACED ON 27 DEC 60 AIRCRAFT HAD TOTAL OF SIX ADDI-TIONAL HOURS AT TIME OF REPLACEMENT ON 1 JAN 61 FRE-BYENT RECENT FAILURES OF END ITEM ON ALERT AIRCRAFT MANY ME AD INESS REQUIREMENTS QUESTIONABLE N SUBJECT. FMEL AIR STARTER SN 240 BEING HELD AS UR EXHIBIT. PENSING DISPOSITION INSTRUCTIONS O MORRIS W L SR.

19. by ch 11 12 mm

FACE THREE RJUFFNK 91C

OKIAHOMA CITY AIR MATERIEL AREA
UNITED STATES AIR FORCE
COMM Representative Office
_/o Bosing Airplane Company
Spattle, Washington



ROUTING

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KC-135 FILE

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CO MOCRE WB PALRYMPLE

CCNCSO-1

17 Jenuary 1961

ECP DO-KC-135-4651-2, Contract AF34(601)-7785, KC-135 Aircraft, Revise Lubrication Harkings on Air Cyclo Nechine, Fuel Air Startor Compressor and Portable Air Compressor, MIP CCC-10548823.

OCAMA (CONSI) Timber AFB, Okla

1. Attached ressage number RESER-1-5-1100-18-1546 is forwarded for your information and action as deemed necessary.

2. Subject ECP was requested by COMMA to furnish material required by TCTO 10-15f(M)A-999. The above TOTO was propered by COMMA from T.O. Ites 221 and publication has been held in abovene pending procurement of the necessary materials. Call number E-61-00-99F has been issued and funds have been obligated and reserved as recommended in the attachment.

3. It is requested that this office be furnished 330 copies of TOTO 10-135(k)A-959 on or before 27 January 1961, per telecon between this office and CONTOA, for intertion into hits prior to shipment. Kits will be shipped as seen as possible efter 27 January 1961, but not later than 8 February 1961, to AFM 2033, Site E, Tinker AFB, Okla.

W. In view of the above, subject MIP is renumbered to 0000-10544R23K where it will remain until 20% of kit shipment is completed.

is SX

Copies to: Major, USAF
FILE OCAMA Reprosentative
ENG

To:	Boeing Airplane Co.	
From:	AF Plant Kep.	
For:	Action	
1	Reply	,
1	Info.	
	CSQ	
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DIS AIR FORCE BOEING SEATTLE, WASH

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RJEBKL/COMDR 4238STW BARKSDALE AFB LA
RJEDAA/COMDR MATS SCOTT AFB ILL
RJEDSQ/COMDR WADC WPAFB OHIO
RJEDSQ/COMDR AMC ASC WPAFB OHIO
RJESBH/COMDR 4228STW COLUMBUS AFB MISS
RJEXDH/COMDR 8AF WESTOVER AFB MASS
RJEXDH/COMDR 57AIRDIW WESTOVER AFB MASS
RJEZFF/COMDR 1801 ABWG ANDREWS AFB MD
RJEZFH/COMDR 42BW LORING AFB ME
RJWEKN/COMDR 15AF MARCH AFB CALIF
RJWFAP/COMDR 28BW ELLSWORTH AFB SDAK

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FOR TOWN AS TOWN

BKC

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65-1139-E

RJWFFU/COMDR 816 AIRDIV ALTUS AFB OKLA
RJWFFU/COMDR 11BW ALTUS AFB OKLA
RJWFGM/COMDR 4130 STW BERGSTROM AFR THY

RJWFBG/COMDR 816 AIRDIV BIGGS AFB TEX

RJWFDB/COMDR 4123SW CLINTON SHERMAN AFB OKLA

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RJWFJP/COMDR GBW WALKER AFB NMEX
RJWFNK/COMDR GCAMA TINKER AFB OKLA
RJWFNK/COMDR OCAMA TINKER AFB OKLA
RJWFNK/COMDR TBW CARSWELL AFB TEX
RJWFSK/COMDR 19AIRDIV CARSWELL AFB TEX
RJWXBR/COMDR 19AIRDIV CARSWELL AFB NEBR
RJWXBR/COMDR 19BW OFFUTT AFB NEBR
RJWZDL/COMDR 14AIRDIV TRAVIS AFB CALIF
RJWZGP/COMDR 92BW FAIRCHILD AFB WASH
RJWZJL/COMDR 413ASTW MATHER AFB CALIF
RJWZJM/COMDR 93BW CASTLE AFB CALIF
RJWZNF/OTIG USAF NORTON AFB CALIF
AF GRNC

BT

UNCLAS OCRST-6-5-1139-E FOR OCNSP, WCLOD-31C, DM4, LMSJ, WCOF, AFCDI-2, SALEK, PI CONTROL OFFICER; ALL AF, BW, AIRDIV, STW, ABWG AND ABW FOR DM. SUBJ: MIP OC9-18018E, HAMILTON-STANDARD FUEL AIR STARTERS, FAS-450-16-18-21-22, KC-135 ACFT. 1. THIS OFFICE RECEIVED EUR 6BW 59-40 CITING THE FAILURE OF FUEL AIR STARTER TO FUNCTION. THE SUBJ MIP WAS ESTABLISHED WITH CONTR AND VENDOR FOR INVESTIGATION AND FOR RECOMMENDED CORRECTIVE ACTION. THE FOL EUR'S WERE RECEIVED CITING VARIOUS DIFFICULTIES AND FWD TO THE CONTR AS REPEAT ON THE PREVIOUSLY ESTABLISHED PROJ: EUR'S SSN NRS 6BW 59-40, 6BW 59-86,

BW 59-183, 7BW 59-68, 7BW 59-81, 7BW 59-83, 7BW 59-136, 7BW 59-137, 11BW 59-50, 4130 SW 59-17, 4130 SW 59-25, 4228 SW 59-31, 4228 SW 59-65. 1881ABW-59-117. 3982 ABW 59-78. 2. INVESTIGATION REVEALED THAT MALFUNCTIONS REPORTED IN UR 6BW 59-48, 7BW 59-137 AND 11BW 59-50 OCCUPRED WITHIN THE STARTER ELECTRICAL CONTROL BOX. THE ONE UR EXHIBIT RECEIVED AT THE VENDOR'S FACILITY, APPLICABLE TO UR SSN 6BV 59-40, DASH 16 SER NR 11550, WAS TEST FIRED, AND FUNCTIONAL TESTS WERE PERFORMED SATISFACTORILY. THE EXACT CAUSE OF THE MALFUNCTION COULD NOT BE DETERMINED. HOWEVER, OTHER MALFUNCTIONS WITHIN THE STARTER ELECTRICAL CONTROL BOX RECEIVED AT THE CONTR WERE FOUND TO BE PDN DEFICIENCIES. THE VENDOR HAS INITIATED A MORE RIGID QUALITY CONTROL INSPECTION THAT WILL ELIMINATE THE MALFUNCTIONS DUE TO PDN DISCREPANCIES. A. UR 11BW 59-56 WAS RECEIVED AND DID NOT QUOTE STARTER SERIAL NR, OR THE AVAILABILITY OF THE EXHIBIT. HOWEVER. IT WAS ASSUMED THAT THE REPORTED FAILURE WAS ON ONE OF THE EARLIER MODIFIED DASH 22 STARTERS AND THAT NO CHANGES WERE MADE TO THE CONTROL BOX DURING MODIFICATION. 3. THE FOL UR WERE RECEIVED AND ARE APPLICABLE TO THE -21 AND -22 STARTERS: EUR SSN NR 6BW 59-86, 6BW 59-183, 7BW 59-56, 7BW 59-68, 7BW 59-81, 7BW 59-83, 4136 SW 59-17, 4228SW 59-31, 1001 ABW 59-117, 7BW 59-137 AND 4136 SW 59-221. A. INVESTIGATION OF THE ABOVE REPORTED FAILURES

6-5-1139-E

Ham - Std Starters,

PAGE THREE RUWKBF 28B

REVEALED THAT MALFUNCTIONS WERE CAUSED BY PRIMARY OR SECONDARY SWITCH FAILURES OR BOTH. THE TRIP-OUT OF THE SECONDARY SWITCH IS PRECEDED BY THE MALFUNCTION OF THE PRIMARY SWITCH UNLESS A PREAMATURE TRIP-OUT OCCURS. IN THE EVENT OF A TRIP-OUT, STARTER REMOVAL IS ROR. THUS CAUSING NUISANCE STARTER CHANGES. B. THE VENDOR HAS MADE RETROFIT CHANGES AT OVERHAUL EFFECTIVE AT STARTER SER NR 12711 AND ONE. THE SECONDARY SWITCH SETTING WAS INCREASED FROM 2700 PLUS OVER PINUS 186RPM TO 2986 PLUS OVER MINUS 186RPM TO MINIMIZE PREMATURE SECONDARY SWITCH ACTUATIONS /TRIP-OUTS/. C. AS ADDITIONAL INFO. THERE ARE TWO TYPES OF PRIMARY CENTRIFUGAL SWITCHES THAT HAVE BEEN USED INTERCHANCEABLY IN THE STARTERS. ONE MODEL OF THE SWITCH HAS A SOLID PIN TYPE ACTUATING BUTTON. IN SOME CASES THE PIN WAS MADE OF A SOFT MATERIAL WHICH WAS SUBJ TO WEAR THAT RESULTED IN A CHANGE TO THE CUT-OUT SPEED SETTINGS. THE OTHER TYPE SWITCH HAS A BALL AND SOCKET TYPE BUTTON WITH HARDENED SURFACES THAT ARE RESESTANT TO WEAR. THE LATTER TYPE IS INSTALLED IN ALL STARTERS EFFECTIVE AT SER NR 12852. AND ON. THE MANUFACTURER RECOMMENDED THAT ALL STARTERS BE CHANGED AT OVERHAUL TO THE BALL AND SOCKET TYPE SWITCH. THIS RECOMMENDATION WAS APPROVED AND IS BEING ACCOMPLISHED BY HAMILTON STANDARD ENGINEERING CHANGE 47911 WHICH REPLACES THE SWITCH AND BRACKET ASSY, PART NR 508581, WITH SWITCH AND BRACKET ASSY. PART NR 549530 AT TIME OF OVERHAUL. 4. UR 4130 SW 59-25 WAS INVESTIGATED AND IT WAS DETERMINED THAT THE STARTER MALFUNCTION WAS ATTRIBUTED TO FAILURE OF PRESSURE SWITCH. THE CONTR RECORDS

PAGE FOUR RUWKBF 28B

INDICATE THAT THIS IS THE ONLY MALFUNCTION OF THIS PART REPORTED TO BATE. THEREFORE, NO CORRECTIVE ACTION IS RECOMMENDED PENDING THE RECEIPT OF ADDITIONAL REPORTS. 5. UR 7BW 59-98 WAS INVESTIGATED AND IT WAS DETERMINED THAT THE MALFUNCTION WAS CAUSED BY BURNER PRESSURE SWITCH FAILURE. THIS SWITCH WAS REPLACED ON PDN ACFT BY PRR 4415. EFFECTIVE AF 57-1485 THROUGH AF57-1495, WITH AN OIL FILLED TYPE SWITCH. RETROFIT WAS ACCOMPLISHED AT HAMILTON-STANDARD CORP BY ECP 4415 DURING OVERHAUL. 6. UR 4228 SW 59-65 WAS INVESTIGATED AND IT WAS DETERMINED THAT STARTER FAILURE WAS CAUSED BY INTERNAL FAILURE OF THE GEAR TRAIN AND CASE. IT WAS ALSO DETERMINED, BASED ON INFO AVAILABLE, THAT THE STARTER UNIT ELECTRICAL SYSTEM HAD BEEN JUMPERED DURING AN ATTEMPTED PNEUMATIC START. THIS CAUSED THE UNIT TO OVERSPEED AND RESULTED IN FAILURE. 7. UR 3902 ABY 59-78 AND 42BW 59-110 HAVE UNDERGONE PRELIMINARY INVESTIGATIONS WHICH SHOW THAT NEITHER OF THESE STARTERS HAS BEEN MODIFIED TO THE LATEST CONFIGURATION BY THE CONTR OR THE COMMODITY AMA. 8. INVIEW OF THE FOREGOING EXPLANATION REGARDING THE ACTIONS THAT ARE BEING ACCOMPLISHED TO IMPROVE THE RELIABILITY OF ALL MODELS OF THE HAMILTON-STANDARD FAS-450 STARTER, THIS OFFICE FEELS THAT THE PFOJ CAN PROPERLY BE CLOSED. WITH THE EXCEPTION OF THE INSTALATION OF A NEW BURNER SECTION TO MODIFY THE -21 TO A -22 WHICH WAS DISAPPROVED

NECONOMICAL UNTIL THE -22 HAS BEEN GRANTED QUALIFICATION

APPROVAL BY THE AF. ALL STARTERS ARE BEING MODIFIED WITH ALL KNOWN

FIXES AS THEY PASS THROUGH THE PDN OR OVERHAUL FACILITY. ALSO

IT SHOULD BE NOTED THAT CONTINUING SURVEILLANCE OVER THE

FUEL-AIR STARTERSYSTEM RELIABILITY PROBLEM IS BEING MAINTAINED

THROUGH AN ACTION ITEM OF THE KC-135 WEAPONS PHASING GROUP. THEREFORE

THIS PROJECT IS BEING RENUMBERED TO PHASE 3 AND CLOSED. IN THE

EVENT FUTURE SERVICE REPORTS PROVIDE NEW RELIABILITY INFO ON THE

LATEST CONFIGURATIONS THESE FACTORS WILL BE SEPARATELY CONSIDERED

AT A LATER DATE

BT

29/21257 RUWKBF

NNNN

ner.

BOEING AIRPLANE COMPANY 235 American National Bidg. Oklahoma City, Skiekowa.

HH

WISH HOE GED WED

June 22, 1960 1-2400-4-1262

FILE OHOTE KE 135 LECIND

To:

D. R. Selbel

Subject:

FAS Air Bottle Control Valve, KC-135

Reference: 6

6-7171-1-12559 Dated June 13, 1960

Reference letter requested quantity and reason for overhaul of three versions of subject valve. The following information was furnished by OCAMA, Commodities Division:

Part Number

Quantity Overhauled

38E13-8A (Bendix) None - A quantity of these valves have been procured. Mobile AMA will control this item.

38E13-3A (Bendix) No record of procurement.

84891 (Kidde) From July 1, 1959 to date, a total quantity of 402 valves have been subject to overhaul. No record maintained prior to fiscal year 1960.

Shop personnel were contacted for the reason for overheul - their comment was as follows:

Presently, the attrition rate on the air pressure gage, Bendix Part Number 643897, Stock Number 6685-726-1908 is approximately 100-115%. A large percentage of valves returned for overhaul are found to operate satisfactorily but the air pressure gage is either inoperative or inaccurate. Physical inspection of the Part Number 643897 gauge shows it to be flimsy and subject to Part Number 643897 gauge shows it to be flimsy and subject to Brodon tube damage whenever jarred or subjected to rough handling. Effect of normal engine vibration is unknown, but "kid glove" handling is required during shipping, installation and normal maintenance. The "115%" failure rate is due to gage failure during functional pressure testing after valve overhaul. The overhaul T.0. was not checked for functional test air pressure

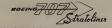
requirements; however, OCAMA shop personnel indicated the T.O. requirements were complied with. They indicated that two or three applications of the specified air pressure could result in gage failure. This problem was not encountered with the original MU.S.Gage Company aggs.

In cases when actual valve failure was found, due main reason was due to "9" ring enlargement. Evidently, oil from the F/A starter air compressor gets into the valve, causing the "9" ring to swell end bind the shuttle. Apparently two sources for the "9" ring have been used, both during initial installation and overheui. At present, only the "9" ring subject to enlargement is being furnished to the SCAMA shop. This is Part Number 62278-14, Stock Humber 600-589215-7, Menufactured by Stillman Rubber Company (sample attached). Following our discussion, OCAMA shop supervisory personnel indicated they would try to obtain the other "non-swelling" "9" ring. They didn't have a manufacturer, part number or stock number to go by as the man actually doing the overheul could identify the good "9" ring only by the color markings. He indicated that he would save samples of both types of "0" rings when aveilable from subsequent overhaul. These parts will be forwarded when available.

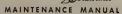
WJG/sp

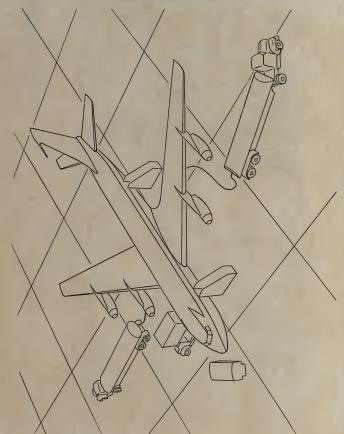
Attachment

W. J. Groseclose
Staff Representative
Engineering



SERVICING
Servicing General
Maintenance Practices





SERVICING Servicing General Maintenance Practices

6. Toilet Servicing

A. Forward and aft toilet drain panels are located on lower right side of fuselage. The forward toilet service drain panel is located at station 30%, right buttock line 45 and water line 165. The panel contains toilet sever drain, waste water drain, forward and aft flush connection, water waste value, and forward and aft sewage values. The aft toilet drain panel is located at body station 1413, buttock line zero, and water line 190 and contains a toilet sewage drain, left and right flush values, and left and right flush connection.

7. Water Servicing

- A. The forward water tank pressure filler and drain connection is located on left side of body station 357 at water line 154.
- B. Aft water tank filler and drain connection is located at body station 1265, water line 184. (See chapter 38-0.)
- C. The water injection tank for atrplanes equipped with JT3G-4 engines has a capacity of 450 U.S. gallons. The tank filler is located on outside of body near trailing edge of wing on left side. Provisions for installation of two additional tanks in aft wheel well area have been added to accommodate water injection demands for JT3G-6 engine installations. The additional tanks each have a capacity of 142 U.S. gallons, and are interconnected to main tank.

SERVICING

1. General

A. The design configuration of the 707 airplane provides for most major servicing to be accomplished on right side of <u>fuselage</u>. Passenger loading doors are located forward and aft on left side of fuselage to avoid interference during ground servicing activities.

2. Air Servicing

- A. Hydraulic Accumulators.
 - The utility, auxiliary, and brake hydraulic accumulators are located in the right wing trailing edge, just outboard of wheel well. Utility and auxiliary accumulators are air precharged to 2000 psi and the brake accumulator is air precharged to 1500 psi.

3. Fueling

- A. Pressure Fueling
 - A pressure fueling system is installed with two fuel adapters located on lower surface of each wing. Fueling control panels are located adjacent to adapters for manual operation and visual reference by a ground service operator. (See chapter 28-0.)

4. Hydraulic Fluid Servicing

- A. Hydraulic Tanks.
- A 7-gallon hydraulic supply reservoir is located in left wing trailing edge, outboard of wheel well and just aft of rear spar. In servicing, the reservoir is filled to the 5-5/8-gallon position to allow space for fluid expansion. If hydraulic system has been completely drained, 27 to 30-gallons of fluid will be required to service system. The 707-121 uses Skydrol 500 as an operating fluid.

5. Oxygen Servicing

- A. Oxygen System.
 - Oxygen system replenishment is accomplished by removal of four oxygen cylinders located overhead behind a drop ceiling panel between stations 1200 and 1200.
- B. Portable Oxygen Bottles.
 - Two portable oxygen bottles are located in forward clothes closet and two bottles are in aft closet.



CHAPTER 12

SERVICING

TABLE OF CONTENTS

Subject											Si	ubject No.
SERVICING - GENERAL .												12-1-0
ACCESS AND INSPECTION	OPENINGS.											12-2-0
CLEANING AND WASHING.												12-3-0

REQUIRED PLACARDS
Placards
Description and Operation



PLACARDS (MARKINGS) - DESCRIPTION AND OPERATION

1. General

A. Placards are placed on both, the interior and exterior of the airplane. Some of them give information as to what procedures to follow when servicing the airplane units. Some of them give a CAUTION or MARNING in places of potential damage or danger. Most of the larger placards on the exterior of the airplane are for identification. The insignia and exterior markings on the airplane are applied by silk screening, decals or stencils. The interior markings are applied by decals, metal-cals or stencils. Stencilng or silk screening that becomes damaged must be repaired. Decals and metal-cals that become damaged must be replaced. The application procedure for decals varies with the type of decal used and the location and type of surface to which it is applied. Care must be taken to clean the receiving surface thoroughly and use the proper application procedure.

END



CHAPTER 11

REQUIRED PLACARDS

TABLE OF CONTENTS

Subject	Subject No.
PLACARDS	 11-0

ICE AND RAIN PROTECTION
Engine and Nacelle Anti-icing Systems
Description and Operation



ENGINE AND NACELLE ANTI-ICING SYSTEMS - DESCRIPTION AND OPERATION

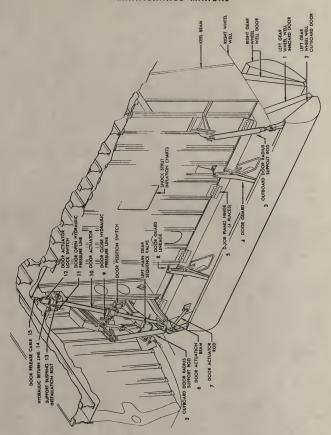
1. General

A. The engine nose cowl and engine inlet guide vanes are anti-iced by engine high pressure compressor bleed air. The air is ducted from the bleed port of each engine to the nose cowl and inlet guide vanes for that engine. Shutoff valves located in each supply line are controlled by an individual switch for each engine located on the pilots' overhead panel.

END

7. Landing Gear Retraction - Extension Actuators

- A. The landing gear retraction-extension system is provided with hydraulic piston type actuators for actuation and locking of the landing gear. The actuators are jdg located and have no adjustments. The head and piston rod terminals are equipped with self-aligning bearings with a lube fitting on terminal housing. The landing gear retraction-extension system actuators include: wheel well door actuators, landing gear actuators, landing gear actuators, landing gear actuators, main gear side strut actuator and nose gear lock retention actuator.
- B. Wheel Well Door Actuator
 - (1) Main Gear Door Actuator
 - (a) The main gear door actuator, figure 6, is located at forward inboard end of each main wheel well. The actuator receives hydraulic pressure from landing gear positioned door control valve. The actuator cylinder end is trunnion mounted to upper side of keel beam web. The actuator rod end is attached to a jig located non-adjustable actuator beam pivoted on keel beam. The actuator extends to open doors and retracts to close doors. The open or close cycle is completed in approximately one second with actuator bottoming at each end of actuation.



32-1-0 Page 10 Main Gear Door Actuator Figure 6

July 20/57



MAINTENANCE MANUAL

(b) The actuator lock mechanism, figure 7, consists of a lock shaft extending out through cylinder end of actuator to actuate "door locked" micro-switch and attached to door release cable from emergency extension shaft assembly and ground door release handle. The lock rod incorporates (on inner end) a pair of folding toggles which actuate two diametrically opposite bronze lock segment blocks. The blocks are supported in broached holes in a steel retainer cylinder and seat behind a flange on end of actuator piston rod, locking it in retracted "door closed" position. A compression spring and spring seat cylinder attached to lock rod by a lock ring loads lock rod towards locked position. System pressure applied at cylinder end of actuator (door open pressure) forces lock rod upward against return pressure and spring load. As rod moves up, toggles fold inward allowing piston to push lock segment blocks inward freeing actuator piston. As actuator piston extends (door opening) a spring loaded retainer segment follows piston to slide outside of lock segment blocks keeping them in for return of piston on retraction (door closing). As actuator extends, displaced fluid returns to hydraulic system by way of a restricted passage in piston rod bearing. Restriction of displaced fluid provides snubbing action to slow piston travel near end of stroke. With hydraulic pressure applied at rod end of actuator for door closing, the piston is retracted to contact spring loaded retainer segment pushing it back and sliding over lock segment blocks. With piston retracted (to bottomed position) and door closed, the spring loaded lock rod is pushed down causing toggles to expand, pushing lock segment blocks out to lock the actuator in retracted position. The lock balance port at cylinder end of actuator is designed to prevent return surge pressures in line to cylinder end of actuator piston from unlocking the door actuator.



3. CONTROL SURFACES

The state of the s	
Total Aileron Area AFT of Hinge Line	
Inboard Aileron, including 5.8 Square Feet of TAB area	39 Square Feet
Outboard Aileron, including 5.5 Square Feet of TAB area	80.6 Square Feet
TOTAL	119.6 Square Feet
Horizontal Tail Area Total	500 Square Feet
Stabilizer, to Elevator Hinge Line, including 60.9 Square Feet of Fuselage	382.7 Square Feet
Elevator AFT of Hinge Line including 18.0 Square Feet of total area	117.6 Square Feet
Span	39 Feet 8.4 Inches
Vertical Tail Area Total (not including Fin)	303.7 Square Feet
Dorsal Fin	8.7 Square Feet
Fin to Rudder Hinge Line including 4.9 Square Feet of Fin Tip Hinge Line	201.8 Square Feet
Rudder, AFT of Hinge Line including	101.9 Square Feet
Fin Height	38 Feet 4 Inches
BODY	
Length	138 Feet 10 Inches
Width	12 Feet 4 Inches

Cross Section Vertical Height....

14 Feet 2-1/2 Inches



5. LANDING GEAR

Tread, Main Gear	21 Feet 1 Inch
- ,	
Wheel Base, Nose to Main Gear	
Main Gear, Wheels and Tires	15.50 x 20
Nose Gear, Wheels and Tires	12.50 x 16



CHAPTER 7

LIFTING & SHORING

TABLE OF CONTENTS

Subject													170	Subject No	2.
AIRPLANE JACKING														7-1-1	

AIRPLANE JACKING

1. General

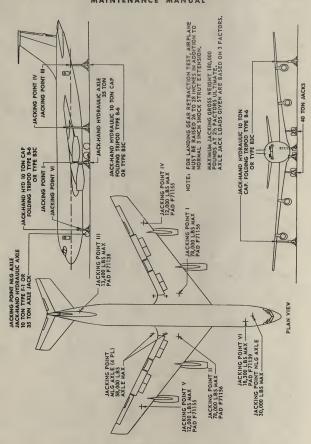
- A. The airplane is provided with three main jacking points and three stabilizing jacking points, (figure 201). The main jacking points are the two inboard wing jacking points I and II (limited to 78,000 pounds each) and the aft fuselage jacking point III (limited to 13,000 pounds). Main jacking points will collectively carry airplanes weighing up to 169,000 pounds. The stabilizing jacking points are the two outboard wing jacking points IV and V (limited to 12,000 pounds maximum, each), and the forward fuselage jacking point "VI" (limited to 18,000 pounds). In addition, there is a jack pad on under side of each main gear truck axle (limited to 58,000 pounds each) and a jack pad under nose gear axle (limited to 30,000 pounds).
- B. A preliminary figure for wind limitations for outside jacking has been established. The airplane shall not be raised on jacks in winds exceeding 35 miles per hour.

2. Jack Airplane

- A. Make sure all landing gear down locks are in place.
- B. Head airplane into the wind if in an exposed area. Lower vertical fin if airplane is to remain on jacks for an extended period of time or if winds are unstable.

CAUTION: DO NOT JACK AIRPLANE IF WINDS EXCEED 35 MILES PER HOUR.

- C. Install jack pads and position jacks per figure 201.
 - NOTE: Jacks must be equipped with pressure gages or a table used for converting pressure readings to pounds of load at jacking point.
- D. Remove wheel chocks and release parking brakes.



7-1-1 Page 202 Jacking Diagram
Figure 201 (Sheet 1 of 2)

May 20/57

AALE JACKS						
SOURCE	MODEL	CAPACITY	MINIMUM	HYDRAULIC	SCREW	BASE
SMITH NELSON CORP.	3510-51	35	10.5	11.0	9	A 6 5
	3510-53	35	10.0	10.0	9	12.0
REGENT	9938	25	7	10	m	5.5
	1905	2	10	12	4	, 9
	1921	35	10	77	9	9
	983-s	2	9	10.5	ď	٠,٠
	I-096	20	æ	13)-4	100
	1975	12	10	16	NOWE	30.01
TING INBOARD						10.5
EGENT	989A	100	96-82-09	1	1 91	
	2924		72		2 6	
SMITH NELSON CORP.	4060-14R	2	90-82-09	17	0 0	
	2060-10		2		2	
	-14 -15		96-82-09	Off	العرا	
MLABAR	780R	94	60-73	2	2 0	
ING OUTBOARD, BODY-FORW	ARD					
REGENT	B3C	20	52-77	04	15	
			88-106			
			124-142			

JACK PAD HEIGHT (APPR WITH 3 INCH SHOCK STRUT III

May 20/57

Jacking Diagram
Figure 201 (Sheet 2 of 2)

7-1-1 Page 203

LIFTING AND SHORING Airplane Jacking Maintenance Practices

- E. Use plumb-bob and leveling scale in left wheel well (figure 202) to establish level lateral and longitudinal attitude while raising airplane.
 - NOTE: This method of leveling is accurate enough for general jacking requirements and gear retraction only.
- F. Raise airplane in level attitude with jacks at wing jack pads "I" and "II" and tail jack pad "III" until landing gear clears ground.

CAUTION: JACKS AT PADS "I" AND "II" MIST BE RAISED PRIOR TO OR SIMULTANEOUSLY WITH JACK AT JACK PAD "III." RAISING TAIL JACK AREAD OF WING JACKS MAY OVERLOAD TAIL JACK POINT BY FORCING NOSE OF AIRPLANE DOWN ON NOSE GEAR OR NOSE STEADY-ING JACK.

Jack pad heights above ground, jack pad maximum allowable loads and a source of jacks to be used are listed below. Jack pad heights are based on a three lnch shock strut extension and no flat tires. Airplane must be raised an additional 26 to 28 inches (approximate) for landing gear extension check.

JACK POINT	APPROXIMATE JACK PAD HEIGHT	MAXIMUM ALLOWABLE LOAD
WING INBOARD	80 INCHES	78,000 POUNDS
WING OUTBOARD	136 INCHES	12,000 POUNDS
BODY - FORWARD	72 INCHES	18,300 POUNDS
BODY - AFT	124 INCHES	13,400 POUNDS



JACKS -- WING INBOARD

-SOURCE	MODEL	CAPACITY TONS	MINIMUM HEIGHT	HYDRAULIC LIFT	SCREW EXTENSION		
REGENT	989A	40	60-78-96	44	16		
4	2924	75	72	50	20		
SMITH- NELSON	4060-14R	40	60-78-96	1+14	18		
	5060-10,						
	-14, -15	50	60-78-96	40	16		
MALABAR	780R	40	60-73	40	18		
JACK WING OUTBOARD, BODY - FORWARD AND AFT							
REGENT	взс	20	52-70-88	40	15		
			106-124-142				

JACK PAD ADAPTERS

PART NUMBER

	260
F71138	Adapts Jack to fuselage aft jacking point "III."
F71139	Adapts Jack to fuselage Forward jacking point "VI."
F71155	Adapts Jack to outboard wing Jacking Points "IV" and "V."
F71156	Adapts Jack to Inboard Wing Jacking Points "I" and "II."

LIFTING AND SHORING
Airplane Jacking
Maintenance Practices

G. Raise outboard wing jacks "IV" and "V" and nose jack "VI" until sufficient weight is supported to steady airplane.

CAUTION: DO NOT EXCEED ALLOWABLE LOAD ON JACKS.

NOTE; Lower all jack ram lock nuts as jacks are raised. Maintain a clearance of one-inch from nut to collar until jacking is complete, then summ up nut and tighten lockscrew.

3. Lower Airplane

A. With jacks supporting airplane per figure 201, lower airplane by first lowering steadying jacks "IV," "V," and "VI" ahead of tail "III" and inboard wing jacks "I" and "II."

NOTE: To lower jacks, turn jack ram lock nuts up preceding jack collar by one-inch.

B. Lower main jacks "I," "II" and "III" evenly and simultaneously checking continuously to make sure main gear touch ground as soon as, or prior to nose gear, so tail jack point "III" is not overloaded.

CAUTION: IF A JACK "HANGS-UP," THE RAM IS NOT DROPPING INTO CYLINDER, DO NOT PRESENDE JACK COLLAR WITH JACK RAM LOCK NUT BY MORE THAN ONE INCH. "HANG-UP" CONDITION MAY BE RELIEVED BY RAISING AND THEN LOWERING JACK (WORKING JACK) UNTIL FREE. IF "HANG-UP" CONTINUES, IT MAY BE NECESSARY TO RAISE AND CRIB AIRPLANE, AND THEN REPLACE FAULTY JACK.

4. Axle Jacking

A. Jacking points are provided under each landing gear axle for removal of wheel and tire or brake assembly without raising entire airplane, see figure 201. Axle jack pad load allowables, height dimensions and jacks are listed below.

CAUTION: DO NOT RAISE EITHER END OF MAIN GRAR TRUCK TO EXCEED 15°.

DO NOT ATTEMPT TO JACK AIRPLANE WITH JACK UNDER CENTER OF MAIN GRAR TRUCK (UNDER SHOCK STRUT INNER CYLINDER FORK)
JACK PADS ARE NOT PROVIDED UNDER FORK OF SHOCK STRUT INNER CYLINDER.

AXLE JACK PAD HEIGHT CLEARANCE BETWEEN TIRES

CONDITION	NLG	MLG	NLG	MLG
NO TIRE FLAT ONE TIRE FLAT TWO TIRES FLAT ON ONE AXLE JACK PAD HEIGHT REQUIRED FOR WHEEL CHANGE	13.1" 10.2" 7.50	14.4" 11.0" 6.0	11.5"	18.5"
	16.6	18.4		

MAXIMUM LOAD AT A SINGLE JACK PAD NLG - 30,000 POUNDS

MLG - 58,000 POUNDS

JACKS:

SOURCE	MODEL	TONS TONS	MINIMUM	HYDRAULIC LIFT	SCREW EXTENSION	BASE WIDTH
REGENT	993R 1905 1921 983-S 960-T 1975	25" 25 35 5 10	7" 10 10 6 8	12" 18 11 10.5 13	3" 4 6 3 4	5.5" 6 6 5.5 7.8
SMITH- NELSON CORPS.	3510-51 3510-53	35 35	10.5	16 11.0 10	NONE 6 6	6.5 12.0

6. Jack Airplane With Collapsed Gear

- A. Nose Gear Collapsed
 - Raise airplane by using a 40-ton jack at each inboard wing jack pad,
 "T," and "II." Do not exceed 78,000 pounds on each inboard wing
 jack.
 - (2) Crib forward fuselage as airplane is raised by wing inboard jacks.
 - (3) Follow fuselage aft jack pad down with a Regent Model B3C jack. Do not exceed a load of 13,400 pounds on fuselage aft jack pad.
 - (4) If airplane is to be moved without using nose gear, use flat bed truck (capacity 20,000 pounds) under fuselage forward section. Tow airplane using two tractors attached by cable to main gear towing lugs. Coordinate movement of tractors and truck.

LIFTING AND SHORING
Airplane Jacking
Maintenance Practices

MAINTENANCE MANUAL

B. One Main Gear Collapsed

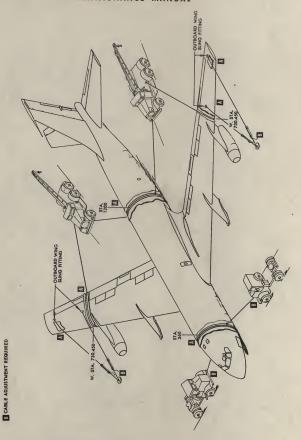
- (1) Place pneumatic bag, 1130, 1D-988 or equivalent under lower wing surface between front and rear spars (in area of wing inboard jack pad) but clear of jack pad so when airplane is raised sufficiently a jack can be inserted to finish raising procedure, see figure 204.
 - NOTE: Trucks or tractors attached to airplane by anchor lines must be used to keep airplane from rolling on pneumatic bags, see figure 203 and paragraph "D" below. Wood cribbage should be used under fuselage and wing structure to ensure against bag collapse or any slippage. Pneumatic bags may be inflated with a type A-1 (3.5 psi) blower or a Worthington air compressor or by air-nitrogen bottles, used with a regulator for inflation control.

C. Both Main Gear Collapsed

- Place pneumatic bags under wing lower surface between spars (clear of wing inboard jack pads), see figure 204.
- (2) Anchor airplane by anchor lines fastened to trucks or tractors to prevent airplane from rolling on air bags. (See figure 203 and paragraph "D").
- (3) Raise airplane by inflating pneumatic bags until jacks can be used on wing inboard jack pads and fuselage aft jack pad. As airplane is raised, crib wing and fuselage with wood timbers. Do not exceed jack pad maximum allowable loads, figure 201.
- D. Moor Airplane for Pneumatic Bag Raising
 - The airplane is not equipped with mooring or tie-down provisions.
 For emergency mooring and for mooring while using pneumatic air bags for raising airplane, see figure 203 and following instructions.
 - a. Wrap heavy padding around fuselage at station 360.
 - b. Wrap cable around fuselage over padding and directly over fuselage production break (approximately station 360 bulkhead) and attach cables to anchor stakes or heavy truck or tractor.
 - NOTE: Anchor cables must be attached to anchor in such manner to facilitate letting-out or taking-in of cable as airplane is raised or lowered.
 - Attach similar padding and cable at fuselage production break (approximately station 1200) and outboard wing to inboard wing production break.
 - d. Attach mooring fittings to outboard wing hoist sling attachment points and attach mooring cables to be secured to anchors forward of wing.

NOTE

| PROVIDE PADDING FOR ALL CABLE ATTACHMENTS
| TO AIRCRAFT



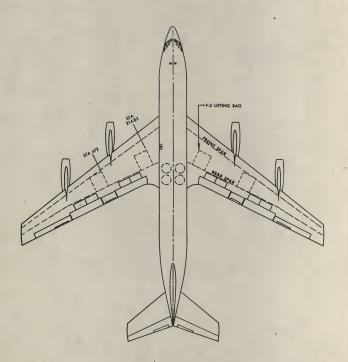
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Airplane Mooring for Pneumatic Bag Raising Figure 202

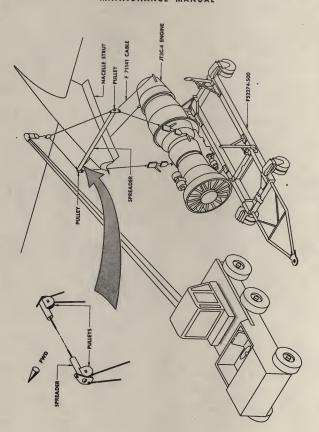
7-1-1 Page 209



LIFTING AND SHORING
Airplane Jacking
Maintenance Practices



Pneumatic Bag Placement Under Wing Figure 203



May 20/57

Engine Installation Hoisting Equipment Figure 204

7-1-1 Page 211



CHAPTER 8

LEVELING & WEIGHING

TABLE OF CONTENTS

Subje	ect	2																					2	Subject No.
LEVELING	•	٠	•		٠	٠	٠	٠	٠	٠	•	٠	٠	٠	•	•		٠		٠	•	٠	•	8-1-1
WEIGHING				•						٠			٠					٠	٠					8-2-1



LEVELING

1. General

A. The airplane must be level to permit an alignment check of airplane structure following hard landings and following structural repair or modification. The airplane must also be leveled for jacking to prevent side loads from being applied on jacks or pads, see figure 201.

2. Level Airplane

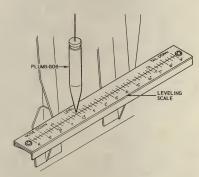
- A. Park airplane on level site (or approximately level).
- B. Place main and stabilizing jacks in position and jack airplane until wheels clear ground.

NOTE: Do not load stabilizing jacks.

- C. Attach plumb-bob to hook above leveling provision scale in left wheel well, see figure 201, so plumb-bob just clears scale.
- D. Adjust main jacks until plumb-bob is centered fore and aft and laterally on scale to indicate airplane is level.

CAUTION: DO NOT OVERLOAD JACK PADS. BRING STABILIZING JACKS UP JUST FNOIGH TO LOAD THEM FOR STABILIZING.





WEIGHING

1. General

A. The airplane is weighed after any modification work in which units have been deleted or added to the airplane to affect a change in center of gravity location. Weighing is required for gross weight computation and center of gravity location.

2. Tools and Equipment Required

Cox and Stevens electric weighing unit (or equivalent).

3. Weigh Airplane

A. Place a weighing cell on each of main jacks positioned under wing inboard jack positions and under fuselage aft jack position, figure 201. See also 7-1-1, figure 201.

CAUTION: AIRPLANE MUST BE LEVEL AND JACKS ALIGNED TO PREVENT SIDE LOADS ON WRIGHING CELLS.

- B. Locate kit on a stand convenient for connecting to weighing cells on tacks.
- C. Connect indicating unit to operating electrical power source and allow tube filaments to warm up to operating temperature for approximately 45 minutes.

CAUTION: FOLLOW OPERATING INSTRUCTIONS FURNISHED WITH WEIGHING KIT FOR PROPER VOLTAGE AND POLARITY.

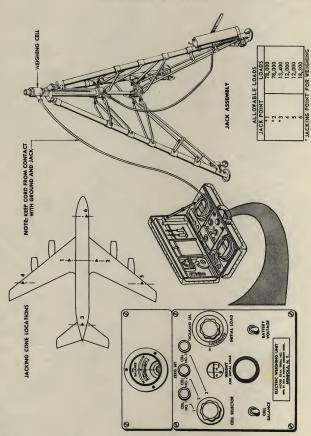
- D. Adjust indicators to zero setting for each weighing cell.
- E. Jack airplane by operating each jack simultaneously to keep airframe in level attitude as checked by leveling scale and plumb-bob in left main wheel vell.

CAUTION: OBSERVE JACK PRESSURE GAGES TO AVOID EXCEEDING LOAD LIMITATIONS ON JACK PADS. See 7-1-1, figure 201.

- F. When all tires clear ground, weighing cell load values may be read and recorded.
- G. Lower and reweigh airplane with weighing cells interchanged to check weight and accuracy of weighing cells.



LEVELING AND WEIGHING
Weighing
Maintenance Practices



END 8-2-1 Page 202 Weighing Equipment Figure 201

May 20/57



CHAPTER 9

TAXIING & TOWING

TABLE OF CONTENTS

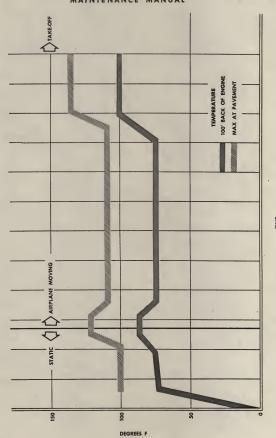
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TAXIING	٠	•	٠	٠	•	•	٠	•	•	•	٠	•	•	•	٠	•	•	•	•	•	•	•	•	•		•	9-1-1
TOWING																											9-2-1



TAXIING

1. General

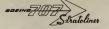
- A. Taxing of the airplane is no more difficult than taxing any of large passenger airplanes presently in use. The main difference is that the swept wing configuration places wing tip farther back from pilot's line of sight which creates illusion of less span than that of straight wing airplane.
- B. The 138-foot 10-inch fuselage configuration actually gives an overall length of 143-feet 9-inches from nose tip to elevator trailing tip. Overall span is 130-feet 10-inches.
- C. The maximum taxi steering turning radius of nose gear is 58° on either side of center or a total of 116° turning angle.
- D. It is anticipated that majority of maneuvering at terminals will require no more than 80% thrust and this power would be required only to start a static loaded airplane rolling with nose gear turned from center.
- E. The basis for engine run-up areas may be determined from information in figures 201, 202, 203, 204 and 205.
- F. In regard to foreign object damage picked up through engine (compressor) intakes, every effort should be made to maintain clean parking, taxtway and runup areas. This may be accomplished by cross sweeping with conventional sweepers or by use of heavy duty commercial vacuum cleaners. Studies made by NACA indicate that vortices, generated at engine inlet during some power conditions, may be capable of lifting foreign objects from concrete expansion joints or other ramp irregularities. Ingestion of some objects could cause severe engine damage.



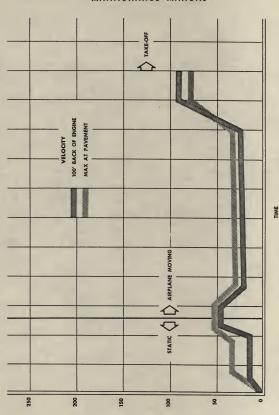
9-1-1 Page 202 Typical Operating Temperature Figure 201

May 20/57

TAXIING AND TOWING Taxiing Maintenance Practices

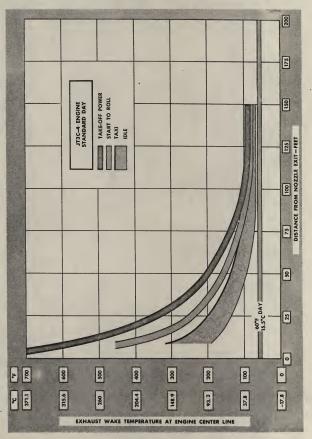


MAINTENANCE MANUAL



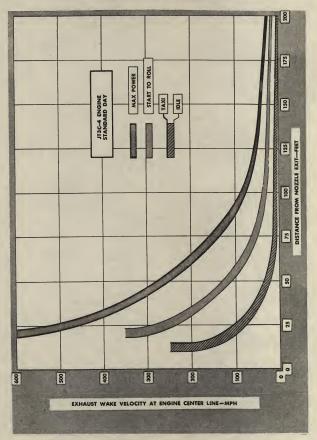
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Typical Operating Velocities Figure 202 D 6-1198



9-1-1 Page 204 Jet Exhaust Temperature Figure 203

May 20/57



May 20/57

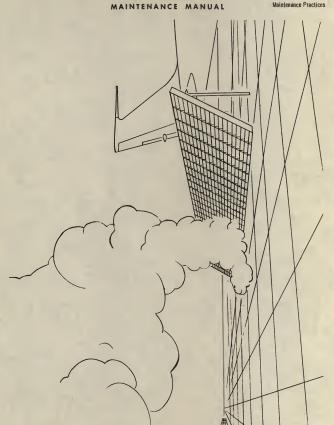
Jet Exhaust Velocities Figure 204

9-1-1 Page 205 Stratoliner

TAXIING AND TOWING

Taxiing

Maintenance Practices



END 9-1-1 Page 206 Blast Fence Figure 205

May 20/57



TOWING

1. General

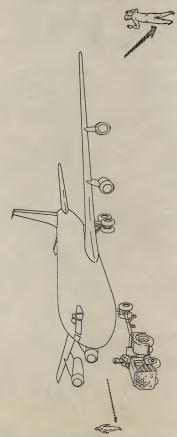
- A. A towing lug is provided on forward part of nose gear strut to which a tow bar can be attached. The lug is designed to attach to a tow bar which consists of a single 8" tube approximately 2! feet long and supported by two wheels when not attached to airplane. The bar connects to airplane with a single pin fitting and is used for towing, pushing and steering the airplane by using a standard type tug tractor.
- B. Under towing conditions, the nose gear wheels must not be turned more than 58° on either side of center. If a sharper turn is desired, the nose gear torsion link pin may be disconnected, allowing nose gear wheels to rotate within 180°. Under this condition, the airplane can be turned within a 72-foot 8-inch radius or a minimum overall diameter of 156 feet. Without torsion link pin disconnected from steering collar, a maximum 58° turn would require a 101 foot radius or an overall turn diameter of 202 feet.
- C. Towing lugs are also provided on forward and aft ends of each main gear truck for attachment of towing cables to aid in moving an airplane mired in snow or mud.
- D. The tow load design for nose gear for pulling or pushing is 37,000 pounds. For each main gear, design tow load is 28,000 pounds. The draw bar load required to handle the airplane at 250,000 pounds gross weight on a 3% grade is 12,500 pounds. The torsional force required to rotate nose wheel with airplane in static condition on a dry concrete ramp is 60,000 inch-pounds maximum.



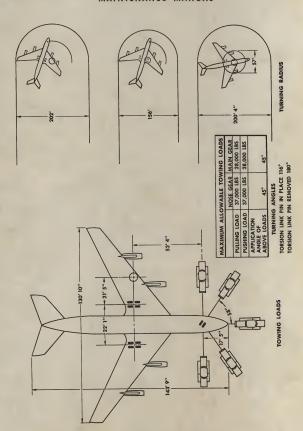
TAXIING AND TOWING

Towing

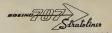
Maintenance Practices



Typical Towing Arrangement Figure 201

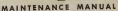


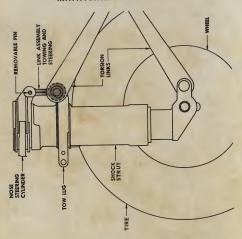
Towing Loads and Turning Radius Figure 202



TAXIING AND TOWING Towing Maintenance Practices

REMOVABLE PIN AND LINK NOSE WHEEL STEERING





BAR ASSEMBLY
AIRPLANE PUSHING AND TOWING

END 9-2-1 Page 204

FOR TOWING, PUSHING AND STEERING THE AIRPLANE USING STANDARD TUGS.

DESCRIPTIONS USAGEs

SINGLE 8 INCH TUBE APPROXIMATELY 21 FEET LONG SUBPORTED, WHEN AN CONNECTED TO THE AIRPLANE, BY TWO WHEELS, A LUNETTE EYE ATTACHES TO THE TUG, A DOUBLE PIN FITTING ATTACHES TO A REPLACEABLE COLLAR ON THE SHOCK STRUT.

Towing Bar Attachments Figure 203

D 6-1198

May 20/57

BUEING AIRPLANE COMPANY TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT



On postflight inspection - found spark ignitor ROUTING (PN 313092) seized to electrical lead (PN PO-160116). Believed due to overtorquing and lack of lubication

- 1. On a routine training mission. Engine ignition was used for approximately
- 2. In inspection in accordance with 2 AF Twx, DMAA-3738, the spark igniter (P/N 313092, T.O. 2J-J57-54, figure 50, indix 24) was found to be seized to electrical lead (P/N 10-16011, T.C. 2J-J57-54, figure 52, index 19).
- 3. Spark igniter (P/N 313092) and electrical lead (P/N 10-1600116) were

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BOEING AIRPLANE COMPANY

FAILURE OR UNSATISFACTORY REPORT

Therefore of the Control of the Cont	Committee of the commit	19 N (HON REAR MIG
		33115 PART N/	BRACKET 365
PRATWHIT 7	7445 CARSWELL 29	A,C SERIAL 436 A C HOURS	N DATE FAILED D 12 8
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PART SERIAL NUMBER	REF CAT. NO. 23 -J57-54 FIG. NO. 7 INDEX NO. 2	78W-58-204	OTHER REF.
REMARKS. Include background, symptoms, correct	tive action, recommendations, or sketch, length of	delay or turnback	

ROUTING

During periodic - three ignition unit war mounting brackets were found cracked at the top aft and,

Cause - excessive vibration EXTRACTED DIRECTLY FROM UR

1. 100 hr. post flight was in progress.

- 2. While pulling 200 hr post flight, it was discovered that those ignition unit mount brackets were cracked at top aft end.
- 3. It is believed that excessive vibration is causing brackets to break.
- 4. Part was put on order see and broken brackets will be replaced as soon as possible.
- 5. Recommend using more durable material.

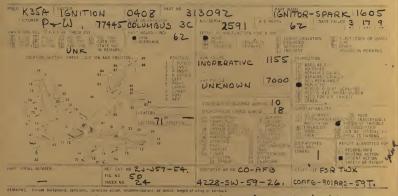
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BAC 3590 (P)

BOEING AIRPLANE COMPANY TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT



On poetflight inspection - found sparke ignitor PAW P/N 313092) (made by B.G. Corp). completely inoperative - apparently an internal failure. Removed and replaced. EXTRACTED DIRECTLY FROM UR

On a routine training mission, engine ignition was used for approximately twenty minutes, continual usage.

On inspection after landing, in accordance with 2AF TWX, DMAA-3738, the spark igniter, P/N 313092. Figure 50, index 24, T.O. 2J-J59-54, was found to be completely inoperative.

Spark igniter, P/N 313092, was removed and replaced with like serviceable item. System checked out satisfactory.

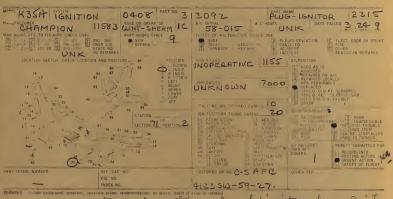
ALYSIS

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BOEING AIRPLANE GOMPANY TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT



en acceptance inspection - found I guitar plug - P. inde. #2 engine - inspective. Slight consision found on plug. Possible internal failure.

EXTRACTED DIRECTLY FROM UR

- 1. Acceptance check was in progress.
- During visual inspection, spark lightor right side no. 2 engine was found to be slightly corroded. Ignitor did not seem to fire during buzz check. Ignitor did not fire during visual check with power on.
- 3. Removed and replaced with a like serviceable item.

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BUEING AIRPLANE COMPANY TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT

The second section of the second					
K35A SYSTEMULTION	0408 PART NO 2	65015	COIL	-IGNITIO	N 0620
MANUFACTURER P&W 774	45 COLUMBUS 3C	A/C SERIAL 1505	ACH KS	4 DATE FAI	10 4 2 9
MAN HOURS REQ TO FIX AIRP CHECK NE	NO PAST HEIR INCE			HT DEVIATION F	FILE ODOR OR SMORE THE R REASON IN REMARK.
LOCATION SKETCH CHECK LEGATION AND	86 7 88 1 L 0U a 0 2 L INB 3 87 3 R INB 0	INOPERATIVE	1155	O SPIL THON TO USED AS 15 12 AUTO TED 17, REPAIRED ON 7	
13 13 14 83 15 15 15 15 15 15 15 15 15 15 15 15 15	4 R 0.1B 0 5 FFT 6 R (GP1 UPPI R 48 9 LOWER 9 FORE	UNKNOWN	7000	A REPAIRED LO A N REPAIRANT HAPT ED HELD OUT PE	RAPPEI Fr FR
71 24 30 33 46 31 31 31 31 31 31 31 31 31 31 31 31 31	2 87 87 AFT	MACHINETING TO BE US	NG 18	O' OTHER CANDIA VALUETY	
3 4 7 3 61	95 SECTI N 71 P T N		A A CONTROL AND THE STATE OF TH	H STATE	1 POOR 5 ILAC E LES 1 TRIBLE 10 AVE LEM 14 BE INSTAL (0
43 11 12	13 13	1 FEE 0. 1 SIDE NG 09 TAKE FF 1 F 1 MB	FEE COPECI N	CO FATELLE F THIS RPT TOVERS	RETURN SUBMITTED FOR
PART STRIAL NUMBER RE	74	12 LRUGE 14	LUKAS WA	07.150.015 T 1.3	SAFETH OF FLIGHT
	F CAT. NO 2J-J57-54 G. NO 50	CUSTOMER UR NO CO F		OTHER REF TW.	
CONTRACTOR	0EX NO. 15	901 ARS - 59 -	-33,	COAFB-90	IARS-74T.
REMARKS Include background, symptoms, corrective	action, recommendations or sketch, length of	relay or turnback.			

On postflight - found ignition coil inoperative.
Possible cause was extended use of ignition system
beyond design limits, in secondarie with existing
AF regulations.

EXTRACTED DIRECTLY FROM UR

- 1. On routine training mission, engine ignition was used for approximately thirty minutes.
- 2. After landing the ignition system was inspected IAW 2 AF TMX DM 4A-3738. The outboard ignition unit, P/N 10-94109-1A, figure 50, item 15, T C. 24-457-54, was found to be inoperative. Possible cause of failure is the extended use of ignition system beyond designed limits. This is a sealed unit and is beyond our capability of investigation.
- 3. Unit remove ${\ensuremath{\text{d}}}$ and replaced with like serviceable item.

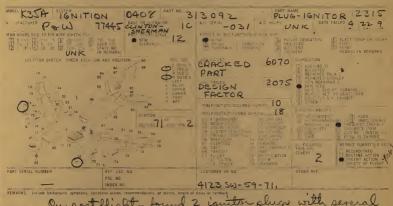
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FAILURE OR UNSATISFACTORY REPORT



On postflight-found 2 ignitor pluge with several cracks in the exposed ceranic section. Ottributed to orcubest resulting from prolonged ignition use.

EXTRACTED DIRECTLY FROM UR

- 1. Post flight was in progress in accordance with T.O. 10-135A-6.
- 2. Visual inspection of the exposed ceramic section revealed several cracks.
- 3. Removed and replaced with a like serviceable i em.

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BOEING AIRPLANE GOMPAN

FAILURE OR UNSATISFACTORY REPORT



On postflight found LH ignitor plug #4 engine cracked appears, 12 inch around upper flange. Operated 36 minutes on last flight.

EXTRACTED DIRECTLY FROM UR

- 1. Aircraft ignitor plugs being inspected during after flight inspection.
- 2. Inspection of plug from no. 4 combustion charber on no. 4 engine was found cracked approximately one-half inch around upper flange: Ignitor plug operated for a total time of 36 minutes during last flight.
- 3. Defective plug removed and replaced with a like serviceable item.

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BOEING AIRPLANE COMPANY TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT



On postflight-found one ignition unit moperate Ignition was 'ON' for 35 minutes on last flight,

EXTRACTED DIRECTLY FROM UR

- 1. Ignition unit was used thirty-five (35) minutes during flight.
- 2. Unit was ground checked after flight and found defective.
- 3. Removed and replaced with serviceable like item.

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BOEING AIRPLANE COMPAN) TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT



In flight - #1 engine ignition curent breaker tripped and could not be reset. On postflight-found ignition unit inoperative. Unknown internal failure.

EXTRACTED DIRECTLY FROM UR

- In flight on routine training mission.
- 2. Observed that no. 1 engine ignition circuit breaker on switch D-C bus panel hand opened. A no. of attempts were made to reset the circuit breaker but it would not remain the the close position. After flight investigation by audible and visual check, revealed that right hand ignition unit failed to operate.
- Replaced ignition unit and difficulty corrected.

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BOEING AIRPLANE COMPANY TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT



On postflight - #3 engine water pump impeller housing was found cracked 270 degrees around the circumfernice.

Cause - unknown EXTRACTED DIRECTLY FROM UR

- 1. Afterflight inspection following 8 hours flight and wet take-off during which water injection appeared to function nermally.
- 2. water pump impeller housing. The crack extended approximately 270° around the circumference.
- 3. Exhibit parts being replaced.

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(OFFICE)

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1/14/9 DATE :...21648

BAC 3590 (9)

ROUTING

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BOEING AIRPLANE COMPANY TRANSPORT DIVISION

K35A SYSTEM INJECT 0411 PART NO T	T 118600 -1 WAT	FER PUMP 2340
MANUFACTURER THOMPSON 59875 BASE OR OPERATOR 61	AC SERIAL 3606 A C HOURS	KN DATE FAILED N 10 8
MAN HOURS REQ TO FIX AIRP CHECK ONE 0 -12 72 21 - 5 72 - 11 9 250 510 3 - 1 13 - 5 10 20 8 100 200 8 0VER 50 1 2 2 5 10 20 8 100 200 10 NERMARKS	ID DELAY ENTH N CAN	F ED FIRE O MER TO REMARK
LOCATION SKETCH CHECK LOCATION AND POSITION 89 POSITION 89 POSITION 89 1 E-11/25 POS	BLADES 4015 BINDING	CLEPONITION (ILLU FD AS ILLU ZA ANDERED 3. HEPAIRED ON A/S 4. REI AIRED LOCAL Y
13 5 LEFT 19 88 6 RIGHT 7 UPPL 8 1 LOWER 9 FORE 9 FORE 19 AFT 19	FAILURE OF 1106 COMPONENT PART	E WIN REPAIRABLE REPLACED PLPL COLO PT S RAPPED HEPL D RET TO VIPE MFR HELD F UR FXHIBIT
172 39 33 15 0 APT 172 16 STATION 70 SECTION 71 POLITICISM	MALE MOTO CONTROL 24 MALE MOTO MIND DURI G 18 FASTI ATTI	TA FANABLITY AND THE ARM AND THE TRANSPORTERS BUT THE TRANSPORTER TO
12 16 31 33 32 34	STAF No. 0 FERLAD	GOOD LAN BE HISTALLED FREQ IS (WRONG
43 11 12 14 14 15 15 15 62 71 4 72 71 71 74	DE TAXELEF STATE TO THE TOTAL TOTAL TOTAL TO THE TOTAL TO	REPORT SUBMITTED FOR RECORD/INFO ROUTINE ACTION ROUTINE ACTION SAFETY OF FLIGHT
PART SERIAL NUMBER PP-830 A REF. CAT. NO10 FIG. NO. 4-24 INDEX NO. 90	1 LUSTOMER UR NO. LAFB 42 BW-58-2300	OTHER REF.

BOUTING

On postflight - the water pump blades were noted binding.

Cause - leaving failure

- Aircraft undergoing postflight inspection.
- Pump blades hard to move and blades binding.
- Bearing failure.
- 4. Removed and replaced with serviceable pump. Defective item turned into supply for disposition and repair.
- 5. Manufacturer be advised and necessary action be taken to preclude future failures.

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(OFFICE) SIGNATURE KO HENZERT

BOEING AIRPLANE COMPANY TRANSPORT DIVISION FAILURE OF INVESTORY DEPORT

FAILURE OR UNSATISFACTORY REPORT

F-CI CVLICH	· · · · · · · · · · · · · · · · ·		IR SHUTOFF
WAN HOURS REQ TO FIX AIRP WHECK WE	115CT 0411 PART NO 11982 BASE OR OPERATOR 61		AME VALVE 3400 JATE FAILED 9 29 8
1	NEW DERHAUL	PARKS A ST	AT DEVIATION OF FIRST OF ROTE OF THE STATE O
19 17 62	66 68 68 68 68 68 68 68 68 68 68 68 68 6	INOPERATIVE	DISP TION 1 U ED AS ID 2 ADJUTED REPAIRE DOWN A 4 PEPAIRE LOVELIN
13 34 81 15 5 7 32 71 74 7 30 33 46	48 81 9 FUE 9 AFT	CIRCUIT 2060 POOR	THE REST OF THE
On 14	93 TATION 3 SETTION 71 POSITION 3 16 31 33 32 34	TALL TO UND OUT TO AFF TO DE TO AFF TO DE TO AFF TO DE TO AFF TO	TANTERAS.III THE ALL Y TANTER BLE ALL THE TA
6 11 12 14 15 12 14 15 12 12 12 12 12 12 12 12 12 12 12 12 12	1/2 - 17 18 13 13	TOTAL ING CONTROL OF TAXABLE IN T	AN BE INSTALLED FRO TO TO TWO THE FOR PEPUT - BUTTLE FOR ROTTLE ACTION THE GETT ACTION
PART ITRIAL NUMBER	REF CAT. NO/0 FIG. NO. 4-24 INDEX ND. /03	12 CRUTE : INANAMAN CISTOMER UR NO LAFB 42 BW-58-1630	OTHER REF.
REMARKS. Include background, symptoms, correct	tive action, recommendations, or sketch, length of	delay or turmback	

POUTING DEP

SRJ

RT

LH

IBM

SERVICE ANALYSIS FILE PRUS 12/10 During routine shock - #3 engine air shut-

Cause - bad electrical connection.

EXTRACTED DIRECTLY FROM UR

- 1. Routine water injection sheek.
- 2. During routine water injection check, valve part no 1650-628-2988 on no. 3 engine failed to operate.
 - 3. Electrical connection bad, valve would not open.
- 4. Valve removed and replaced with like serviceable item. Defective item being held for disposition instructions.
- 5 Rec mmend a teardown and study be made $-\xi$ item to determine cause of failure.

(OFFICE)

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HOEING AIRPLANE GOMPANY

FAILURE OR UNSATISFACTORY REPORT

FN6	TIMONE ON ONDATIO	EAS										
MODEL K33 A SYSTEM STARTER D. ACTURER CORNELUS 14650 BASS	407 PART NO 130 R 2101-1 E OR OPERATOR C3 A. U SERIAL 497	A C HOURS DATE FAILED 6 49										
	NEW 148 ENT OF MALEUNTIN	GTH N CAN SEED DEVIATION TO LECT OO H OF INCKE										
6 10 12 10 13 15 15 15 15 15 15 15 15 15 15 15 15 15	## 1	1037 DISPOSITION 10 MIN AS 15 MI										
130 -21728 REF CAT. NO. 1/22 INDEX NO. 2	1C-135(K)H-7 CUSTOMER UR NO 2 5- 7811/59-	- 226										
REMARKS. Include background, symptoms, corrective action, recommi	endations, or sketch, length of delay or turnback.											

ROUTING

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WEBRE

DURING POSTFLICHT INSPECTICA CIBATAILPED -RESET, AND TELEPED AGAIN. OIL FLOWD DIS-COLORED TO A DARK DROWN. SUSPECT OIL STARVATION OR SURPLIAT. OIL EXTRACT DIRECTLY FROM UR.

1. On postflight \underline{t} spection the circuit breakers on the fuel air starter compressor were out.

2. The circuit brewers were reset and they apped again. Upon inspection the coapressor was find to be frezen up. The cil quantity was checked and found to e fully serviced. The cil was listed red to a dark brown. The cil was checked for the fully to the cilculations.

3. James of exclunction , where α , oil storvation or excessive heat caused the malfunction.

4. Compressor was replaced with serviceable compress., system was checked and open ted normal. The defeative compressor was turned into regular supply channels for repair.

5. Recommend that test be run on the lubricating system on the compressors to determine if the lubrication is at fault.

RLS 6/30

(OFFICE)

SIGNATURE D. H. Wilson

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BAC 3580 (P)

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FAILURE OR UNSATISFACTORY REPORT BUTTERPLY AIR SETTING OF A THE CONTROL O

BUEING AIRPLANE COMPANY

Valve sperated normally until circuit
breaker popped, Resets were unsuccessful.
Cause - internal short within the valve

LATRACO DIRECTIA FROM UR

- Valve operated negually until circuit breaker popped. Circuit breaker has reset several times and would not when anti-icing valve switch was actuated.
- 2. Internal short within the valve actuator.
- Unknown.
- 4. Removed and replaced with serviceable item Delective item turned into supply.
- 5. Continued evaluation of this unit be made to perfect reliability of this valve.

(OFFICE)

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ROUTING

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FAILURE OR UNSATISFACTORY REPORT

BOEING AIRPLANE COMPANY TRANSPORT DIVISION



ROUTING

During postflight - found WI injection control assy on #3 angent with an upper mounting flinge broken below the mounting hele.

- 1. Aircraft was undergoing a routine postflight inspection.
- 2. During the postflight inspection it was discovered that the upper mounting flange was broken below the mounting hole of no. 3 engine's water injection control valve.
- 3. Overtorque of mount bolt, misalignment, or engine heat expansion.
- 4. Broken control assembly was removed and replaced with a like serviceable item. Broken item held as UR exhibit.
- 5. A possible change in the torque requirement table for the upper mounting flange or manufacture control out of better material.
- 6, Copy of this UR 'c be forwarded to JFRC, BAC, Seattle 14, Washington.

(OFFICE)

SIGNATURE KO Henzler

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BAC 3590 (P)

BOEING AIRPLANE COMPANY TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT



Operation "quick switch" - water injection pumps bracket was found exacked upon amoval of water pump,

- 1. Engine received in shops for Project Quick Switch.
- When water pump was removed, it was noted that subject Support Bracket. P/N 69-8900, was cracked. (See enclosed Photo Mr 2640F).
- 3. Unknown. This bracket is a replacement for bracket that had failed previously, and was manufactured as a stronger replacement for 56 series.
- 4. Replaced with like serviceable item.
- 5. Recommend that an investigation be conducted to determine if this is an isolated case, or failures are still being encountered.

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ROUTING

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BOEING AIRPLANE GOMPANY TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT

MODEL (35 A STATION TRAINED TOWN TO THE ABOVE THE PROBLEM TO THE ABOVE THE	FNG	TAILO	IL OII ONSAIISI ACIONI	REPORT
LOCATION SECTION AND POSITION 89 POSITION	FACTURER BENDIX MAN HOURS REQ TO FIX AIRP CHECK ONE) Do 1 1 217 5 2 2 1 1 2 1 1 2 1 1 1 2 1 1 1 1 1 1 1	77820 G.C./F/153 80 250 SDO OVER STATE HOURS SINCE 1/2 STATE HOURS SINCE 1/2	I FINE F MALFUNCTION CHECK ONE	DATE EALLED 6 18 9
FIG NO. 52	9 77 34 32 33 34 34 34 34 34 34 34 34 34 34 34 34	64 97 9 98 9 99 99 99 99 99 99 99 99 99 99 99	MACTERNATURE TOWN MACTERNATURE OF COUNTY DURING WAS PROMOTION OF THE COUNTY DURING 10 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	LUCY TIME A 15 ALOUTED ON A. THE PROPERTY OF
REMARKS: Include background, symptoms, corrective action, recommendations, or sketch; length of delay or turnback.	PART SERIAL NUMBER 45947	FIG NO. 52 INDEX NO /	4039-5W-59-163	OTHER REF.

ROUTING
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MOH
IBM

DURING FUNCTIONAR TEST OF IGNITION 5/3.

ICNITION PLUG IN NO. 5 CAN FAILED TO FIRE.

INVESTIGATION DISCROSED IGNITION UNIT 18HD.

UNIT REPORTS HEAR AS UR EXHIBIT.

- Postflight inspection in progress.
- 2. During functional test of the immittion system in accordance with T.O. 135 (K)A-24-Parayraph bay, it was noted that the igniter plug mounted in number five burner can mailed to fire. Further investigation and inspection disclosed that the ignition unit 1/h 10-106700-10 was defective. At the present time monities are not available for been elected that unit.
- Unknown.
- 4. Defective ignition unit replaced with like serviceable item. This action corrected the difficulty. Subject item being held for disposition instructions.
- 5. Due to the fact that the subject item is of the latest configuration, recommend a study be conducted on the exhibit item to determine the exact cause of failure.

(OFFICE)

SIGNATURE D. H. Wilson

s. Fur 19256

ENGINE		AIR FRONT TUBE						
K35A ANTI-ICE	BASE OR OPERATOR I .	1822/3 PART N	GASKET 1360					
MAN HOURS SEQ TO F.X. ATRP HELS THE	77445 CARSWELL A FART HOURS NOT 116 VER 10 VER 10 VER 10 VER 116 VER 1	EL DE A LENGTH A CLEAR	Deviation E FLET GOOD AF					
LOUATION SKEICH CHECK LOLATION	N AND POSITION . 69 86 - 88	BLOWN	T AS IL T A DE CON A C T REVAIRED LOCALLY					
13 34 8 15 32 32 71 74 30 1, 33	85 6 RICHT 7 UPPER 8 LOWER 9 FORE 9 AFT	PRESSURE.	TO SEPARABLE VE ALL LE DOID PT CHAPPE LE DOID PT CHAPPE LE TO SERVER EXCHAPTE TO SERVER TO S					
0	61 16 31 33 32 34	A CASTO ELECTION AND ADDRESS OF A CASTO ADDRESS OF A CASTO AND ADDRESS OF A CASTO AND ADDRESS OF A CASTO AND ADDRESS OF A CASTO ADDRESS OF A CASTO ADDRESS OF A CASTO AND ADDRESS OF A CASTO A	AC E > 2.111 1.5 AC E 1.5 AC					
\$ 11 12 14 62 71-5.	14 15 13	12 Roll E 13 CONNONN	REFORM THE RECORDING TO POPULINE ACTION TO LINGENT ACTION TO SAFETY OF FLIGHT					
PART SERIAL NUMBER	REF CAT. NO 2J-J57-54 FIG. NO. 66 INDEX NO. 4	18W-58-222	OTHER PEF.					
REMARKS: Include background, symptoms, corre		be unti-ining an	in brond tube					

gaskets on engines #1 and #3 were found blown.

Course - Excessive heat and pressure EXTRACTED DIRECTLY ARCM UR

- 1. 160 | turn to tflight inspection was in progress.
- 2. During the inspection of the number three and number one engines, the following anti-icing gaskets were found blown:
 - a. 62-5-.8-0=641-7370, left and right side. b. 0245-2840-041-0910, left and right side.
- 3. Excessive heat and pressure.
- 4. Removed blown maskets and replaced them with serviceable like item.
- 5. Use more durable materials.

(OFFICE)

BIGNATURE KO /Krezler DATE

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BAC 3890 (P)

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BUEING AIRPLANE CUMPANY TRANSPORT DIVISION FAILURE OR UNSATISFACTORY REPORT

FAILURE OR UNSATISFACTORY REPORT
BUTTERFLY AIR

K35A ANTI- ICI	ING DAID	119165 SHU	TOFF VALVE 3400
WHITTAKER 7	9550 LOPPING 61		IKN DATE FAILED 9 23 8
	PART RS INCE SER ST ATE NO REMARKS	E PELAY LIMITH AV	T EVIATION E LE DOUR OR TOKE OFF D DE FLAS. N REMARKS
LOCATION SKETCH CHECK SATION 19 17 13 13 13 14 13 15 14 13 13 14 15 15 15 15 15 15 15	86 88 1 1 2 18 0 2 18 0 4 87 3 8 18 0 4 8 0018 0 5 LEFT	INTERMITTENT 4168 INTERMITTENT 4168 OPERATION WIN 14160 8 UNK NOWN	DISPLANTION IT INSPIRATE THE PROPERTY OF THE
12 12 12 12 13 16 17 17 18 18 18 18 18 18 18 18 18 18 18 18 18	10 93 STATION TO 10 10 10 10 10 10 10 10 10 10 10 10 10	The second of th	CONTROL OF THE CONTRO
PART SERIAL NUMBER	REF CAT. NO 23-J57-54 FIG NO. 65 INDEX NO. 9	1 USTOMER UR NO LAFB 428W-58-1494	OTHER REF
REMARKS: Include background, symptoms, correc	tive action, recommendations, or sketch, length of	delay or turnback.	

ROUTING At prive

at periodic - butterfly shutoff valve operated intermittently.

Couse - unknown

1. Airor ft undergoing periodic inspection.

- 2. Butterfly won't ower te properly butterfly open tes intermittently.
- Inknown.
- 4. Lentwed and replaced with like serviceable stem. (1d valve turned into supply for disposition.
- 5. Recommend manufacture be advised of this condition and take necessary action.

SERVICE ANALYSIS FILE

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HA BOEING AIRPLANE COMPANY TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT

ACTURE BCADIX OBST STATION ACTURE BCADIX OACTURE OACTURE BCADIX OACTURE O	EN6	INE	AJA4			
DO 3 - 1 2 -	ACTURER BENDIX	POWER 0405	A.C. SERIAL A.C. HOURS	VEL CONTROL 0680		
O COURT OF THE PROPERTY OF THE	图 2 2 5 图 2 50	OVER OVERHALL	TONE SENGIA 1 STA	F FUET OD R OR STOKE FOR STATE OF STATE ENT. REAL N IN REMARKS		
181838 FIG. NO. 110EX NO. 4/23 5 W 59-148	10 10 10 10 10 10 10 10 10 10 10 10 10 1	53 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	REGULATION Improved any failed 7000 UNK MALEURCHON GRINNS FRUND DURING 18 CONTROL OF STAND DURING 18 CONTROL OF STAND OF STAND 19 CONTROL OF STAND	A TALLER OF A 15 STANDARD OF A 15 STANDA		
	PART SERIAL NUMBER		CUSTOMER UR NO.	OTHER PEF		
	181838 REMARKS. Include background symptoms	Section for the second section of the contract				

WHILE ENTER ING TRAFFIC PATTERN NO. 1 ENG. 9UT. GROUND CHECK REVEALED ENG. O.K. UP to 85% - then would shut ITSELF DOWN.

SUSPECT FAILURE OF PT4 SENSING SYSTEM .
EXTRACTED DIRECTLY FROM UR

- 1. ACFT was entering traffic pattern after completion of flight.
- 2. Filet reported that the no 1 engine failed in pattern. Loss of EPR, RPN, cll pressure, and fuel flow. Ground run revealed that engine operation was CK to eight-five percent, at that point the engine shut itself down.
- 3. The AJA4 fuel control, $\rm S/N$ 181838 was replaced with a like SVC item. Engine checked out CK with new AJA4.

SERVICE ANALYSIS FILE

ROUTING

(OFFICE)

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DATE 6/18/9 SHT 1 OF /

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BOEING AIRPLANE COMPANY TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT



lu postflight-found one ignition unit inoperatire.

Janition was 'ON' for 20 minutes on last flight.

EXTRACTED DIRECTLY FROM UR

- 1. Ignition unit was used twenty minutes inflight.
- 2. Unit was pround checked after flight and found defective.
- 3. Removed and replaced with serviceable like item.

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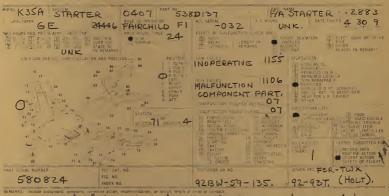
R.C. Shurn

5/4/0

s.AF) UP 23436

BOEING AIRPLANE COMPANY TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT



On starting attempt - F/A starter was inoperative. Found pins A, B and C of burner presence switch shorted together. Failure coursed a ground about of a scheduled mission.

EXTRACTED DEFECTLY JUNIUR

- 1. ACFT scheduled for 1730 take-off 1 headstart roman 2, mission. Unable to start no. 4 engine due to starter being inoperative. ACFT aborted.
- 2. Inspection of starter revealed that the turner pressure switch P/N 733B377Pl had shorted so that continuit, was obtained between all pins in the cancer $pl_{\rm eff}$.
- Defective ctarter reduced with a "arillen Glandard starter Stock No. 2995-033-4827, Defective starter will be repaired locally and returned to service as secon as recessary carts are received.

OFFICE RL Sintres.

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BOEING AIRPLANE GOMPANY

FAILURE OR UNSATISFACTORY REPORT

T/IT						
K35A STARTER	0407 PART NO 136	0RZ101-1-5 CON	PRESSOR 640			
CORNELIUS 14	-650 CASTLE C4		50 DATE FAILED 3 19 9			
2 -2125 0-20 B 10-20 SA	PART HOURS SINCE 210 NEW OVERHAUL TE NO REMARKS	DI HELAY LENGTH V CAN	CHT DEVIATION F ELLT DOOR OR S KE FLEED DOOR OR S K			
LOCATION SKETCH—CHECK LOCATION A	ND POSITION . 89 POSITION 1 L OUTB'D 2 L INB'D 1 R INB D	SEIZED 5285	DISPO-ITION II LSEO AS IS 22 ADJULTED 13 REPAIRE ON ALC 4 REPAIRE ON ALC			
13 13 32 49	85 7 LEFT 6 RIGHT 7 UPPER 8 LOAER 9 FORK 0 AFT	MALEUN TIM OCCURED DURING 10	NEM REPAIRAB E NEM REPAIRAB E REPLICED REPLICATION REPLICATION REPLICATION REPLICATION REPLICATION OF THE MINISTRUCT NEW MARKET ALL NEW METALL NEW MARKET NEW M			
71 16 - 61	95 STATION SECTION 74 PUSITION 4	VALFUNCTION FOUND DURING 18	WALLTA WABLETY FROMAT SEA Y S INAD ES BLE ACT SBLETY T NU SANCE ITEM			
4 12 13 12 12 14 15 14 17 14 17 14 17 15 16 17 17 18 18 18 18 18 18 18 18 18 18 18 18 18	30 32 34 30 17 37 19 4 15 13	104. SYSTEM FEW-ITOMAL 16. LANDING GROUND PERATN. 2 INSTITUTION 16. PRETIGHT 1 PROSTLY 16. STARTING 15 PERIOD 17.	AIR GAY BE INFEAL ED AIR GEREQ IS WANNE OF FAMILIES THIS FOT COVERS COVERS COVERS CAN BE INFEAL ED GREQUE S SWANNE RECORD/HED RE			
	REF CAT. NO. FIG NO.	CUSTOMER UR NO. CAFTS	OTHER REF FSR TWX			
	INDEX NO.	93BW-59-143.	OES-56T.			
REMARKS: Include background, symptoms, corrective action, recommendations, or sketch, length of delay or turnbock						

compressor circuit breakers and could not be reset. In postflightfound compressor served.

- 1. Juring after flight inspection.
- 2. The congressor circuit breakers were found in the open position. The circuit treaters were reset but immediately tripped Further investigation revealed that compressor could not be rotated by applying pressure to the fan blades.
- 3. Cause undetermined, possibly seizure of cylinders.
- 4. Desective compressor replaced and difficulty corrected. Compressor being held for Cornelius representatives inspection and disposition instructions.
- 5. That a study and analysis be made on exhibit compressor under MIP project CC9-10C11U1 to determine exact cause for failure and initiate corrective action as required.

POUTING

s. (F) UP 22225

SHT 1 OF

BOEING AIRPLANE COMPANY TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT

The second second second		HIR BOTILE			
	START 0407 PART NO.	840891 PART N.	AME YALVE 3400		
	83612 CASTLE C4	A/6 LERIAL 05 4. A C HOURS 5	O DATE FAILED 6 18 9		
WAN HOURS REQ TO FIX AIRV CHE K ONE 10 0- 12 3 2: 5 0 20 50 50 12 1 212 5 10 -20 8 100 - WK	PAR* HOURS SINCE SO VERY VERY UNITARIES NO. 1 VERHAUL	TURNHOCK REMARKS A AC	SHI LEVIATION T ELEC DOWN OR SMOKE FIFE FIFE D SHAREN N REMARKS		
19 17 13 15 32	ON AND POSITION. 89 P. FITON 49 - LIFS 0 50 - 10 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	INCRECED 1155 INCRECED 545 INV FAILED 7000	TOURS THAN FOR SER A WARED A HARROOM : HERAIRED ON A L WARED SERVICE SERVEL REPLACED TO BENEFILMER REPLACED TO BENEFILMER		
30 33 31 31 31 31 32 32 32 32 32 32 32 32 32 32 32 32 32	95 92 0 AFT 95 STATION 96 SECTION 70 Prosition 97 98 98 99 99 99 99 99	MALFUNCTION FOUND DURING 24 MALFUNCTION FOUND DURING 24 L FABBULGATIVE 3 AGREET DELANCES APPOACH APPOACH LANGUAGE APPOACH LANGUAGE AND SPRAIN LANGUAGE AND LANGUAGE AND SPRAIN LANGUAGE AND LANGUAG	HELD FOR U.S. EXHIBIT OTHER TO THE TO THE TO THE TO THE TOTAL TO THE T		
	71 €	0	ALR STEEL TOWNONG ALUMES THE RECORDINED FOR ROUTINE ACTION PROBLEM ACTION SAFET FILIGHT		
ART SERIAL NUMBER 986	REF CAT. NO. FIG. NO. INDEX NO	93 BW-59-283	THER REF. FSR		
EMARKS. Include background, symptoms, cor	rective action, recommendations, or sketch, length of		TWX -065-111T		

ROUTING

FO

BA

DURING ATTEMPTED START ON NO. 4 ENG. UNABLE TO
TO OBTAIN AIR TO FUEL AIR STARTER. SUSPECT
INTERNAL FAMURE OF VALVE ASSY. PREVENTING
FLOW OF AIR FROM STOCAGE BOTTLE TO STARTER
DSSY.

EXTRACTED DIRECTLY FROM UR

- $1-\lambda t_{\rm total} \, tin\,$ to start no 4 engine in preparation for routine training mission.
- 2. Unable to obtain air to fuel air starter.
- 3. Valve and obl. replaced and corretionally checked satisfactorily.

SERVICE ANALYSIS FILE

RC3

D. H. Wilson

s. Dur 19191

DATE 6/23/9 SHT 1 OF /

BAC 3590 (P)

6-70

MA

BOEING AIRPLANE GOMPANY TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT



ROUTING BFO RDF MOH DURING PREFLIGHT ATTEMPTED START, STARTER WOULD CUT-OUT AT 8%. FURTHER INSPECTION REVEALED CONTROL UNIT PIN 16800-14 HAD AN INTERNAL OPEN SELONDARY CIRCUIT.

EXTRACTED DIRECTLY FROM U

- 1. System operated a smally on last flight. On the nextpreflight a start was attempted on so, 4 engine and engine failed to start.
- 2. Further inspection revealed starter would cut out at 8 per cent.
- befortive starter was removed and replaced with a serviceable starter cambalized from nC-13%, ACFT 57-1444, subject aircraft starter operated satisfactory.

SERVICE ANALYSIS FILE

RLS

(OFFICE)

D. H. Wilson SIGNATURE

s. 19217

DATE 6/18/4 SHT 1 OF /

BOEING AIRPLANE COMPANY TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT



On starting - # 1 rogine starter failed to

Cause - unknown; U.R. suspects failure of centrifugal switch.

JATRACTED DIRECTLY

- Normal starting of no. 1 engine.
- 2. No. 1 e gine faired to rotate.
- Suspected contribugal switches are not operating.
- hem ved and re, laced with like serviceable it in. Defective item turned into supply for disposition and repair.
- Recommend ranufacturer be advised of this condition and corrective action be taken as necessary.

(OFFICE)

SIGNATURE KO HENZLEY

s: 24415

SHT 1 OF

BAC 3550 (P)

ROUTING 1. G F/2

IPM

BOEING AIRPLANE COMPANY TRANSPORT DIVISION

FAILURE OR UNSATISFACTORY REPORT



COUTING

On preflight - air bottle valve assembly was found to k leaking air.

Cause - unknown XTRACTED DIRECTLY FROM UR

- 1. Routine preflight.
- Air bettle would not hold air.
- Valve assy. Part #1/50-511-5286 was found to be leaking air.
- Lemoved and replaced with serviceable item. Defective item turned into supply for disposition.
- 5. Manufacturer be advised of this condition and necessary action be taken.

(OFFICE)

SIGNATURE KO Hanzler

s. 124534 SHT I OF

BOEING AIRPLANE COMPANY

FAILURE OR UNSATISFACTORY REPORT

AIR BOTTLE					
K35A SYSTEM NAMUFACTURER W KIDDE	ER 0407 PART NO. 8	740891 PART N A/C SERIAL 3595 A C HOURS UN	AME YALVE 3400 KN DATE FAILED N 7 8		
2 1 2 2 5 10 20 B 100 250 R	PART HOURS SINCE NER 500 TATE NO N REMARKS	TURNBACK REMARKS A ACT	GHT DEVIATION LE ELECT COPP OR SMOKE COENT JUENT REASON IN REMARKS		
12 12 12 12 12 12 12 12 12 12 12 12 12 1	84 87 88 1 L OUTB'D 2 L INE D 2 R INE D 3 R OUTB'D LEFT LEFT	NO FALLED 4155 INO PERATIVE WHY FALLED 8 WHICH NO WING 79 MARFUNCTION FOUND DURING 79 MARFUNCTION FOUND 70 MARFUNCTION ALL DEPORTMENT 10 MARFUNCTION ALL DEPORT			
PART SERIAL NUMBER	REF CAT. NO10 FIG. NO. 4-72	CUSTOMER UR NO. LAFB	OTHER REF.		
DEMARKS Indicate bediened	INDEX NO. 25	428W-58-2259			
REMARKS. Include background, symptoms, correctine action, recommendations, or sketch, length of delay or turnback.					

ROUTING INGFE During 2rd periodic - the sir bottle valve failed to relieve excessive pressures and also failed to allow air to pass from the bottle to the starter.

- Aircraft was undergoing second periodic when failure occurred.
- Valve would allow too much pressure to enter the bettle.
- Check valve failed to allow air from bottle to the starter.

4. Removed and replaced with like serviceable item. Item being held for UR exhibit.

5. Recommend a tear down and study to determine cause of malfunction.

(OFFICE)

s. 24425 SHT 1 OF

BAC 3590 PA

FIELD SERVICE REPORT

BOEING AIRPLANE COMPANY

TO: ENGINEERING SERVICE DEPARTMENT

SEATTLE Y WICHITA

SUBJECT:

BASE FILE

SERVICE DEPT.

SUBJECT FILE

SI REPORT.

OES Report to General Ryan dated February 27, 1959 CLASSINED CARTRIDGE STARTERS.



On the above date the OES reported to Major General John P. Ryan,
Director of Material, SAC Headquarters on the Airesearch and Sunstrand cartridge starters. Highlights of this report are the following:

On Palymony 24, 1950 representatives of Airesearch and Sunstrand

On February 24, 1959 representatives of Airesearch and Sunstrand arrived at Castle to demonstrate their certridge starters. A B-52F power pack without the alternator drive and a KC-135 # 4 position power pack without the fuel-air starter and air bottle were selected for the evaluation of the starter compatibility on built-up engines. Both starters fit easily in the # 4 engine or the KC-135 However, neither starter will fit within the available envelope of the B-52F power pack without changing the existing location of the water ijection pump supply line, motor operated drain valve, # 15 fire detector and right air exit duct support for the oil cooler. The Airesearch starter also will require changes to the air exit duct of the oil cooler. The Sunstrand unit can be mounted if the above mentioned items are relocated and if the starter exhaust shroud is recountered. The Sunstrand representatives stated that reshaping of the exhaust shroud of the starter imposes no problem. At this point little consideration has been given to the starter exhaust and low pressure air inlet port locations. This will be further investigated.

On February 25, 1959 functional demonstration of both starters were made on a bare -43W engine. Two cartridge starts and two pneumatic starts from the MA-1 air cart were made with the Airesearch unit. Engine idle rpm was obtained within an average 30 seconds on the cartridge starts and an average of 55 seconds on the pneumatic starts. The Airesearch starter cannot be started through the aircraft pneumatic system in its present configuration because the pneumatic inlet port also functions as the exhaust port when the starter wink as operated with a cartridge.

Two cartridge starts were attempted and two air starts were made on the Sunstrand unit. Engine idle rpm was obtained at 30 seconds unilizing the cartridge and at an average of 43 seconds on the pneumatic starts. The first attempt to start the engine with the cartridge was aborted due to an external fire at the breach-to-nozzle transfer tube. This was attriguted to an oil saturated heat shield on the transfer tube; however, this was associated with special instrumentation and was not a result of a starter malfunction. The second try using the cartridge was partially successful in that engine idle rpm was obtained in 30 seconds, immediately followed by flames emitting from the starter fan intake. The Sunstrand representatives stated

NAMEI	aul Ribar	urd		REPORT N	o. CAFB-	OES-635F	DAFebruary	27,1959
STATION	lastle AF	3		LOCATION	v Merce	d. Califo	rnia	and the same of
SUBJECTOI	S Report	to Gener	al Ryan d	ated Febr	uary 27,	1959	MODEL	
REFERENCES	None			ENCLOSI	JRES	2		
					() (1120		Page 1 of	2
BAC 1264-R2	FSR	FSR	FSR	FSR	FSR	FSR	FSR >4/3	13/2 20

SUPPLEMENTARY SHEET

that this condition was attributed to the combination of excessive clearances between the starter turbine wheel and flow separator and afterburning of the cartridge and could be easily rectified.

The OES has requested authorization to install and fly the Airesearch and Sunstrand cartridge starters on two KC-135 aircraft assigned to this base. Both starters will be capable of operating with the cartridge or through a quick disconnect directly to an air cart. To accelerate the testing no attempt will be made to connect the starters to the pneumatic manifold. No aircraft will be flown until installation approval is obtained from WADC and Boeing has coordinated on the installation.

The Airesearch cartridge starter appears airworthy and is being qualified by WADC. In addition this unit is installed on the F-105 aircraft and is a production item. The Sunstrand unit is still in the prototype stage, therefore, qualification by WADC has not been initiated.

1. Cleaning. 2. Duying. 3. Hardening. 4. Shaping.
4. Shaping.
5. Hadwing.
6. Duping.
7. Spraying (BR).
8. Plating.
9. Polishing.
10. Lacque apray.
11. Wounting.

12.

U.S. AIR FORCE BOEING SEATTLE, WASH

JAN 10 9 25 PM '61"

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RR RJWZDMB

DE RBEGUP Ø1Ø

ZNR

R 101500Z

FM AF ENGR SUPPORT OFF BUWEPSREP EAST HARTFORD CONN

TO RJESBH/4228SW COLUMBUS AFB MISS

RJWFNK/OCAMA TINKER AFB OKLA INFO RJWFNH/SAAMA KELLY AFB TEX

RJWXBRB/SAC OFFUTT AFB NEBR

ROWALKET ONG CITCII ALE ILEAK

RJWZDMB/AFPR BOEING SEATTLE WASH

RJEDSQ/AMC WPAFB OHIO

RJWZNF/OTIG NORTON AFB CALIF

RJEBKF/2AF BARKSDALE AFB LA

RJEXDHB/8AF WESTOVER AFB MASS RJWBKN/15 AF MARCH AFB CALIF

NAVY GRNC

BT

UNCLAS SANTSK-174446 FOR 4228SW/D/M/ME/DCM,OCAMA/OCMQ. INFO SANTSA,
SANTRE, SANEP, SANSIA, SAC/DMAB, AFPR/OORSTE, AMC/MCMT, OTIG/AFCD1-3-2,
OCAMA/OCNSP, AFS/DMAA SUBJECT: TDR 61-2002 EUR 4228SW 61-1 DTD 7 JAN
61. THIS MESSAGE IN THREE PARTS. PART ONE FOR 4228SW. SUBJECT UR HAS
BEEN DOWNGRADED AND ASSIGNED TDR 61-2002. REQUEST ENGINE J57-59W
S/N P631481 REMOVED FROM KC135 S/N 58-713 BE FORWARDED OCAMA FOR PRIORIT
II TDR. SAAMA SHIPPING ORDER OD 2050-2840-61-2009-7040 IS ASSIGNED.
ADVISE AF ENGINEERING SUPPORT OFFICE, SANTSK, PRATT & WHITNEY AIRCRAFT,
EAST HARTFORD, CONN; SAAMA, ATTN: SANTSA, SANTRE; AND OCAMA ATTN:

ATE, MODE OF TRANSPORT AND GBL NR COVERING SHIPMENT. PART II FOR

PAGE TWO RBEGUP Ø10

OCAMA. REQUEST PRIORITY II TDR BE ACCOMPLISHED ON J57-59W S/N P631481 ENGINE . ENGINE IS EXHIBIT ON UR 4228SW 61-1 ASSIGNED TOR 61-2002. REQUEST TOR BE PERFORMED TO DETERMINE CASE OF FAILURE. AT 3000 FT FELT SLIGHT INDICATION OF OIL FUMES IN CABIN BUT QUICKLY DISSIPATED. AT 10,000 FT NR. 1 ENGINE OIL PRESSURE DROPPED TO 10 PSI AND LOSS OF POWER EXPERIENCED. ENGINE SHUT DOWN AND MISSION ABORTED. GROUND Oil Pumps & Accessory Housing INSPECTION REVEALED PIECE OF OPAH FRONT COVER BETWEEN TACH GEN PAD AND STARTER PAD MISSING. N1 AND N2 COMPRESSORS SEIZED. BEARINGS IN OPAH AND ENGINE FAILED FOR LACK OF LUBRICATION. NO INTERNAL FAILURE OR CONTACT OF PARTS WITH OPAH COVER. PROJECT NR TDR-NTSK-61-2002 HAS BEEN ASSIGNED AND SHOULD BE ENTERED IN THE UPPER RIGHT HAND PORTION OF AMC FORM 399. FORWARD THREE COPIES OF COMPLETED FORM TO AF ENGINEERIN SUPPORT OFFICE, SANTSK, PRATT & WHITNEY AIRCRAFT, EAST HARTFORD, CONN., WITH MASTER COPY OF 399 TO SAAMA, ATTN: SANSIA. PART III FOR SANTRE. THIS ADVISES USE OF SHIPPING ORDER NR PD-2050-2840-61-0009-7040 ON TDR PROJECT NTSK-61-2002 ABOVE.

10/1500Z JAN RBEGUP

BT

NNNW ZCXGA212ZCWWD545

RR LINERG

DE MUNERY 173 A

112010 7 ZEX

OCAMA THEFER AFF HET A

TO RJESBA/MOAMA BROOKL Y AFR ALA

INFO RJESER/ 4228S TRATUC COLUMBUS AFE MISS

RJWFKG/AFPR POEING AIRPLANE CO WICHITA KANS

RJWFNW/SAAMA KELLY AFP TEX

RJUZNEA STIE NORTON AFE CALIF

RJW ZGP/928 OMEWG FAIRCHILD AF

RJEZFH/45AD LORING AFE NO

RJWFAF/821 AD ELLSWORTH AFE SDAK RJESSL/4138STRATWS TURNER AFB SA

BT

UNCLAS OCNSIE-5645 FOR TOWS! MOA! A APOUL-3-2 CTIS SANRT SAAMA DMAT 2AF DCMQC 42235 TRATWG. THE FOLLOWING COMMODITY PROBLEM EUR FM 42255 COLUMBUS AFF MISS IS RETLA MMITTED FOR YOUR ACTION AND DIRECT

REPLY TO SUBMITTING ACTIVITY WITH I.E. C. F REPLY TO OCAMA POCNSIEF. QUETE HATTE TO GE TOZ I MEDIATE ALVIATE AND FOR AFPR AND

SAC/DM4. LUFU FOR DCANA / UTVCI DITT A ... 1-0-2 SAAFA/4

2AF/DM4A ALL AF BY ADIV SI AND PIF CURROL 5-52 BASES. SUBJECT EMERGENCY & SPECIAL ANIDLING REGULT AT TO 00-35D-54 A.

60-105 B. TART CULTRUT VALVE CLAST 2995 C. 105492-1-5 S/M

37P-4705 D. AIRSEARC T. KC-135A-58-0106 - J57-P59% - S/N



Date Suspense

Date

TRANSFURT MI JAM 20

CONTRACT ADM

10 23 A

1-/45 422 834

PAGE TWO RUWFAK 173A P-628801 - 902:00. F. BUPTIS WORNAL START PROCEDURE NUMBER 1 ENGINE FAILED TO INDICATE ROTATION. . AIR START CONTROL VALVE FAILED TO OREN WEEN START SWITCH WAS PLACED IN GROUND START PUBLITION. ELECTRICAL -GENTINUITY-AND OPERATION OF CONTROL VALVE SOLECID CHECKED SATISF FACTORY. CAUSE OF FAILURE SUSPECTED TO BE PINDING OF CONTROL VALVE BUTTERFLY VALVE. A. REPOVET AND RAPLACED WITH LIKE SERVICEABLE ITEM I. 4 J. 2 - CNE NOT REPAIRABLE BUL TO FAULTY SOLENGID. ONE NOT REPAIRABLE DUE TO BINDING BUTTERFLY UNIVER NO DEPOXIMATELY 90 PERCENT OF THE ENGINE START PROBLEMS AT THE ACTIVITY ARE CAUSED BY FAILURE OF THE AIRSTART CONTROL VALVE TO OFEN. FAILURE OF THIS VALVE SERIOUSLY AFFECTS MISSION CAPABILITY IT IS SLIEVED A MAJOR CAUSE OF CONTROL VALVE MALFUNCTION IS BIRDLY OF THE PUTTERFLY VALVE IN THE CLOSED POSITION. WEST BINDING TOOTHS THE RESULT ON MIK PRESSURE IS "INSUFFIC-IENT TO BREAK THE BUTTLACKS WILL LOSSE. IT IS RECOMMENDED FAILED W CONTROL VALVES FR OTHER MOINTILS FE RETURNED TO MANUFACTURER AND A COMPLETE INVESTIGATION - COMBUCTED AND CORRECTIVE ACTION TAKEN. L. 902:00 NEW N. HEID FUR PISTON TION INSTRUCTION. N. ROBERT L LEWIS CAPT 4228 STRAT WING NOT PHONE SE4-7646. NON-DUTY GL4-6228. UNQUOTE.

11/2023 JAN RJWFNY

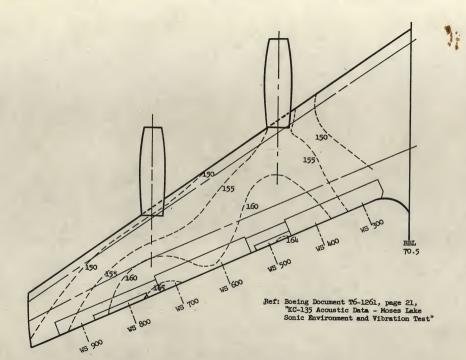


FIGURE 8 - SOUND PRESSURE LEVEL CONTOUR MAP OF KC-135 LOWER WING SURFACE (OVER-ALL FREQUENCY BAND AT FULL WET POWER)

DETERMINED, 1 - CONTACT CONNECTIONS DEFECTIVE, 2 - OVERSPEED, 2 - FAULTY PARTS, PERIOD 1 SEP 1960 THRU 28 FEB 1961.

H 9 - BEFORE FLIGHT, 2 - INFLIGHT NO-ABORT, 44 - BETWEEN FLIGHTS,

1 - PREFLIGHT INSPECTION, 1 - HOURLY POSTFLIGHT INSPECTION. PERIOD

1 SEP 1960 THRU 28 FEB 1961.

I 50 - REMOVED AND REPLACED, 1 - REMOVED REPAIRED AND REINSTALLED,

1 - REPAIR OF ATTACHING PARTS, 3 - ADJUST, 2 REMOVED. PERIOD

1 SEP 1960 THRU 28 FEB 1961

J 57

K 482.2 MANHOURS

L INVESTIGATION REVEALED THE FOLLOWING TYPE MALFUNCTIONS RESULTED

IN FAILURE OF FUEL AIR STARTERS PAN 7TH \$18-M35 MANUFACTURED BY

GENERAL ELECTRIC CO: 1. CUT-OUT CENTRIFUGAL SWITCH OPENS CIRCUIT

BEFORE ENGINE HAS ATTAINED ENOUGH RPM TO SUSTAIN GOMBUSTION. ACCELERATION

2. FUEL INJECTION IS RESTRICTED BY CARBON BUILD-UP AROUND THE

INJECTION NOZZLE. 3. FUEL LEAKS DEVELOPING AROUND THE FUEL INJECTION NOZZLE. THE FOLLOWING TYPE MALFUNCTIONS RESULTED IN FAILURE

OF FUEL AIR STARTERS PAN HS541091 MANUFACTURED BY HAMILTON STANDARD:

PAGE THREE 432

(1) NORMAL CUT-OUT CENTRIFUGAL SWITCH OPENS BEFORE ENGINE HAS
ATTAINED ENOUGH RPM TO SUSTAIN COMBUSTION (2) NORMAL CUT-OUT
CENTRIFUGAL SWITCH FAILS TO OPEN AND OVERSPEED SWITCH ACTUATES
TO STOP STARTER. THE OVERSPEED SWITCH MUST BE RESET MANUALLY
AND REQUIRES REMOVAL AND REPLACEMENT OF STARTER (3) CLUTCH FAILS
TO MAKE A POSITIVE ENGAGEMENT AND SLIPS UNDER TORQUE. INVESTIGATION



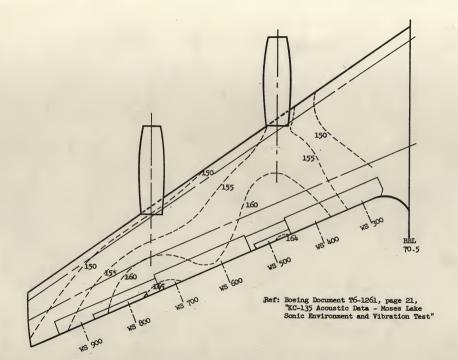


FIGURE 8 - SOUND PRESSURE LEVEL CONTOUR MAP OF KC-135 LOWER WING SURFACE (OVER-ALL FREQUENCY BAND AT FULL WET POWER)

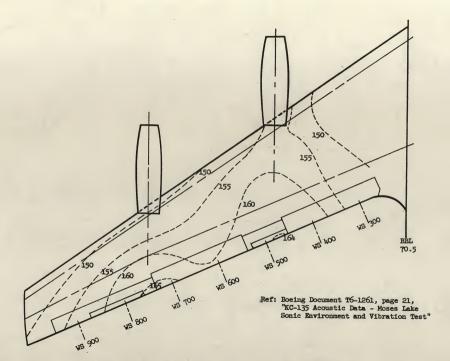


FIGURE 8 - SOUND PRESSURE LEVEL CONTOUR MAP OF KC-135 LOWER WING SURFACE (OVER-ALL FREQUENCY BAND AT FULL WET POWER)

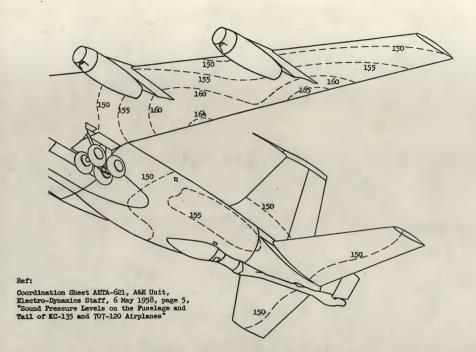
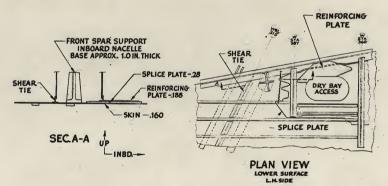
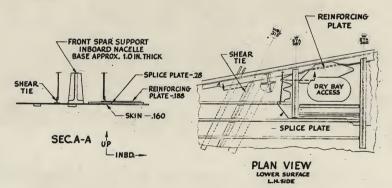


FIGURE 7 - MEASURED SOUND PRESSURE LEVELS OF OVER-ALL FREQUENCY BAND ON KC-135 WITH J57-P43 ENGINES AT FULL WET POWER

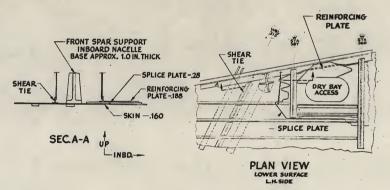




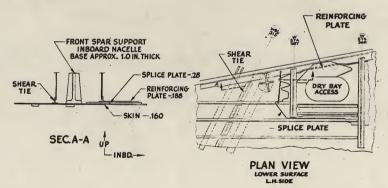




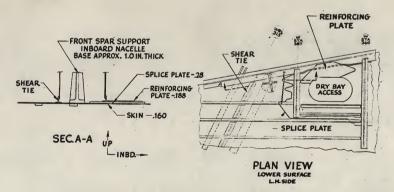




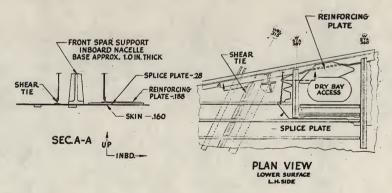




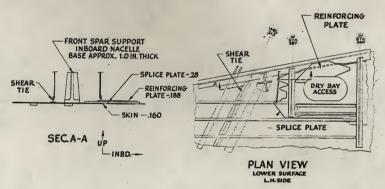




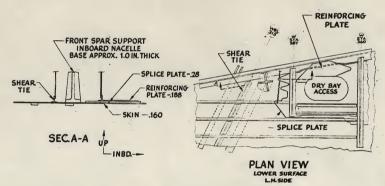




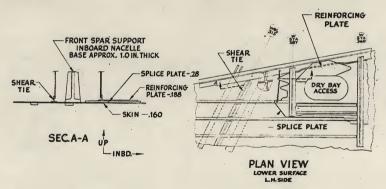




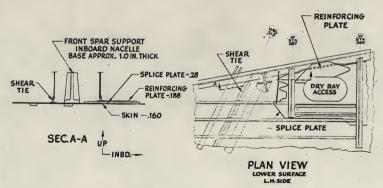




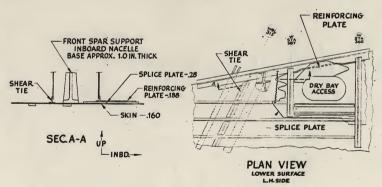




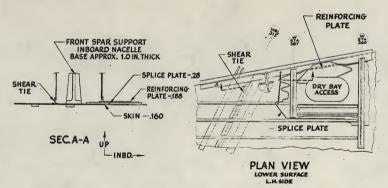












LEADING EDGE SKIN CRACKS

PROBLEM:

CRACKS IN LEADING EDGE SKINS AT THE RIVET COMMON TO THE INTERSECTION
OF SPANWISE STRINGER AND THE RIB - UPPER AND LOWER SURFACE

CAUSE:

FATIGUE - BUFFETING OF THE SKIN

ACTION:

- A REPLACE MAGNESIUM SKINS WITH ALUMINUM SKINS
- B REPAIR OF CRACKS
 - 1. . CRACK LESS THAN .03 DRILL OUT RIVET & REPLACE WITH 1/4 INCH RIVET.
 - 2. CRACK LESS THAN .40 LEAVE AS IS EXCEPT I ABOVE
 - 3. CRACK IS .40 TO .75 STOP DRILL I/8" & FILL WITH SEALANT
 - 4. TWO OR MORE CRACKS PER RIVET .40 TO .50 STOP DRILL 1/8" & FILL
 - CRACKS IN EXCESS OF ABOVE FLUSH PATCH REPAIR PER IC-135(K)A-3.

LEADING EDGE SKIN CRACKS

PROBLEM:

CRACKS IN LEADING EDGE SKINS AT THE RIVET COMMON TO THE INTERSECTION OF SPANWISE STRINGER AND THE RIB - UPPER AND LOWER SURFACE

CAUSE:

FATIGUE - BUFFETING OF THE SKIN

ACTION:

- A REPLACE MAGNESIUM SKINS WITH ALUMINUM SKINS
- B REPAIR OF CRACKS
 - 1. . CRACK LESS THAN .03 DRILL OUT RIVET & REPLACE WITH 1/4 INCH RIVET.
 - 2. CRACK LESS THAN .40 LEAVE AS IS EXCEPT I ABOVE
 - 3. CRACK IS .40 TO .75 STOP DRILL 1/8" & FILL WITH SEALANT
 - 4. TWO OR MORE CRACKS PER RIVET .40 TO .50 STOP DRILL 1/8" & FILL
 - CRACKS IN EXCESS OF ABOVE FLUSH PATCH REPAIR PER IC-135(K)A-3.

PROBLEM:

CRACKS IN LEADING EDGE SKINS AT THE RIVET COMMON TO THE INTERSECTION
OF SPANWISE STRINGER AND THE RIB - UPPER AND LOWER SURFACE

CAUSE:

FATIGUE - BUFFETING OF THE SKIN

- A REPLACE MAGNESIUM SKINS WITH ALUMINUM SKINS
- B REPAIR OF CRACKS
 - 1. CRACK LESS THAN .03 DRILL OUT RIVET & REPLACE WITH 1/4 INCH RIVET.
 - 2. CRACK LESS THAN .40 LEAVE AS IS EXCEPT I ABOVE
 - 3. CRACK IS .40 TO .75 STOP DRILL 1/8" & FILL WITH SEALANT
 - 4. TWO OR MORE CRACKS PER RIVET .40 TO .50 STOP DRILL 1/8" & FILL
 - CRACKS IN EXCESS OF ABOVE FLUSH PATCH REPAIR PER IC-135(K)A-3.

PROBLEM:

CRACKS IN LEADING EDGE SKINS AT THE RIVET COMMON TO THE INTERSECTION
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PROBLEM:

CRACKS IN LEADING EDGE SKINS AT THE RIVET COMMON TO THE INTERSECTION
OF SPANWISE STRINGER AND THE RIB - UPPER AND LOWER SURFACE

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 - CRACKS IN EXCESS OF ABOVE FLUSH PATCH REPAIR PER IC-135(K)A-3.

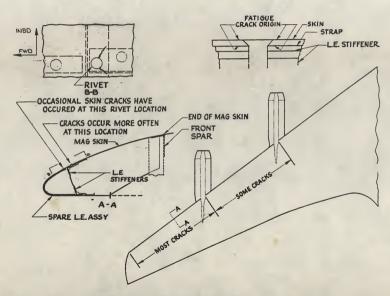
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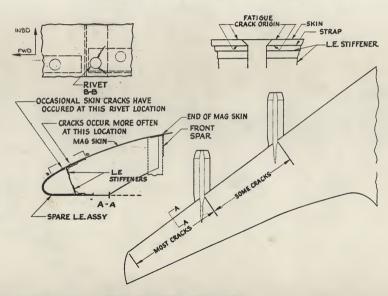
CRACKS IN LEADING EDGE SKINS AT THE RIVET COMMON TO THE INTERSECTION
OF SPANWISE STRINGER AND THE RIB - UPPER AND LOWER SURFACE

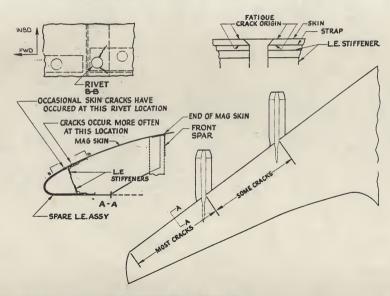
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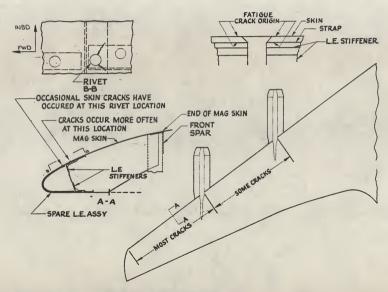
FATIGUE - BUFFETING OF THE SKIN

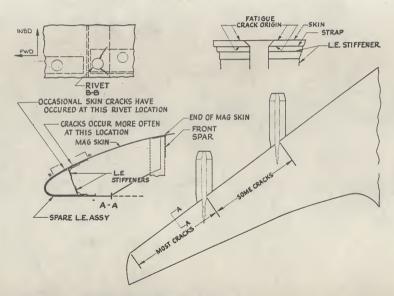
- A REPLACE MAGNESIUM SKINS WITH ALUMINUM SKINS
- B REPAIR OF CRACKS
 - 1. . CRACK LESS THAN .03 DRILL OUT RIVET & REPLACE WITH 1/4 INCH RIVET.
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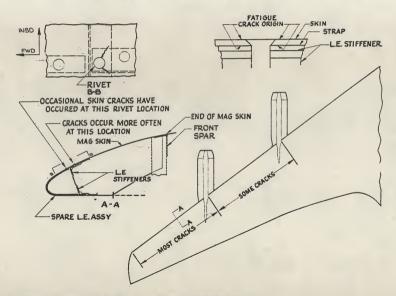


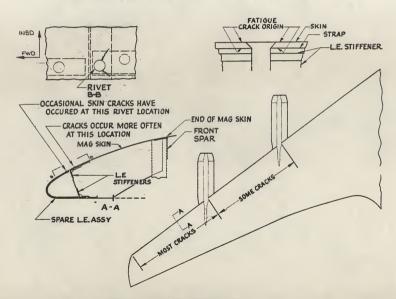


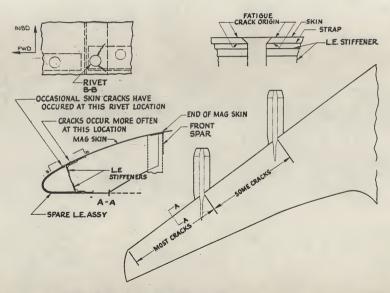


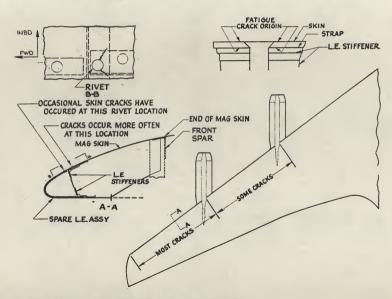


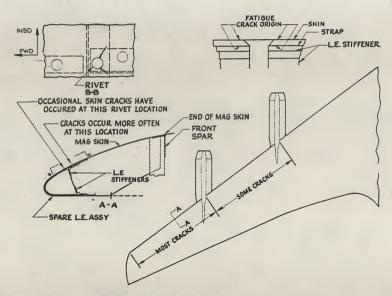












Attachment I to C/S 61-5 Page 2 of 2

INBOARD AILERON TAB

PROBLEM

AILERON CONTROL BINDING

CAUSE

TAB NOSE RETENTION SCREWS BACKING OUT (VIBRATION)

- A PRODUCTION
 - COATED SCREWS AND HELI-COIL INSERTS WITH BMS 5-29

 TYPE I OR II EFFECTIVE 59-1483 (386) THRU 59-1497 (400)
 - 2. ITEM I. PLUS COATED TAB NOSE AND BALANCE WEIGHT WITH BMS 5-19
 TYPE BI EFFECTIVE 59-1498 (401) & ON
- B RETROFIT & INSPECTION
- 1. T.O. -875 INSPECTED SCREWS FOR REQUIRED LENGTH
 - 2. T.O. -915 (RELEASED 29 AUGUST 1960) WILL REQUIRE COATING OF SCREWS AND HELI-COIL INSERTS WITH BMS 5-29 TYPE I OR II EFFECTIVE AIRPLANES 57-1464 (144) & ON INCLUDING AILERON TABS 5-87421-61, -62, -69, -70, -79, -80, -87, -88.

INBOARD AILERON TAB

PROBLEM

AILERON CONTROL BINDING

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INBOARD AILERON TAB

PROBLEM

AILERON CONTROL BINDING

CAUSE

TAB NOSE RETENTION SCREWS BACKING OUT (VIBRATION)

- A PRODUCTION
 - 1. COATED SCREWS AND HELI-COIL INSERTS WITH BMS 5-29
 TYPE I OR II EFFECTIVE 59-1483 (386) THRU 59-1497 (400)
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COMPONENT	PRO- JECTED STRUC- TURAL AREA, SQ FT	NUMBER OF REPORTED KC-135 STRUCTURAL MALFUNCTIONS								TOTAL	NUMBER
			0	Ф		▽	•	-	•	NUMBER OF PRIMARY RMALFUNG TIONS	
		HONEYC'B DELAM.		CONTROL ROD WORN	SKIN CRACKED	RIB CRACKED	STIFE CRACKED	BRACKET CRACKED			
WINGS, Excl.Cont.Surfaces Inboard Ailerons Inboard Aileron Tabs Outboard Ailerons Outboard Aileron Tabs Inboard Flaps Outboard Flaps Fillet Flaps	1992.0 54.0 5.8 67.0 9.0 162.8 168.0 66.8	5 0 2 30	2 0 179 10 53 0 0	10 21 32 0 27 0 0	59** 1 2 11 0 15 28	49 17 0 3 0 1 0	9 0 0 1 0 0	55 0 0 0 0 0	7 43 12 2 0 0	191 83 230 27 82 31 36 28	0.1 1.5 39.7 0.4 9.1 0.2 0.2 0.4
FIN, Excl.Cont.Surfaces Rudder Rudder Trim Tab Rudder Control Tab Rudder Antibalance-Tab Rudder Stability Tab	197.0 118.3 1.9 1.5 1.4 3.6	- 5 4 10 20	0 3 0 0 0	0 1 1 0 0	0 0 1 0 0 3	0 6 0 0 0	0 0 0 0 0	0 0 0 0 0	2 1 0 0 0	2 11 7 4 10 24	0.01 0.1 3.7 2.1 7.1 6.7
STABILIZERS, Excl.Cont.Surf. Elevators Elevator Control Tabs Stab. Act. Elevator Tabs	374.6 132.8 12.9 4.9	7 7 5	43 7 0 2	0 0 0 8	1 2 0 0	0 0 0	0 0 0	0 0 0	0 0	46 16 7 15	0.1 0.1 0.5 3.1
WINGS, Incl.Cont.Surf. FIN, " " " STABILIZERS, " " "	2525.4 323.7 525.2	58 39 19	244 4 52	90 2 8	116* 4 3	70 6 0	10 0 0	55 0 0	65 3 2	708 58 84	0.28 0.18 0.16
WINGS STABILIZERS FIN TOTAL	3374-3	116	300	100	123	76	10	55	70	850	0.25
	\times	14%	35%	12%	15%	9%	1%	6%	8%	100%	\times

*Not included are approx. 300 skin cracks eminating from rivet holes in the wing leading edge.

COMPONENT	PRO- JECTED STRUC- TURAL AREA, SQ FT	NUMBER OF REPORTED KC-135 STRUCTURAL MALFUNCTIONS								TOTAL	NUMBER
			0	ф		▽	•		•	NUMBER OF PRIMARY RMALFUNG TIONS	
		HONEYC'B DELAM.		CONTROL ROD WORN	SKIN CRACKED	RIB CRACKED	STIFE CRACKED	BRACKET CRACKED			
WINGS, Excl.Cont.Surfaces Inboard Ailerons Inboard Aileron Tabs Outboard Ailerons Outboard Aileron Tabs Inboard Flaps Outboard Flaps Fillet Flaps	1992.0 54.0 5.8 67.0 9.0 162.8 168.0 66.8	0 1 5 0 2 30 20	2 0 179 10 53 0 0	10 21 32 0 27 0 0	59* 1 2 11 0 0 15 28	49 17 0 3 0 1 0	9 0 0 1 0 0	55 0 0 0 0 0	7 43 12 2 0 0 1	191 83 230 27 82 31 36 28	0.1 1.5 39.7 0.4 9.1 0.2 0.2
FIN, Excl.Cont.Surfaces Rudder Rudder Trim Tab Rudder Control Tab Rudder Antibalance Tab Rudder Stability Tab	197.0 118.3 1.9 1.5 1.4 3.6	- 5 4 10 20	0 3 0 0 0	0 1 1 0 0	0 0 1 0 0 3	0 6 0 0 0	0 0 0 0 0 0	0 0 0 0	2 1 0 0 0	2 11 7 4 10 24	0.01 0.1 3.7 2.1 7.1 6.7
STABILIZERS, Excl.Cont.Surf. Elevators Elevator Control Tabs Stab. Act. Elevator Tabs	374.6 132.8 12.9 4.9	- 7 7 5	43 7 0 2	0 0 0 8	1 2 0 0	0 0 0	0 0 0	0 0 0	2 0 0	46 16 7 15	0.1 0.1 0.5 3.1
WINGS, Incl.Cont.Surf. FIN, " " STABILIZERS, " " "	2525.4 323.7 525.2	58 39 19	244 4 52	90 2 8	116* 4 3	70 6 0	10 0 0	55 0 0	65 3 2	708 58 84	0.28 0.18 0.16
WINGS STABILIZERS FIN TOTAL	3374-3	116	300	100	123	76	10	55	70	850	0.25
	\times	14%	35%	12%	15%	9%	1%	6%	8%	100%	\times

*Not included are approx. 300 skin cracks eminating from rivet holes in the wing leading edge.





- (1) Location
- (2) Description
- c. Fill and drain procedures
- 6. Oxygen systems
 - a. Oxygen requirements
 - (1) Crew
 - (2) Passengers
 - b. Passenger oxygen system
 - (1) System equipment
 - (a) location
 - (b) type
 - (c) function
 - (2) System operation
 - (3) Servicing
 - (4) Portable oxygen bottles
 - (a) purpose
 - (b) description
 - (c) location
 - c. Crew oxygen system
 - (1) System equipment
 - (a) location
 - (b) description
 - (c) operation
 - d) servicing
 - (2) Portable oxygen bottle
 - (a) location
 - (b) description
- 7. Lighting

- Cargo compartment doors
 - (1) Type
 - Location (2)
 - (3) Description
 - (4) Operation
- Cargo compartment floor and lining
 - General description (1)
 - (2) Insulation
 - (3) Access and inspection openings
- Cargo compartment equipment
 - (1) Shelves
 - (a) description
 - (b) attachment
 - folding provisions (c)
 - Netted webbing (2)
 - (a) description
 - (b) attachment
 - (c) adjustment
- Fire protection f.
 - Fire detection
 - Control
- 5. Cabin water systems
 - Description of systems
 - (1) Forward
 - (2) Aft
 - b. Service panels

- (1) Escape hatches
- (2) Main entry doors
- (3) Galley doors
- (4) Chop-out areas
- b. Location and description of emergency equipment
 - (1) Escape slides
 - (2) Escape ropes
 - (3) Life rafts
 - (4) Fire extinguishers
 - (5) Oxygen
 - (6) Life vests
 - (7) Crash axes
 - (8) First aid kits
 - (9) Flares
 - (10) Lights
 - (11) Special emergency equipment
- 4. Cargo compartments
 - a. General description
 - (1) Classification
 - (2) Forward compartment
 - (3) Aft compartment
 - b. Load capacities and distribution
 - (1) Forward compartment
 - (2) Aft compartment

- (1) Seating arrangement variations
 - (a) first class
 - (b) tourist
 - (c) mixed service
- k. Floor and floor covering
 - (1) Floor structure
 - (2) Main floor covering
 - (a) removal
 - (b) replacement
 - (3) Lavatory compartment and galley floor covering
- 1. Sidewall windows and panels
 - (1) Insulation
 - (2) Window panels
 - (a) description
 - (b) window size and material
 - (c) window shades
 - (d) panel fasteners
 - (e) removal and installation
 - (3) Dado panels
 - (a) description
 - (b) removal and installation
- m. Ceiling
 - (1) Insulation
 - (2) Panels
 - (a) removal and installation
 - Equipment stowage provisions
- 3. Emergency equipment
 - a. Escape provisions

- f. Galleys
 - (1) Type
 - (2) Location and arrangement
 - (3) Installation
 - (4) Galley service doors
 - (a) type
 - (b) description
 - (c) operation
- g. Coat compartments
 - (1) Description
 - (2) Location
- h. Cabin attendant stations
 - (1) Location
 - (2) Seat provisions
 - (3) Cabin attendant's control panel
 - (a) location and description
 - (b) passenger call system
- i. Miscellaneous passenger cabin equipment
 - (1) Screens and partitions
 - (a) location
 - (b) purpose
 - (2) Magazine racks
 - (a) location
 - (3) Passenger signs
 - (a) type

4 1. BAC 1546 L-R3

- (b) location
- j. Alternate passenger cabin arrangement

86

- (1) Purpose
- (2) Location
- (3) General description
- d. Passenger service units
 - (1) Purpose
 - (2) Location
 - (3) General description of unit and components
 - (a) air outlets
 - (b) reading lights
 - (c) oxygen masks
 - (d) attendant call
 - (e) loudspeaker
 - (4) Spacing adjustments
- e. Lavatory compartments
 - (1) Location and arrangement
 - (2) Toilet equipment
 - (a) description
 - (b) servicing provisions
 - (3) Wash basin equipment
 - (a) description
 - (b) drain provisions
 - (4) Lavatory compartment equipment
 - (a) description
 - (b) location
 - (c) servicing
 - (5) Signs and indicators
 - (a) type
 - (b) location

- (a) oxygen equipment
- (b) fire extinguisher
- crash axe (c)
- (d) first aid kit
- (4) Spare bulb storage
- (5) **Facilities**
- f. Interior finish
 - (1) Lining
 - (2) Flooring
- Passenger cabin equipment and furnishings 2.
 - Main entry doors
 - (1) Type
 - (2) Location
 - Description (3)
 - Operation (4)
 - Passenger seats

b.

- General description (1)
 - (a) types
 - (b) seat arms
 - ash trays (c)
 - seat pockets (d)
 - recline operation (e)
 - removal (f)
 - (g) installation
- (2) Seating arrangement
 - method of attachment (a)
 - seat spacing (b)
 - (c) seat identification
 - interchangeability (d)
- Overhead racks c.

L. Equipment and Furnishings

24 Hours 1, 2, 3, 5, 6, 8,

- Control cabin equipment and 1. furnishings
 - Crew stations
 - Arrangement (1)
 - Control panels (2)
 - b. Crew seats
 - (1) Type
 - Adjusting features (2)
 - c. Coat compartment
 - (1) Coat storage
 - (2) Hat rack
 - (3) Bookcase
 - Equipment for crew members d.
 - (1) Data cases
 - (2) Sunvisors
 - (3) Ash trays
 - Oxygen masks and mask storage (4)
 - Headset and microphone holders (5)
 - (6) Coffee cup holders
 - e. Control cabin bulkhead
 - (1) Location
 - (2) Door
 - Emergency equipment storage (3)

- (a) type and size
- cable run (b)
- (5) Aft rudder quadrant
 - (a) location
 - tab linkage and centering spring (b)
- Upper control tab (6)
- Lower control and anti-balance tab (7)
- (8) Gust damper
- Rudder trim system c.
 - (1) Trim control knob
 - degrees trim (a) pointer
 - (b)
 - Control cables (2)
 - (a) type and size
 - (b) cable run
 - (3) Trim actuator assembly
 - (a) cable attachment
 - (b) movement
 - (c) brake assemblies
 - Rudder trim tab
 - tab attachments (a)
 - deflection angles (b)
 - (c) rudder deflections
- d. Rigging procedures
 - (1) Control cables
 - (2) Linkage
- 8. Examination and review

- (4) Control cables
 - (a) type and size
 - (b) cable run
- d. Rigging procedures
 - (1) Cable system
 - (2) Linkage
- 7. Rudder system
 - Rudder design
 - (1) Structure

 - (a) spars
 - (b) ribs
 - (c) skin
 - balance panel and seals (d)
 - (e) tabs
 - attachments (f)
 - (2) Operational description
 - (a) deflection angles
 - (b) structural stops
 - b. Rudder control system
 - (1) Rudder pedals
 - (a) attachment points
 - (b) stops
 - Rudder pedal adjustment (2)
 - (a) crank and flexible shaft
 - (b) universal joint and screw mechanism
 - (3) Forward quadrants and bus system
 - (a) attachments
 - (b) left and right bus system
 - (4) Control cables

- (2) Operational description
 - (a) deflection angle
 - (b) effectiveness
- b. Electrical actuation
 - (1) Control switches
 - (a) location
 - (b) positions
 - (2) Cutout switch
 - (a) location
 - (b) function
 - (3) Warning light
 - (a) location
 - (b) function
 - (4) Trim actuator
 - (a) trim motor
 - (b) magnetic clutch
 - (c) slip clutch
 - (d) limit switches
 - (e) jack screw
 - (f) differential gearing
 - (g) aft cable drum
 - (h) auto-pilot servo
- c. Manual actuation
 - (1) Control wheel
 - (2) Chain drive and sprockets
 - (a) location
 - (b) function
 - (3) Forward drum mechanism
 - (a) input
 - (b) cable attachments
 - (c) position indicator attachment

- (a) cable type and size
- (b) cable run
- (3) Elevator control quadrant
 - (a) structural attachments
 - (b) auto-pilot servo attachment
- (4) Centering spring
 - (a) function
- (5) Control tab linkage and stops
 - (a) components
- (6) Control tabs
 - (a) type
 - (b) function
- (7) Gust damper
 - (a) location
 - (b) function
- c. Stabilizer actuated tab
 - (1) Linkage
 - (2) Tab
- d. Rigging procedures
 - (1) Cable systems
 - (2) Linkages
- 6. Stabilizer trim
 - a. Design features
 - (1) Structure
 - (a) torque box
 - (b) attachments

- (4) Inboard control differential
- (5) Inboard control valve
 - (a) input (b) follow-up
 - (b) follow-up
- (6) Outboard control differential
- (7) Outboard control valve
 - (a) input
 - (b) follow-up
- d. Rigging procedures
 - (1) Cable system
 - (2) Linkages
- 5. Elevator system
 - a. Elevator design
 - (1) Structure
 - (a) spars
 - (b) ribs
 - (c) skin
 - (d) balance panel and seals
 - (e) tabs
 - (f) attachments
 - (2) Operational description
 - (a) deflection angles
 - (b) stops
 - b. Elevator control system
 - (1) Control column
 - (a) deflection angles
 - (b) stops
 - (2) Control cables

- (a) construction
- (b) materials
- (c) attachments
- (2) Operational description
 - (a) deflection angles
 - (b) blow down features
 - (c) aerodynamic separation control
 - (d) warning horn
- b. Spoiler control system
 - Control wheel
 - (2) Control cables
 - (a) cable type and size
 - cable run (b)
 - Control quadrant and linkage (3)
 - (4) Spoiler control valve
 - (a) input
 - (b) follow-up
 - Spoiler actuator
 - (a) location
 - (b) attachments
 - Spoiler follow-up differential
- c. Speed brake control system
 - (1) Speed brake control lever
 - (a) location
 - (b) positions
 - (2) Control cables
 - (a) cable type and size
 - (b) cable run
 - (3) Input quadrant

- (5) Centering spring
- (6) Gust damper
- (7) Control tab
- Outboard aileron control system
 - Aileron balance bus (1)
 - (a) cable type and size
 - (2) Control quadrant
 - (3) Lockout mechanism
 - (4) Control linikage
 - (5) Balance tab
- Aileron trim system d.
 - (1) Trim control knob
 - (a) location
 - (b) trim indicator
 - (2) Control cable
 - (a) cable type and size
 - (b) cable run Trim mechanism
 - - (a) tack screw
 - brake (b)
- Rigging procedures

(3)

- (1) Cable systems
- Linkages (2)
- Spoiler and speed brake system
 - Spoiler design
 - (1) Structure

- (2) AC electrical motors
 - (a) location
 - (b) type
 - (c) output
- f. Rigging procedures
 - (1) Control cables
 - (2) Drive system linkage
- 3. Aileron system

b.

- a. Aileron design
 - (1) Structure
 - (a) spars
 - (b) ribs
 - (c) skin
 - (d) balance panel and seals
 - (e) tabs
 - (f) attachments
 - (2) Operational description
 - (a) deflection angles
 - (b) structural stops
 - Inboard aileron control system
 - (1) Control wheel
 - (a) type
 - (b) switches
 - (c) deflection angles
 - (2) Control cable system
 - (a) cable type and size (b) cable run
 - .,
 - (3) Control quadrant
 - (4) Control tab linkage

- (3) Flap drive motors
 - (a) location
 - (b) type
- (4) Flap by-pass valve
 - (a) location
 - (b) type
 - (c) power supply
 - (d) function
- d. Flap drive and position
 - (1) Inboard and outboard flap drive units
 - (a) location
 - (b) input
 - (c) internal gearing
 - (d) torque drive output
 - (2) Flap drive torque tubes
 - (a) location
 - (b) couplings
 - (c) drive screw and gear boxes
 - (3) Outboard aileron lockout mechanism
 - (a) angle gear box
 - (b) jack screw
 - (c) aileron lockout attachment
 - (4) Flap position transmitter and indicator system
 - (a) power supply
 - (b) transmitters
 - (c) indicators
- e. Emergency electrical flap drive system
 - (1) Control
 - (a) power supply
 - (b) control switches
 - (c) relays
 - (d) limit switches

- (1) Location
 - (a) inboard
 - (b) outboard (c) fillet
- (2) Structure
 - ------
 - (a) ribs (b) skin
 - (c) attachments
 - (.,
- (3) Operational description
 - (a) fore flap
 - (b) cove lip door
 - (c) flap angle
 - (d) operating time
 - (e) speed limitations
 - (f) flap actuated speed brake cam
 - (g) trim requirements vs flap position
- b. Flap control system
 - (1) Control handle
 - (a) location
 - (b) detents
 - (c) warning horn
 - (2) Control cable system
 - (a) cable type and size
 - (b) cable run
- c. Flap hydraulic system
 - (1) Flow regulating valve
 - (a) location
 - (b) flow rate
 - (c) function
 - (2) Flap metering valves
 - (a) location
 - (b) input
 - (c) follow-up system

K. Flight Controls

24 Hours 1, 2, 3, 5, 6, 8,

1. Introduction

- a. Control surface location
 - (1) Inboard ailerons
 - (2) Outboard ailerons
 - (3) Spoilers speed brakes
 - (4) Elevators
 - (5) Rudder
 - (6) Wing flaps
 - (7) Stabilizer trim
- b. Aerodynamic balance panels
 - (1) Control tabs
 - (a) actuation
 - (2) Internal balance panels
 - (a) hinges
 - (b) seals
 - (c) static balance
 - (d) air bleed control
- c. Control tab follow-up ratio
 - (1) Positive
 - (a) definition
 - (b) function
 - (2) Negative
 - (a) definition
 - (b) function
- 2. Wing flap system
 - a. Flap design

- (2) Actuation
- (3) Pneumatic ports
- (4) Operation
- d. Shuttle valve
 - (1) Location
 - (2) Actuation
- e. Brake
 - (1) Pneumatic actuation
- 8. Anti-skid system
 - a. Skid detector
 - (1) Location
 - (2) Flywheel rotation
 - (3) Commutator signal pickups
 - b. Control shield
 - (1) Location
 - (2) Signal action
 - c. Dual anti-skid valve
 - (1) Location
 - (2) Function
 - (3) Signal reaction
 - (4) Brake pairs controlled
- 9. Examination and review

(6)	Loc	kout deboost valves	
	(a)	location	
	(b)	lockout function	
	(c)	deboost function	
	(d)	servicing operation	
(7)	Auto	omatic brake adjuster valve	
	(a)	location	
	(b)	function	
	(c)	operation	
(8)	Shut	tle valve	
	(a)	location	
	(b)	function	
	(c)	operation	
(9)	Brak	ce	
	(a)	location	
	(b)	type	

7. Pneumatic brake system

a. Pneumatic cylinder

(c)

- (1) Location
- (2) Charge pressure
- (3) Charging valve location

operation

- b. Pressure indicating system
 - (1) Cylinder gage
 - (a) location
 - (2) Cockpit gage
 - (a) location
- c. Pneumatic pressure control
 - (1) Location

- (4) Brake control cable system
 - (a) cable type and size
 - (b) cable routing
- (5) Centering spring
 - (a) location
 - (b) function
- (6) Metering valve
 - (a) cable attachment
 - (b) actuation
- b. Brake hydraulic system
 - (1) Brake pressure source
 - (a) utility system
 - (b) auxiliary system
 - (2) Brake accumulator
 - (a) location
 - (b) pneumatic charge
 - (3) Accumulator charge indicating system
 - (a) transmitter location
 - (b) gage location
 - (4) Brake metering valves
 - (a) location
 - (b) mechanical actuation
 - (c) L.G. "Up" pressure actuation
 - (d) hydraulic ports
 - (e) operation
 - (5) Dual anti-skid valves
 - (a) location
 - (b) hydraulic ports
 - (c) function

- (2) Steering disconnect valve
 - (a) installation
 - (b) trunnion actuation
- (3) Steering metering valve
 - (a) installation
 - (b) hydraulic ports
 - (c) actuation means
 - (d) hydraulic fluid flow
 - (e) centering springs action
 - (f) compensator action
 - (g) flow by-pass passages
- (4) Steering cylinders
 - (a) attachment points
 - (b) hydraulic ports
 - (c) operation
- (5) Nose wheel centering
 - (a) oleo cam arrangement
 - (b) actuation
 - (c) switch location
- 6. Hydraulic brake system
 - a. Mechanical control system
 - (1) Brake pedals
 - (a) location
 - (b) actuation
 - (2) Pedal linkage
 - (a) pedal to crank drum
 - (b) pilot-copilot interconnect
 - (3) Parking brake
 - (a) handle location
 - (b) catch location
 - (c) parking brake application
 - (d) parking brake release

- (a) location
- color (b)
- (3) Circuit
 - (a) wiring installation
 - power source (b)
 - (c) circuit breaker
 - (d) operation
- 5. Nose wheel steering
 - Steering control cable system
 - (1) Steering wheel
 - (a) location
 - operation (b)
 - Cable drum (2)
 - location (a)
 - steering wheel rod connection (b)
 - centering switch installation (c)
 - Control cable system (3)
 - (a) cable type and size
 - (b) cable routing
 - (4) Steering follow-up mechanism
 - (a) location
 - (b) type
 - (c) operation
 - Steering knuckle
 - (a) cable attachment
 - follow-up action (b)
 - Steering hydraulic system b.
 - L.G. selector valve
 - (a) valve actuation
 - (b) pressure source

- (3) Lock switches
 - (a) location
 - (b) actuation
- (4) Gear warning light
 - (a) location
 - (b) color
- (5) L.G. control lever switches
 - (a) location
 - (b) lever actuation
- (6) Warning relays
 - (a) location
 - (b) electrical energizing
 - (c) operation sequence
- (7) Warning horn
 - (a) location
 - (b) sound
- (8) Throttle retard switches
 - (a) location
 - (b) throttle actuation
- (9) Circuit
 - (a) wiring installation
 - (b) power source
 - (c) circuit breakers
 - (d) down and lock operation
 - (e) gear warning light operation
 - (f) gear warning horn operation
- c. Gear door warning
 - (1) Door lock switches
 - (a) location
 - (b) actuation
 - (2) Warning light

4. Landing gear electrical systems

- a. Landing gear lever latch control
 - (1) Lever latch switches
 - (a) location
 - (b) lock action
 - (2) Nose gear centering switch
 - (a) location
 - (b) actuation
 - (3) Main and nose gear safety switches
 - (a) location
 - (b) strut actuation
 - (4) Main gear truck level switch
 - (a) location
 - (b) truck actuation
 - (5) Safety relays
 - (a) location
 - (b) electrical energizing
 - (6) Circuit
 - (a) wiring installation
 - (b) power source
 - (c) circuit breakers(d) operation
 - (d) Operation
- Landing gear position and warning
 - (1) Gear down and lock lights
 - (a) location
 - (b) color
 - (c) dimmer control
 - (2) Gear position switches
 - (a) location
 - (b) actuation

- (d) door opening action
- (e) gear release action
- (f) gear down lock action
- (3) Emergency extension cable system
 - (a) cable type and size
 - (b) cable routing
 - (c) cable spring cartridge installation
- (4) Emergency N.G. door release
 - (a) cable routing
 - (b) operation
- (5) Release drum
 - (a) location
 - (b) locking shaft attachment
 - (c) release operation
- (6) N.G. down lock system
 - (a) down lock pin installation
 - (b) down lock actuation
 - (c) reset of down lock system
- d. Nose gear rigging
 - (1) L.G. control valve
 - (a) centering pin location
 - (b) cable rigging
 - (2) Nose gear mechanical linkage
 - (a) drag brace travel
 - (b) gear actuator travel
 - (c) lock rod travel
 - (d) lock retention rod travel
 - (e) oleo extension
 - (3) Emergency extension
 - (a) emergency door release travel
 - (b) gear release travel
 - (c) gear down lock travel

PAGE

- (d) sequence of port openings
- (6) N.G. lock retention actuator
 - (a) hydraulic port
 - (b) operation
- (7) N.G. lock actuator
 - (a) hydraulic ports
 - (b) operation
- (8) N.G. actuator
 - (a) hydraulic ports
 - (b) operation
- (9) Variable restrictor
 - (a) location
 - (b) purpose
 - (c) hydraulic ports
 - (d) anomation
 - (d) operation
- (10) Fixed restrictors (3)
 - (a) locations
 - (b) purposes
 - (c) hydraulic operation
- (11) Restrictor check valve
 - (a) location
 - (b) purpose
 - (c) hydraulic operation
- c. Emergency extension system
 - (1) Handcrank
 - (a) storage
 - (b) use
 - (2) Handcrank drum
 - (a) location
 - (b) cranking direction
 - (c) pawl operation

- (a) attachment points
- steering forces action (b)
- (10) Steering metering valve
 - valve housing installation
 - follow-up mechanism location (b)
- (11)Landing gear doors
 - (a) attachment points
 - (b) hydraulic actuator installation
 - (c) lock retention bungee installation
 - (d) operation
- Nose gear hydraulic system b.
 - (1) L.G. selector valve
 - cockpit to valve control cable
 - operation (repeat from M.G.)
 - (b) hydraulic ports (repeat from M.G.)
 - (c) three positions (repeat from M.G.)
 - L.G. door control valve (2)
 - (a) location
 - (b) mechanical actuation
 - (c) hydraulic ports
 - (d) sequence of port openings
 - (3) N.G. door actuator
 - (a) location and attachment
 - (b) hydraulic ports
 - N.G. door safety valve (4)
 - (a) location
 - (b) actuation
 - (c) hydraulic ports
 - (d) operation
 - N.G. sequence valve (5)
 - (a) location
 - (b) mechanical actuation
 - hydraulic ports (c)

- (a) temperature limitations
- (b) altitude limitations
- (2) Electrical control
 - (a) control switches
 - (b) pressure switches and lights
 - (c) power lever position
 - (d) fuel regulator water sensing line
- 5. Fire protection system
 - a. Overheat and fire detection system
 - (1) Detector
 - (a) location
 - (b) type
 - (2) Detection cont rol
 - (a) electronic amplifier
 - (b) warning lights
 - (c) warning bell
 - (d) warning bell cutout
 - b. Fire extinguishing system
 - (1) Bottles
 - (a) location
 - (b) discharge valves
 - (c) fire extinguishing agent
 - (2) Plumbing and manifolds
 - (3) Discharge selector valves
 - (4) Operation and control
 - (a) switches
 - (b) relays
- 6. Engine instrument systems

- Constant speed drive oil system c.
 - (1) Oil tank
 - (a) location
 - (b) quantity
 - (c) filler
 - (2) Oil cooler
 - (a) temperature control
 - (b) bypass and relief control
- 4. Water injection system
 - System description
 - (1) Water tank

 - (a) location quantity and indication (b)
 - water pumps (c)
 - drain valves
 - (d) (e) filler

 - (f) thermal drain valve
 - (2) Plumbing
 - (a) locations
 - drain valves (b)
 - Engine mounted equipment (3)
 - (a) shutoff valve
 - (b) regulator
 - discharge manifold (c)
 - b. Fill and drain procedures
 - Water quality (1)
 - Drain valve position
 - Operation c.
 - (1) Requirements

- (b) construction
- (c) filler
- quantity indication (d)
- shutoff valve (e)
- (2) Oil pressure pump
 - (a) location
 - (b) type
 - check and relief valves (c)
 - quantity output (d)
 - (e) pressure output
 - pump case drain (f)
- (3) Oil pressure filter
 - type and location (a)
 - bypass relief (b)
- (4) Oil pressure indicating system
 - (a) pressure transmitter
 - (b) pressure indicator
- (5) Oil pressure distribution
 - oil jet locations (a)
 - (b) bearings
 - bearing seals (c)
- (6) Oil scavenge system
 - (a) pumps
 - (b) distribution
- (7) Oil cooler
 - location (a)
 - medium of heat exchange (b)
 - (c) temperature control
 - (d) bypass and relief control
- Oil breather system (8)
 - (a) case vents
 - (b) oil centrifuge

- (3) Turbine wheel cooling air
- b. Compressor surge bleed control
 - (1) Surge bleed governor
 - flyweight governor (a)
 - (b) metering valves
 - (c) temperature bias
 - (2) Bleed control valve
 - (a) internal operation
 - operation schedule (b)
- c. Turbocompressor air bleed
 - (1) Location and control
- Engine and nose cowl anti-icing d.
 - (1) Engine inlet anti-icing
 - (a) flow control
 - air flow passage (b)
 - (2) Nose cowl anti-icing
 - (a) flow and temperature control
 - (b) anti-icing air distribution
- 3. Engine oil systems
 - Types of oils
 - (1) Lubrication
 - (2) Preservation
 - (3) Quantities
 - Description and operation
 - (1) Engine oil tank
 - (a) location

- (1) Overall dimensions
 - (a) length
 - (b) diameter
 - (c) weight
- (2) Components
 - (a) case breakdown
 - (b) compressors
 - (c) combustion chambers
 - (d) turbine wheels
 - (e) inlet and ex it ducts
 - (f) thrust reverser and noise suppressor
- (3) Engine cowling
- b. Engine accessories
 - (1) Engine fuel system
 - (a) fuel flowmeter
 - (b) fuel pump
 - (c) fuel control unit
 - (d) pressurizing and dump valve
 - (e) fuel nozzle arrangement
 - (2) Hydraulic pump
 - (3) AC generator constant speed drive
 - (a) oil supply tank and lines
 - (b) drive mechanism
 - (4) Engine starter
 - (a) pneumatic starters
 - (b) combustor
- 2. Air bleed systems
 - a. Engine internal air flow
 - (1) Thrust bearing balance chamber
 - (2) Surge bleed chamber

- (2) Waterlines
- (3) Buttock lines
- Design objectives and testing b.
- Structural systems descriptions
 - (1) Stress paths
 - Fail-safe provisions
- 3. Materials
 - Description of materials
 - (1) Strength
 - (a) stress-strain
 - (b) fatigue
 - (c) residual
 - influencing factors (d)
 - (2) Fastening
 - (a) mechanical
 - thermal (b)
 - (c) chemical
 - (3) Forming
 - (a) deforming
 - (b) machining
 - chemical milling (c)
- Processes
 - Finish requirements
 - b. Heat treating
- 5. Examination and review
- D. Power Plant

32 Hours 1, 2, 3, 5, 6, 8,

- General
 - Description of engine



- (2) Waterlines
- (3) Buttock lines
- Design objectives and testing b.
- Structural systems descriptions
 - (1) Stress paths
 - Fail-safe provisions
- 3. Materials
 - Description of materials
 - (1) Strength
 - (a) stress-strain
 - (b) fatigue
 - residual (c)
 - (d) influencing factors
 - Fastening (2)
 - mechanical (a)
 - thermal (b)
 - (c) chemical
 - (3) Forming
 - (a) deforming
 - (b) machining chemical milling (c)
- Processes
 - Finish requirements
 - b. Heat treating
- Examination and review
- Power Plant D.

32 Hours 1, 2, 3, 5, 6, 8,

- 1. General
 - Description of engine



- f. Electrical power
 - (1) Alternating current
 - (a) power source
 - (b) components
 - (c) distribution (d) control
 - (2) Direct current
 - (a) power source
 - (b) components
 - distribution
 - (c) control (d)
 - (3) External power
 - (a) type and source
 - (b) components
 - (c) distribution
 - (d) control
- 7. Examination and review
- 8. Field trip
- Structures

4 Hours 1, 2, 3, 5, 6, 8

- 1. Section breakdown
 - Numerical identification of airplane sections
 - (1) Structural divisions
 - (2) Non-structural installations
 - (a) electrical
 - (b) passenger accommodations
 - (c) other
- 2. Airplane structure
 - Dimensioning practices
 - (1) Stations

- (2) Width
- (3) Cross section height
- e. Landing gear
 - (1) Tread main gear
 - (2) Wheel base-nose to main gear
 - (3) Main gear wheels and tires
 - (4) Nose gear wheels and tires
 - (5) Turning radius
- 4. Principle design weights
 - a. Maximum ground handling
 - b. Maximum in-flight
 - (1) Flaps up
 - (2) Flaps down
 - c. Reserve fuel limitation
 - d. Basic
- 5. General interior arrangement and accommodations
 - a. Control cabin
 - b. Main cabin
- 6. Major systems
 - a. Engine
 - b. Fuel
 - c. Manual
 - d. Hydraulic power
 - e. Pneumatic power

- (8) Aspect ratio
- (9) Mean aerodynamic chord
- (10) MAC location
- b. Flap area
 - (1) Inboard
 - Outboard (2)
 - Fillet (3)
 - (4) Total
- Control surfaces areas
 - Aileron (1)
 - (a) inboard
 - (b) outboard
 - (c) total

 - Horizontal stabilizer (2)
 - (a) span
 - (b) elevator area
 - (c) total area
 - (3) Vertical stabilizer
 - (a) height
 - rudder area (b)
 - (c) dorsal area

 - total area
 - Spoilers (4)
 - (a) inboard are a
 - (b) outboard area
 - (c) total area
- d. Body
 - (1) Length

- (2) Wing
 - (a) swept, low
 - (b) flexible, full cantilever
 - (c) "wet"
- (3) Body
 - (a) semi-monocoque
 - (b) pressurized
- (4) Tail surfaces
 - (a) swept
 - (b) canti-lever
 - (c) folding fin
 - (d) controllable stabilizer
- (5) Landing gear
 - (a) tricycle
 - (b) truck-type main gear
- 3. Principle dimensions
 - a. Wing
 - (1) Span
 - (2) Area
 - (3) Chord
 - (a) root
 - (b) tip
 - (4) Taper ratio
 - (5) Incidence angle
 - (a) root
 - (b) tip
 - (6) Dihedral
 - (7) Sweep back

- a. Attendance
- Examining b.
- Bell system c.
- d. Smoking privileges
- Facilities e.
 - Cafeteria (1)
 - (2) Snack bar
 - (3) Rest rooms
 - (4) Classroom
 - Telephone service (5)
 - Transportation (6)
 - Coat racks (7)
- Airplane General Description В.

 $7\frac{1}{2}$ Hours 1, 2, 3, 5, 6, 9 10, 11

- 1. Introduction
 - History of development
 - 367-80 prototype b.
 - First flight
 - Customer airplane c.
 - (1) "X" model
 - Quantity contracted (2)
 - (3) Time schedule
 - 2. Description
 - Type
 - (1) Number of engines

- a. Structure
- b. Service organization
- c. Training unit
- 2. Program
 - a. Company
 - b. Customer
- 3. Equipment
 - a. Graphic aids
 - (1) Reproducibles
 - (2) Transparencies
 - b. Training devices
 - (1) Cockpit procedures
 - (2) Landing gear
 - (3) Electrical
 - (4) Hydraulic
 - (5) Flight controls
 - (6) Fuel system
 - (7) Air conditioning and pressurization
 - c. Models
 - d. Cutaway parts
 - e. Films
 - f. Manuals
- 4. School procedures

COURSE OUTLINE

INSTRUCTORS AND MAINTENANCE PERSONNEL COURSE

PAA 7121-5

Manner of Hours Training

I. TITLE, DURATION, AND MANNER OF TRAINING

Title:

Model 707-121 Instructors and

Maintenance Personnel

Duration: 192 Hours (24 Academic Days) B.

C. Manner of Training:

Lecture

Projection transparencies 2.

3. Maintenance manual

4. Flight manual

5. Films

6. Charts or photo enlargements

Models 7.

8. Parts or cutaways

9. Trainer

10. Mock-up

11. Airplane

II. OUTLINE OF INSTRUCTION

Orientation

BAC 1546 L-R3

1 Hour 1, 2, 6

Boeing organization

ALIT ORDER NTMBER	SECTION 71 POWER PLANT - GEVERAL	PAA-121 D6-1048	AA-123 D6-2757	CAL_124 D6-2756	TWA-131 D6-2758	254-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	10FT-130 D6-2764	BOAC-LUS 6	AII 4137 D6-2762
71-1	Power Plant Installation	A	800		X	1				es 🗴				X Y X	
71-2	Engine Installation Equipment	X			2	4				X	1		1		
71-3	Engine Mount Details	X													
71-4	Engine Load Diagram	16 🗵													
71-5	Overall Dimensions - JT3C-4 Engine	X	3/	×	×	×		P(1) (2)			X	×			
.71-6	Engine Cowling	P.U.X													
71-7	Engine Nose Cowl and Tab Assembly	Pick				-									
71-8	Engine Load, Strut Structure and Access Diagram	×													
71-9	angine Front View	PLI X	-										1	1-	
71-10	Engine Left Side View	617											1		
71-11	engine Rear View	8 5											1		-

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ART ORDER NUMBER	SECTION 71 (cont.) POWER PLANT - GENERAL	PAA-121 D6-1048	AA-123 D6-2757	CAL-124 D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	cus-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331-	LUFT-130 D6-2764	BOAC-436	AII-437 D6-2762
71-12	Typical Jet Engine Operating Curves	Y NO													
71-13	Engine Right Side View	X													
71-14	Engine Accessory Section - Bottom View) X	`_		L	L									
71-15	Engine Front View	v ₀ ⊠ X							-						
71-16	Engine Plumbing Disconnect	X													
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ART ORDER NUMBER	SECTION 72 . ENGINE	PAA-121 D6-1048	AA-123 D6-2757	CAL_124 D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUTT-130 D6-2764	BOAC-136	ALI-LO7
72-1	Engine Internal Arrangement	ρ Δ 🗵 'Y	BRD		X	X				P41 X		L		X	~
72-2	Engine Bearing and Accessory Drive Schematic	× ×				H					X	L		T	
72-3	ombustion Chamber Details	X Sir X	-	-			-	Ч						Н	
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ART ORDER MUNBER	SECTION 73 (cont.) ENGINE FUEL AND COUTTOL	PAA-121 D6-1048	AA-123 D6-2757	CAL_121, D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	1077-130 26-2764	BOAC-U36	AII -437 D6-2762
73-12	Engine Driven Fuel Pump	73 X						·					L		
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A.i.T. ORDER NUMBER	SECTION 73 . ENGINE FUEL AND CONTPOL	PAA-121 D6-1048	AA-123 D6-2757	CAL_124 D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AP-328 D6-2761	SAB-329 D6-2760	TWA-331	105-7-130 106-2764	BOAC-136	AII 437 Do-2752
73-1	Engine Fuel Control Unit	Pu X													
73-2	Eng.ne Fuel System Block Diagram	VI, X					_								
73-3	Fuel Manifold Schematic	×											-		
73 - la	Fuel Nozzle Schematic Cutaway														
73-1		X													
73-€	JFC=12 Hydromechanical Fuel Control	×													
73-7	Pressurizing and Dump Vaive	E" X									L				
73-8	Fuel Pump and Fuel Control Quick - Disconnect	V.X	L												
73-9	Primary and Main Fuel Flow V - S MPM	\ \\ \\ \\						1							
73-10	Fuel Pressure Indicating System Schematic	×		-											
73-11	Fuel Control Functions Schematic	PU- X													

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A.(T CRDER NUNBER	SECTION 74 .	PAA-121 D6-1048	AA-123 D6-2757	CAL_124, D6-2756	TWA-131 D6-2758	UEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUTT-130 D6-2764	BOAC-136	AII-437 D6-2762
71,-1	Engine Ignition Diagram	X					L	L							
74-2	Engine Ignition	A A													
74-3	Engine Ignition System Installation	×													
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4		SECTION 75	PAA-121 D6-1018	AA-123 D6-2757	CAL_124 D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BNP-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	1011-130 D6-2764	BOAC-136	ATI -4.37 D6-2762
The section of the se	75-1	Engine Air Distribution - Lest Side	B						-						L	
The state of the s	75-2	Engine Air Distribution - Right S'de	A						L							
	75-3	Surge Bleed Control	90 ×									-				
-	75-4	Surge Bleed Governor	, ×							H	Ч	4				L
	75-5	Thrust and Start Levers	şı. X							×	H					
-	75-6	Engine Compressor Bleed System	×				Ч	- 4	Ч	Ч		-		-	L	
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A H.T. ORDER NUMBER	SECTION 76 ENGINE CONTRILS	PAA-121 D6-1048	AA-123 D6-2757	CAL_121, D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-2764	BOAC-436	AII 4.37 D6-2762
76-1	Engine Throttle Controls	4							L				L		. (
76-2	Engine Tachometer	X										L	L		
76-3	Engine Control Cables	PVX										L			L
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	ART ORDER NUMBER	SECTION 77 ENGINE INDICATING	PAA-121 D6-1048	AA-123 D6-2757	CAL_124 D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BNP-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-430 D6-2764	BOAC-L36	AII-437 D6-2762
	77-1	Engine Pressure Ratio System Schematic	ζ'. ×													
de la companya de la	77-2	PRESSURE RATIO TRANSMITTER SCHEMATIC	\boxtimes								L	L				
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AHT ORDZR ATMBER	SECTION 78 EXHAUST	PAA-121 D6-1048	AA-123 D6-2757	CAL_124, D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	1.077-130 06-2764	BOAC-136	AII-437 D6-2762
78-1	Jet Exhaust Velocity	X	X	X	X	X	L	X	×	×	X	X		5# X	X
76-2	Jet Exhaust Temperature	X	X	X	X	X		X	×	×	X	X	as X	X	X
78-3	Typical Operating Velocities	×	×	X	X	X		X	X	×	X	X	PIN X	X	X
78-4	Typical Operating Temperature	X	X	X	X	X	L	X	X	×	X	×	? · X	, X	30 X
78-5	Reverse Thrust and Noise Suppressor	×			H				Ť	4	Î	-	-		
78-6	Engine Exnaust Temperature Indicating System	Pu X				Ч		4	H		4			4	
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	S. Carrie	SECTION 79	PAA-121 D6-1048	AA-123 D6-2757	CAI_124 D6-27>6	TWA-131 D6-2758	JEA-138 D6-2763	CUB-139	Br.F-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUTT-130 26-2764	BOAC-436	AII-437 D6-2752
79	-1	Engine Oil System Schematic	PLUX			L			1_							-
79	-2	Engine Oil Cooler and Bypass Valve Assembly	X	X										L	T	TE
79	- 3	Oil Pressure Indicating System Schematic	, X										L			73
75	-4 -	Engine Oil Ground Gooling Control	() ^A								Ч	4		Ц		TIE
79.	-5	Engine Cil Tank	X								4	Н		Ч	4	
79-	-6	Oit Cooler Ejector Valve Override	A				4		4	Ц					H	
79	-7	ENGINE OIL DISTRIBUTION	X										H	L		
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AET ORDER NUMBER	SECTION 80 .	PAA-121 D6-1048	AA-123 D6-2757	CAL_124 D6-2756	TWA-131 D6-2758	QE4_138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	1017-130 16-2764	BOAC-136	AII -437 D6-2762
50-1	Engine Fuel - Air and Pneumatic Starter System	, » X							·						
8042	Engine Start Circuit	- X													
b0 - 3	Engine Pneumatic Starter Control System	/4			-										
∂0=l;	Air Turbine Starter	V													
60-5	Starter Clutch Schematic	A													
80-6	STARTER AIR DISTRIBUTION	×											-		
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		4	-4												
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AHT ORDER NUMBER	SECTION 27 Cont.	PAA-121 D6-1048	AA-123 D6-2757	CAL_124 D6-2756	TWA-131 D6-2758	154-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-2764	BOAC-136	A11-437 D6-2762
27-23	Elevator Snubber Assembly	Р.И. 🗵													
27-24	Rudder Control System	, . X	esp												
27-25	Rudder Pedal Adjusting	9 , X													
27-26	Rudder Gust Damper Details	p.u X						-							
27-27	oudder Trim System	A													
27-28	Stabilizer Trim Control System	X	-												
27-29	Stabilizer Trim Control Details	PU X						E							
27-30	Stabilizer Trim Circuit	A			-										
27-31	Flap Drive Ball Screw Nut Details	50 X					4.	, L		-					
27-32	Tab Follow-up and Internal Balance Panel Mechanism	×													
27-33	Stabilizer Trim Actuator Mech- ism Details	×													

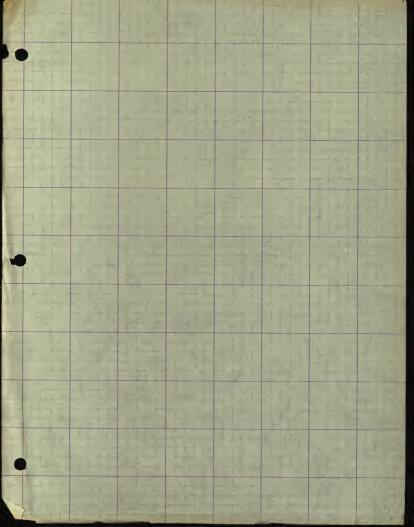
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AT OROER NUMBER	SECTION 26	PAA-121 D6-1048	AA-123 D6-2757	CAL_124 D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	1077-430 06-2764	BOAC-136	AII -437 D6-2762
24-1	Engine Fire Detector	2				L_				X	- 7 X	3 X	3-1X	. 2	n3 N
25-2	Engine Fire Extinguisher System	P		712	70 6	(3° K2	3 2	×	7	-	3 4	(. L			
2(-3	Engine Fire Extinguisher System Control	p.u X													
26–4	Engine Fire Detector Control Unit	6.0 🗙													
245	CANCEL CANCES Digine Fire Extinguishing System														
26-6	Engine Dire Switch Schematic	A A		.											
26-7	Fire Detection and Extinguish- ing Systems		ļ L.		-									-	
26-8	Fire Extinguisher Bottle and Valve Diagram				-		-		-				1		
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ART! ORDER NUMBER	SECTION 25 Cont. EQUIPMENT AND FURNISHINGS	PAA_121 D6_1048	AA-123 D6-2757	CAL_124 D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BKP-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-430 D6-2764	BOAC-136	A11-437 D6-2762	
25-45	Observer's Seat	X		X	×	\boxtimes	×	×	X	X	X		×			
25-46	Flare System II	×	X		×	\boxtimes	X	X	K	10		A				
2:-47	Attendants' Seat	X	L	L_		L	<u> </u>		X		L			L-		
25-48	Passenger Double Seat with Table		×			-						<u> </u>		L		
25-49	Passenger Double Seat - Luxury		L		X											
25-50	Passenger Triple Seat - Luxury		K									L	*			
25-51	Passenger Triple Seat Tourist		L		X								355			
25-52	Emergency Exit Escape Rope Installation	X	×		K	×		X			×	. K				
25-53	Control Cabin Bulkhead _ Equipment Location	×														
25-5h	Overhead Rack	×	X	X	X	×	×		Z	×			×		4 >	4
				-										1		1

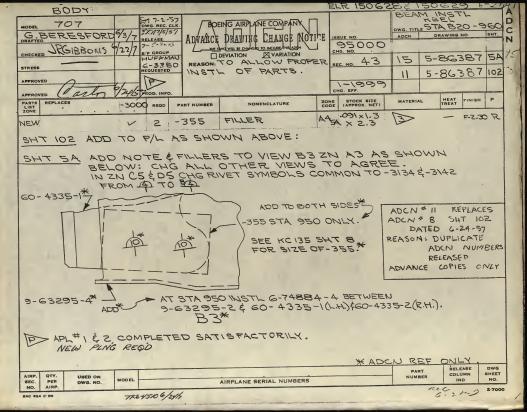
ANT ORDER NUMBER	SECTION 25 Cont.	PAA-121 D6-1048	AA-123 D6-2757	CAL-12h D6-2756	TWA-131 D6-2758	UEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-2764	BOAC-136	AII 437 D6-2762
25-34	Passenger Cabin Floor Covering	×													
25-35	Passenger Cabin Floor Covering Details	×				L									
25-36	Control Cabin Floor Installation and Covering and Details	×										Ĺ_			
25-37	Control Cabin													[
25-38	Inflatable Escape Slide	CANCEG									. [
25-39	Inflatable Escape Slide Ejection	×						-							
25-40	Inflatable Escape Slide Packing Sequence -I	X			-										
25-41	Inflatable Escape Slide Packing Sequence - II	X													
25-42	Inflatable Escape Slide Packing Sequence - III	X													
25-43	Escape Slide Stowage	X									L		L		
27-114	Control Stand	XX												Ц	

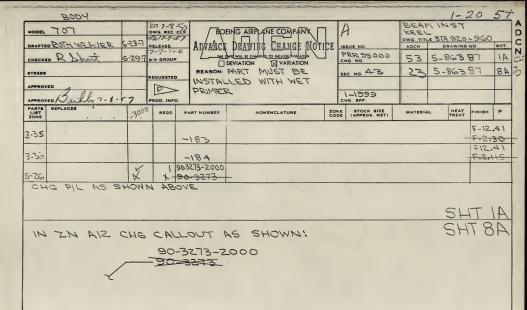
	ART ORDER NUMBER	SECTION 25 Cont. EQUIPMENT AND FUNCISHINGS	PAA-121 D6-1048	AA-123 D6-2757	CAL-124 D6-2756	TWA-131 D6-2758	QEA-139 D6-2763	CUB-139	BRF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-2764	BOAC-136	A11-437 D6-2762
	25-23	Navigation Station raneing	CANCEL													
	25-24	Control Cabin Equipment	X													
	25-25	Lower Nose Compartment Equip- ment	X													
	25-26	Peneral Alegtronic Control	CANCEL													
	25-27	Art Pestronic Control Panel	P" X													
	25-28	Alternate Crew Station Panel		×												
	25 - 29	Mectronic Cooling Air Flow System	611 🗵													
	25-30	Passenger Service Unit	×													
-	25-31	Passenger Service Unit Details	X							×						
	25-32	Navigation Station Arrangement	X													
-	25-33	Seat Tracks	X													

															Principal
An T ONDER NUMBER	SECTION 25 Cont Equipment and Furnishings	PAA-121 D6-1048	AA-123 D6-2757	CAL-12h D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BKF-227 D6-2759	PAA-321	AF-328 D6-2761	3AB-329 D6-2760	TWA-331	D6-2764	BOAC-136	AII-437 D6-2752
25-12	Aft Passenger Section	\boxtimes													
25-13	Aft Lavatory Compartment	82 🗵									-	L			
25-14	Porward Lavatory Compartment	X 8.7. X											-		
25-15	Passenger Compartment Insulati Installation - Typical Cross Section in Window Areas	on 🗵												-	
25-16	Theulation and Sidewall Insulation Suildup-Passenger Compartment Constant Body Section	X													
25-17	Passenger Compartment Insul- ation Installation - Escape Door Area	X			L						-				
25-18	Passenger Cabin Lower Ceil- ing Forward	×													
25-19	stagnists Panel - Att	×													
25-20	A Cheddres Parel & Toward	×						-							
25-21	Observer's Panel	X	X												
25-22	Pilot's Auxiliary Panel	X	X				1.		1	1			1		



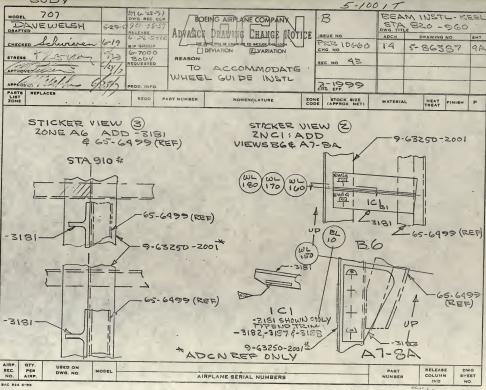
Terminal servicing arrangement,





APL OOI & ON MUST COMPLY

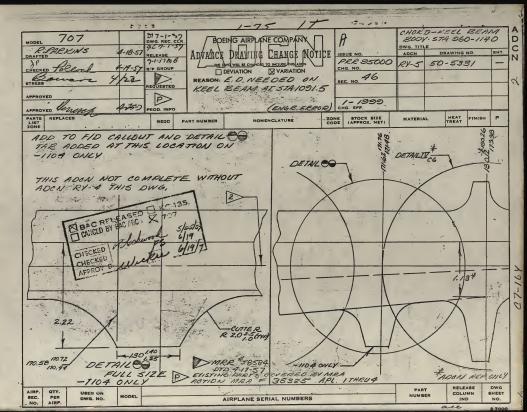
RELEASE DWG AIRP. QTY. PART USED ON COLUMN SHEET MODEL SEC. PER NUMBER DWG. NO. AIRPLANE SERIAL NUMBERS NO AIRP. IND NO.

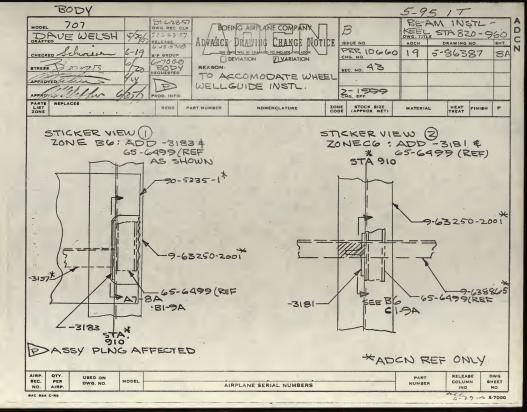


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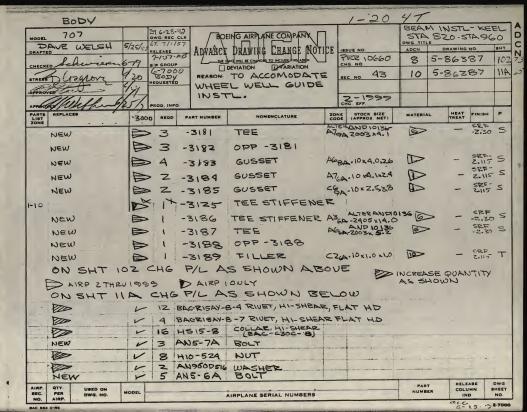


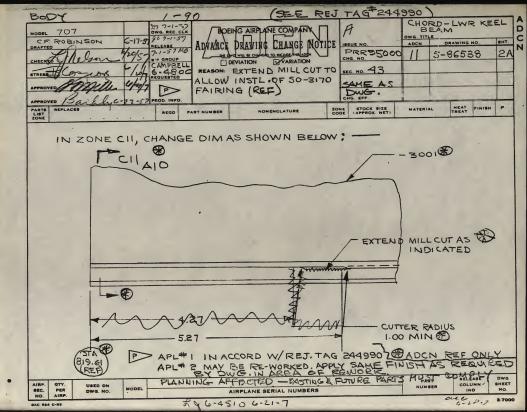


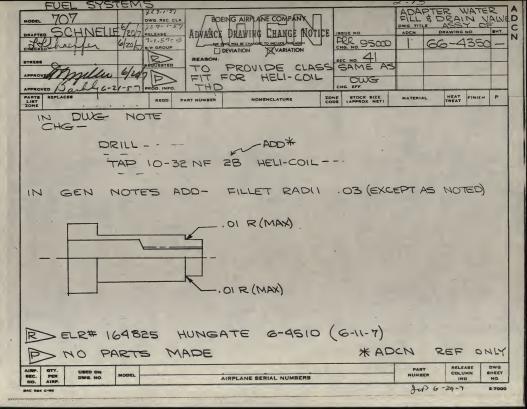
BODY			1.	-/-	25 17				
DAVE WELSH	516-28-57 DWG. REC CLK 5-25-57 K717/1157	- / . \	EING AIRPLANE COMPANY	7	A		M INSTL	96	0
P A	S-1-3 BIP GROUP	ADVANCE	DRAWING CHANGE NOT		PRR 10660	47	5-8638		1A
STRESS DOS LOR	6-7000 BODY	REASON:	TO ACCOMODA		HG. NO.				
CAPPROVEDED	G/ZY REQUESTED	WHEE	IL WELL GUIDE		and the state of the				
whitelelle g	5/) PROD. INFO.	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			2-1999				
PARTS REPLACES LIST ZONE	-3006 REOD PA	RT NUMBER	NOMENCLATURE	CODE	STOCK SIZE (APPROX. NET)	MATERIA	L HEAT	FINISH	Р
I-59		3058	ANGLE STIFFE						
1-56		3055	ANGLE STIFFENE						
1-57 2-72		3056	ANGLE STIFFENE	R					
2-72		2076	STIFFENER						-
2-73			- ILLENEN						
-3055	₽ 1 -3	3175	ANGLE STIFF		-1407x15,0	6		SRF -2.30	S
-3056	B 1 -	3176	ANGLE STIFF		-1407x15,2	6	-	4	5
-2075	DI -	3177	STIFF		-1407 XIA3	6	-		2
-2076	D 1 -	3178	STIFF		AND 10139 -1407 14.4	6	-	- 1	R
-3058	D 1 -	3179	ANGLE STIFF	CBA	-1407 × 14.3			2.30	\$
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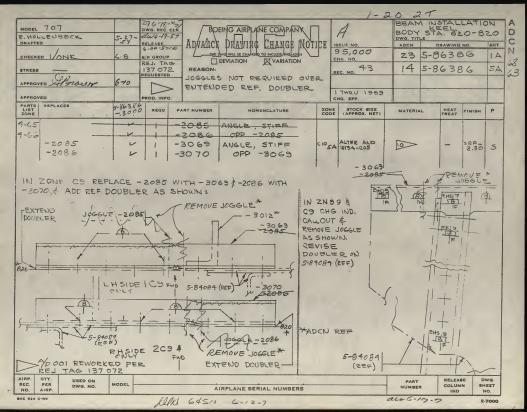
SEE ALSO ADEN 8 ON SHT 102 \$ ADEN 10 ON SHT 11A

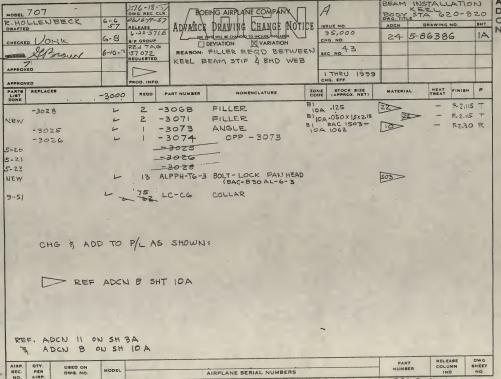
AIRP. OTV. USED ON SC. PER DIME OF MODEL PART RELEASE DWG								
NO. AIRP. AIRPLANE SERIAL NUMBERS IND NO	SEC.	PER	USED ON DWG, NO.	MODEL	AIRPLANE SERIAL NUMBERS	PART	COLUMN	SHEET











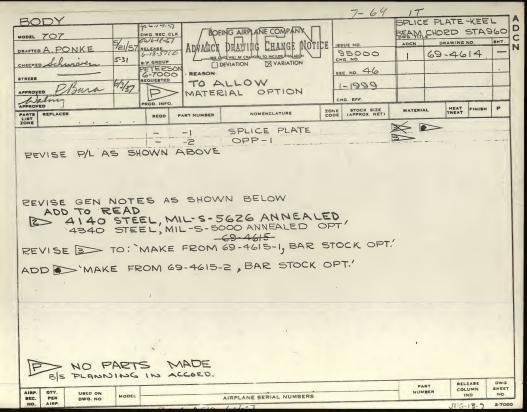
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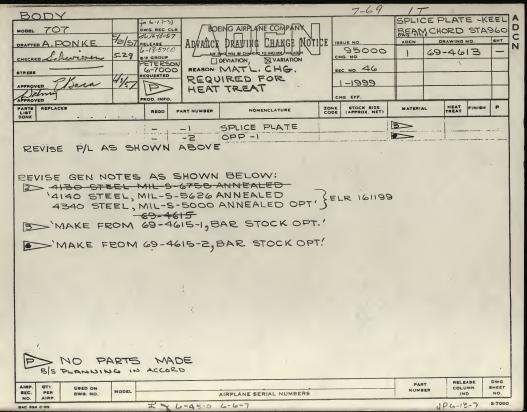
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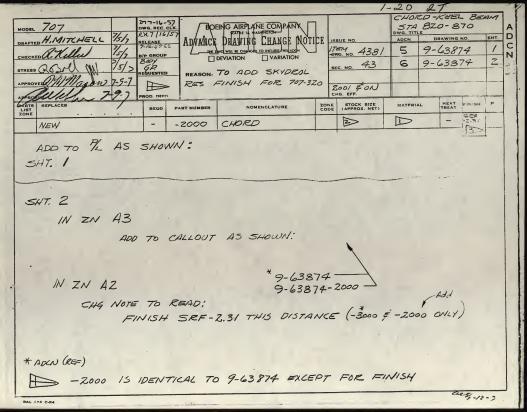
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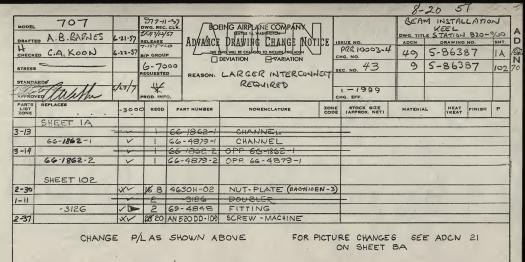
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► 1 THRU 199 ¢ 301 THRU 1999

SCRAP EXISTING PARTS

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PRESS. Pg:	TUBE ASS	r _ =	END FITTING	SS PER TUBE AS	SY	ZONE	OD	THICK	MATERIAL	TREAT	FINISH	IDENT-	TYPE	LGTH

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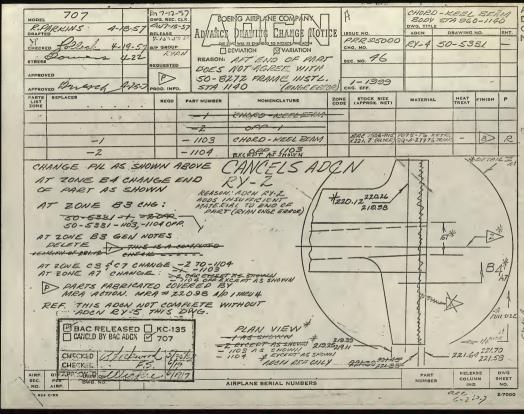
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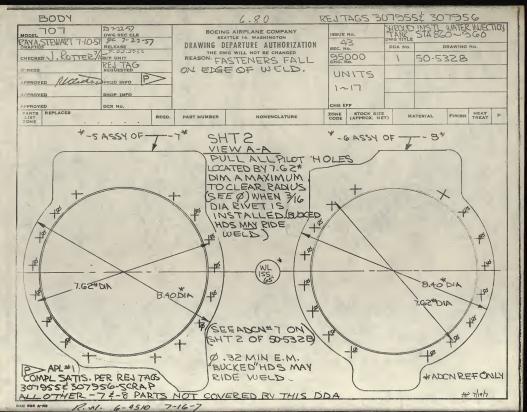
	DBATTED DOUG PRATT 3-217 CHECKED 7 I North 1/2/57 STRESS 14. E. Eryant 4/5/57	M. FALCONES	BOEING AIRPLANE COMPANY ADVANCE DRAWING CHANGE NOTICE TO EVIL BE CONCEDED TO SECURITY OF THE PROPERTY OF THE		155UE NO. 46621 CHG. NO. SEC. NO. 46		CHORD - KEEL BE. BODY STA 960- DWG. 1711E ADEN DRAWING NO. 3 50-5331 5 50-5331			- Company of the last
	APPROVED AND A-7-) P	ROD. INFO,	1-1999		HG. EFF.					-
	LIST ZONE	REQD PART NUMB	ER NOMENCLATURE	CODE	STOCK SIZE (APPROX. NET)	MATERIA	TREA	FINISH	Р	ı
		1		1.1		120				mill.
	NEW	3	OPP-1103		100	- 10		1.		ı
	IN PL ADD -3 AS SHOWN ABOVE. IN ZONE B7 UNDER "PLAN VIEW" ADD: "-3 OPP - 1103" IN ZONES BZ X B-7 ADD: "-3 OPP"									
Taxable or an annual section of the	REPLACES ADON 3 REASON: TO REMOVE - 2 FROM P/L & CHANGE CALLOUT - 1 TO - 1103 DR AFTED: G. McDONALD 6/15/57 CHECKED: FRILLMAN. 6-18-7									

APPD BY: Wieke 6/19/7 REQD' SHERSON 6-7000 PROD INFO : DWG. CLARIFICATION ONLY

IN TAB, BLOCK CHG ENTRIES AS SHOWN BELOW:

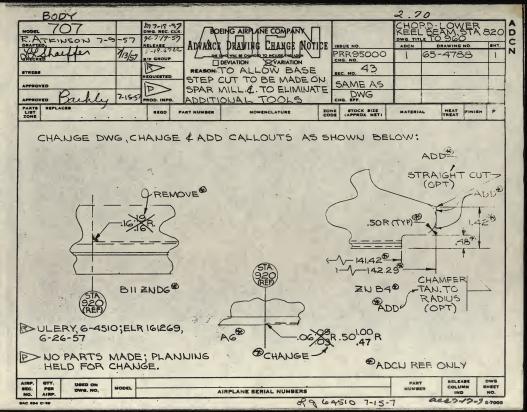
-							
46	-	50 7933	707	1 1999	50-5331-2		
46	×	50-7933	707		50-53311/03		1
SEC.	QTY. PER AIRP.	USED ON DWG. NO.	MODEL	AIRPLANE SERIAL NUMBERS	PART NUMBER	RELEASE	DWG SHEET
BAC 924	C-RS					IND	NO.

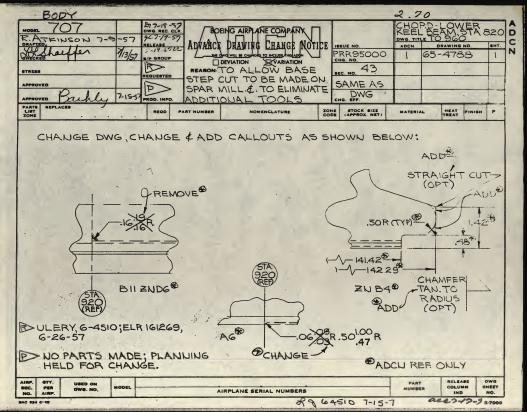




DRAFTED A B. BARNES REL	7-18-57 5 REC CLK 7/19/57 EASE UNIT	DRAWING DEPART	WASHINGTON	PRE 10003-4 	BEAN DWG TITLE	STATION DRAWN	820-560
STREES REG	DE INFO		ITER CONNECT UIRED	1-3		·	
PARTS REPLACES		REQD. PART NUMBER	NOMENCLATURE	ZONE STOC	K SIZE	MATERIAL	HEAT TREAT FINISH
ZONE	DDA DR	AWING 69-	5371 SHTS	122			

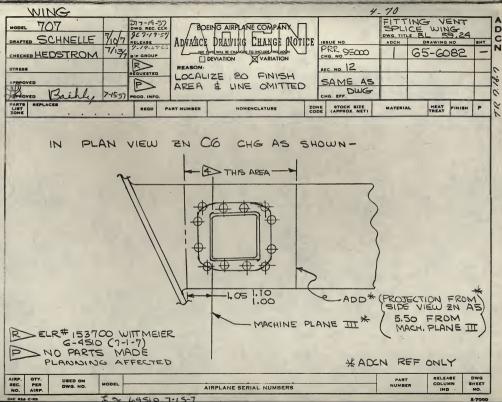
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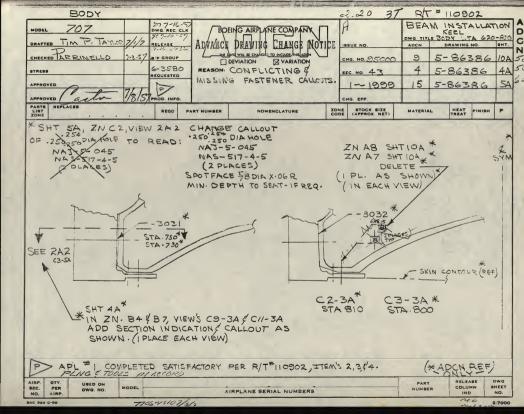


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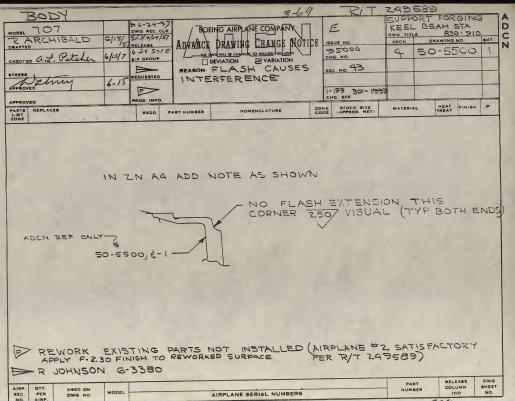
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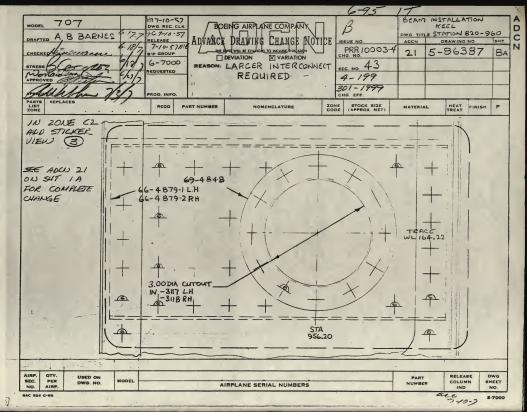


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ORIGINATOR SCHWELL 41: APP WALLOWN SCHWELL APP WALLOWN SCHWELL DEPT 6-4800 BOX NO. 90-1	93 ENGINEERING LIAISON REG	DUEST PLANNING BOX NO. 9/1-90 ZONE STOCK BIZE CODE (APPROX. NET)	PHONE S44-7 MATERIAL HEAT FINISH P (-2.115)
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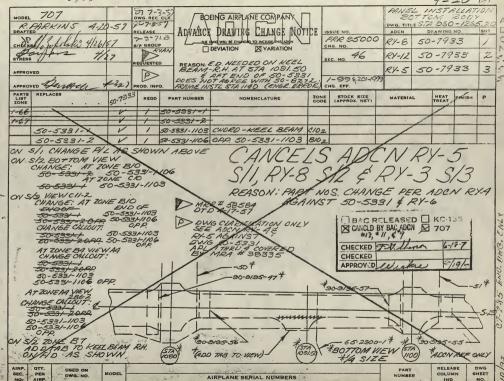


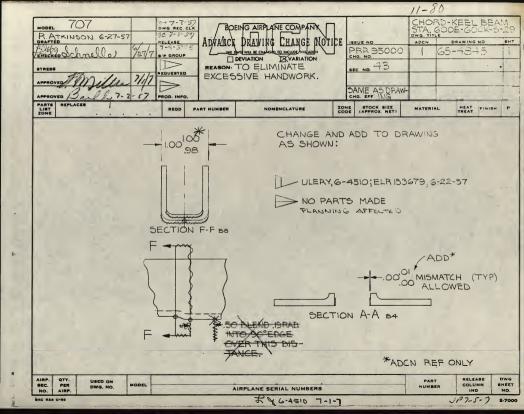
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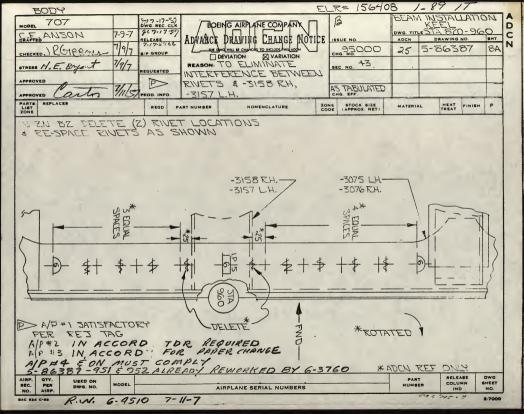
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- 55			1	6-83517	ANGLE STIFF	(8)						
3-64	_		1	6-83517	ALXIC STUTIE	38	s -					
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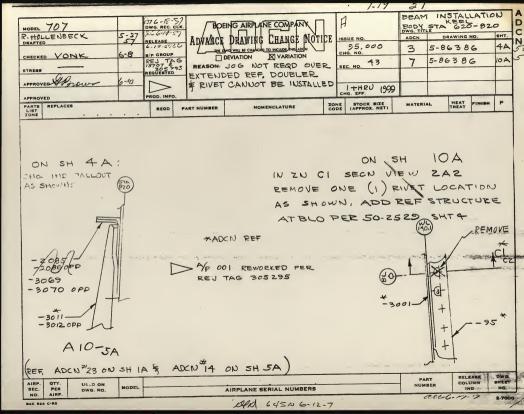
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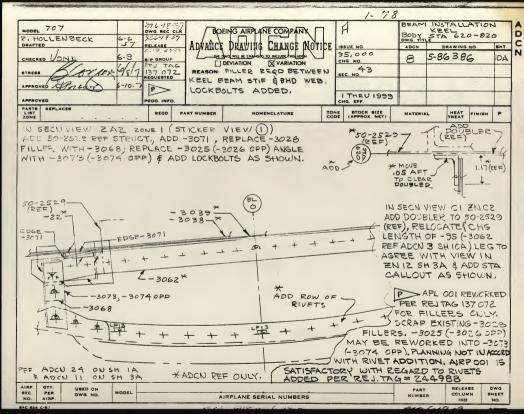
1 6-83517 ANGLE STIFF

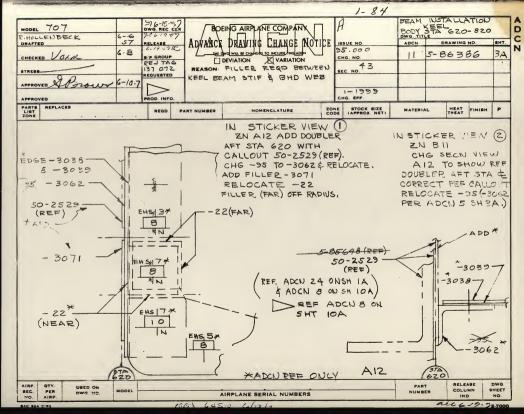
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OHECKED (LECT	(-15-5)	B/P GROUP		DEVIATION AVAILATION		PRR 95000 EHG. NO. 43	-5	3-00.	,	11		
STRESS		REQUESTED	FOR	SKYDROL	ľ	SEC. NO.						
APPROVED Bailly 6-15	-57	PROD. INFO.	NREA	`		1-1999 CHG. EFF.						
PARTS REPLACES	300	REOD	PART NUMBER	NOMENCLATURE	ZONE	STOCK SIZE (APPROX. NET)	MATERIA	AL HEA	FINISH	P		
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DETAIL PLNG, AFF.

AIRP. SEC.	QTY. PER	USED ON DWG. NO.	MODEL	AIRPLANE SERIAL NUMBERS	PART NUMBER	RELEASE COLUMN IND	DWG SHEET NO.
NO.	AIRP.					1316	+ 9.7000

1-75-15 \$77-16-57 707 COWL PANEL ASSY A BOEING AIRPLANE COMPANY L.H. SIDE, ENG NAC B. HANSON CHANGE MOTICE ADCN DRAWING NO. SHT 10749 6 5-85637 IA W/P GROUP CHG. NO. PAR **F1 DEVIATION** VARIATION DONALDSON REASON: TO PROVIDE SEC. NO REQUESTED CLEARANCE FOR THE 1-199 \$ THRUST REVERSER 301-1999 ACTUATOR CYLINDERS PEOD INFO PARTS LIST ZONE -3000 REPLACES PEOD DART NUMBER NOMENCLATURE STOCK SIZE HEAT MATERIAL FINISH -3035 -3070 -3086 FRAME .045×6.0 B F-503 STA 205.00 ×60.0 10.10 -3075 -3072 -3087 CHANNEL F4100 .045× 3.0 F-503> ×4.0 10.10 -3088 TIE PLATE .045×2.20 F -3074503 × 10.50 1010 7-24 TIE PLATE 3074 -3040 -3089 FRAME DII .050×4.00 SRF 501> T4 100 STA 125.04 ×45.0 12.207 1-24 FRAME - STA 205 7-15 CHANNEL 1-15 FRAME - STA 125.04 CHANGE PI AS ABOVE REWORK EXISTING PARTS 407/13/7 AIRP. QTY. USED ON RELEASE SEC. PER MODEL

AIRPLANE SERIAL NUMBERS

COLUMN

NUMBER

SHEET

NO.

BAC #24 C-RS

AIRP.

IOWER SPAR 277-16-57 DWG. REC. CLK INSTALLATION 707 MODEL BOEING AIRPLANE COMPAN' DWG. TITLE OUT BO STRUT 8417-17-5 DRAFTED GT. OSTERLOH 7/9/7 ISSUE NO. ADCN DRAWING NO SHT. 7-18-57 200 PRR 10453 8-8122 CHECKED T. BURDO 2A VARIATION SHE NO. DEVIATION DONALDSON 8-8122 IA 6-7000 REASON: ADDED HOLES REQUESTED FOR FIRE NUTPLATES 7/1/52 - 199 € 301 DETECTOR INSTI THRU 1999 PROD. INFO. CHG FFF REPLACES PARTE ZONE STOCK SIZE MATERIAL REOD PART NUMBER NOMENCLATURE FINISH LIST BAGNIOL A-ASSNUTPLATE (70LHAI-02) FLASTIC STOPNUT CORE AN520-10R6 SCREW, MACH CHANGE PIL IN SHT IA AS SHOWN ABOVE CHANGE PICTURE IN SHT 2A AS SHOWN BELOW MA (IOPLACES) 3004* -3007* AN 520-10R6 (3 PLACES) -218.228 DIA. HOLE (3 PLA KES) AN 520-10RG (5 PLACES) 218228 DIA, HOLE(5 PLACES) 2.0 4.20* BAC-NIOLA-38 (5 PLACES) MA (TYP 3 PLACES) PLAN VIEW* BAC-NIOLA-38 FWD-(3 PLACES) 3003* STA 136 ADCN REF. * AIP 7/15 RELEASE DWG AIRP PART USED ON COLUMN SHEET MODEL BEC PFR NUMBER DWG. NO. AIRPLANE SERIAL NUMBERS IND NO. AIRP PAC 984 C-RS

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PAR' LIS ZON	S REPLACES	-30A2	-3041	-3002		REQD		RT NUMBER	NOMENCLATURE	ZONE	STOCK SIZE	MATERIA		HEAT	FINISH	P	17 6.
6-15	-		-3043	1	-3003	21	9-6	1760-5	ATTACH ANGLE	C008	(APPROX. NET)			TREAT		1	1
6-2		3014		-3004 -5004		1	9-61	760-6	OPP 9-61760-5		3				- 3	-	
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SEC.	PER	DWG.		MODE		***						PART		RELEAS		wa I	

2.20 47 707 BULKHEAD INST. 27-16-57 BOEING AIRPLANE COMPANY DWG. REC. CLK MOUNT INED NAC STA 136 EZN 1/17/57 6/21/2 DRAFTEDG. OSTERLON RELEASE ADCN DRAWING NO. ISSUE NO. 7-18-5720 PRR. 10453 4-5177 2A CHECKED T. BURDO E/P GROUP SHE NO DEVIATION VARIATION DONALDSOA 11 1A REASON: TO PROVIDE 4-5177 STRESS 6-7000 SEC. NO. 72 REQUESTED CLAMPING FOR FIRE (Venalder 1 THRU 199 DETECTION ELEMENT PROD. INFO CHG. EFF. PARTS REPLACES 3000 ZONE STOCK SIZE LIST REQD PART NUMBER NOMENCLATURE MATERIAL FINISH SPACER NUT WS1-32-C NEW BAC-NIODZ-3- O CHANGE PIL IN SHT IA AS SHOWN ABOVE. PLACES - 73108-1(REF) (2 PLACES) NULT SPACE 1.0% 2 PLACES WESTERN SKY INC. P. O. 300 HAYWARD CALIF LIH. SIDE VIEWNA REAR VIEW* CHANGE PICTURE IN SHT ZA AS SHOWN ABOVE AIP 7/15/7 ADCN PEF ONLY AIRP USED ON RELEASE PART PER MODEL DWG. NO. COLUMN SHEET NUMBER AIRPLANE SERIAL NUMBERS AIRP NO. IND NO.

BAC 924 C-RS

COWL PANEL ASS' 817-16-5 707 BOEING AIRPLANE COMPANY MODEL DWG. REC. CLK R.H. SIDE, ENG NAC SW7-17-57 B. HANSON 6/28/07 ADCN DRAWING NO SHT 7-18-5786 10749 6 5-85638 IA CHG. NO. PRR R/P GROUP VARIATION [] DEVIATION 6-7000 SEC. NO DONALDSON REASON: TO PROVIDE STRESS REQUESTED 14 Jonaldson CLEARANCE FOR THE 7/11/57 1-199 € THRUST REVERSER 301-1999 CHG. EFF. ACTUATOR CYLINDERS PROD. INFO REPLACES PARTS 5-85638 STOCK SIZE PART NUMBER MATERIAL FINISH REOD NOMENCLATURE LIST -3000 CIOZA FRAME -.045×4.00 -3023 -3040 -3083 503 10.10 STA 205.00 × 57.00 LATCH CHANNELES .045×300 F-R -3070 -3050 -3084 503> × 15.00 1010 08,000.045×2.70 F--3085 TIE PLATE R 503 -3056 x 10,50 10.10 TIE PLATE C9100 .040×1.50 SRF-XV 2 1 - 30.56 503 ×2.05 2.115 3040 1 3023 1-24 1-71 -30.60 3070 SRF- R C.5 BAC 15/17-1112 FRAME - STA 501 1 X -0014 · 70.00 124.90 .050 ×4.00x SRF -3014 -3085 FRAME - STA 124.50 C5 501> 12,207 R 70.00 3015 050×4.00 FRAME - STA 134.40 BG 50> 5RF T4 12.207 R -3015 -3088 70.00 2016 3037 050×4.00 86 -3087 FRAME-STA192.80 50D F-10 -3016 -3037 T4 R 71.00 EXISTING PARTS REWORK AP7/13/7

AIRPLANE SERIAL NUMBERS

AIRP SEC. NO. BAC 934 C-RE

PER

USED ON

MODEL

RELEASE

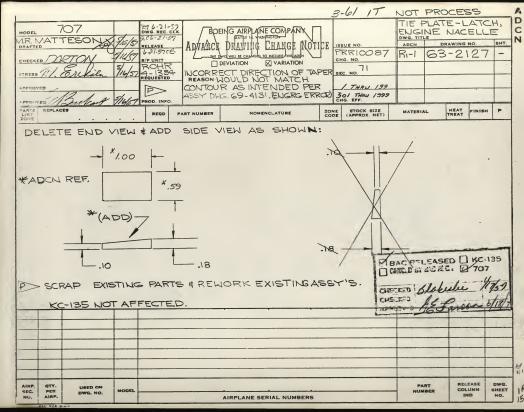
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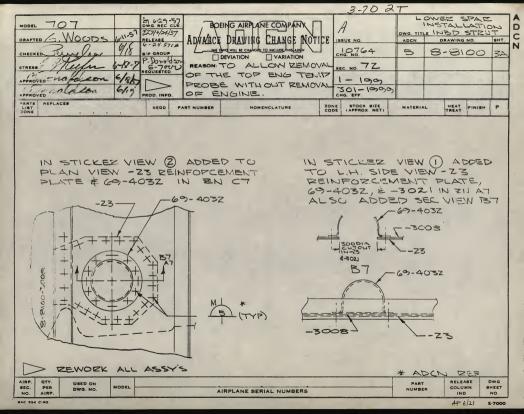
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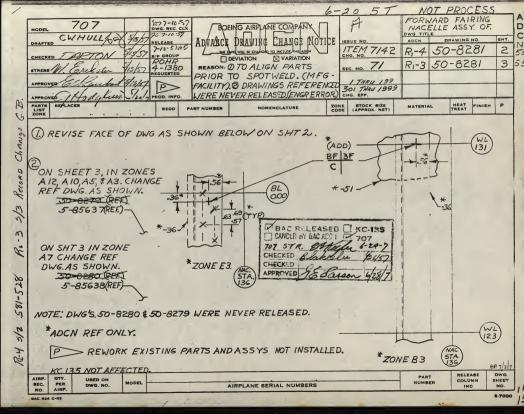
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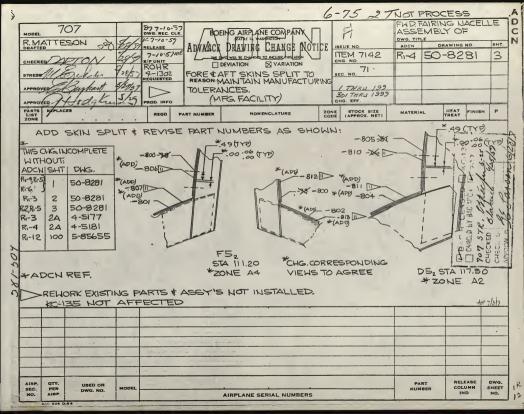
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1-20 MODEL 707 BULKHEAD INSTALATION 07-16-57 DWG. REC. CLK BOEING AIRPLANE COMPAN OUTBO NAC. STA: 136 DRAFTED G. OSTERLOH 7-2-57 RELEASE DRAWING NO. ISSUE NO. ADCN SHT. PRR. 10453 4-5181 2A CHECKED T. BURDO E/P GROUP CHE. NO. [] DEVIATION VARIATION MONALDSON 4-5181 IA PROVIDE 5-7000 REASON: TO SEC. NO. 74 STRESS CLAMPINICA FOR FIRE 1/1/2 APPROVED Donaldson 1-THRU 199 DETECTION ELEMENT 301 THRU 1999 PROD. INFO CHG. EFF. PARTS REPLACES LIST STOCK SIZE BEOD PART NUMBER NOMENCLATURE MATERIAL HEAT FINISH CODE TREAT NUT SPACER WS1-32-C BAC-NIODZ-3-0 SHIT CHANGE P/L IN (2 PLACES SHOWN ABOVE. 6-73108 WS1-32-0 (2 PLACES) 711-.75 1.0 WESTERN SKY INC PO. 300 HAYWARD CALIF REAR VIEW* BL PICTURE IN SHT ZA ABOVE CHANGE AS SHOWN ADON REF ONLY AP 7/15 OTY. RELEASE DWG USED ON PART PER MODEL COLUMP SHEET DWG. NO. NUMBER AIRPLANE SERIAL NUMBERS NO. NO









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MODEL 707 DRAFTED CW HULL S 4/5 CHECKED AFTON 6/6 STRESS HECHT 6/6/5 APPROVED APPROVED PARTS REPLACES 20HE	RELEASE ADVANCE DR	AIRP ANE COMPANY AMING CHANGE NOTING EVARATION ELIMINATE ENCE OF UNIVERSA TS & G5-5C78 (ENGRERR)	EEC. NO. 7/42 SEC. NO. 7/ L. THEM 129 301 THE 129	R,-6 50	FAIRIN ASSEMEDIE PERAWING NO. 1-828	5LY
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PARTS REPLACES - 10-9-8-7/6-5-4		ZONE STOCK SIZE CODE (APPROX. NET)	MATERIAL HEAT	FINISH P
	1 50-5547-4 PLUMBING I	5 (5) 15TL (5) 12 (5) 16TZ (5) 16TZ (5) 16TZ (5) 16TZ (5) 16TZ (5) 16TZ (6) 16TZ (6) 16TZ (7)	JE	
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AIRPLANE SERIAL NUMBERS

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PART NUMBER

AIRP. SEC. NO. AIRP. BAC 924 C-R5

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PER

USED ON

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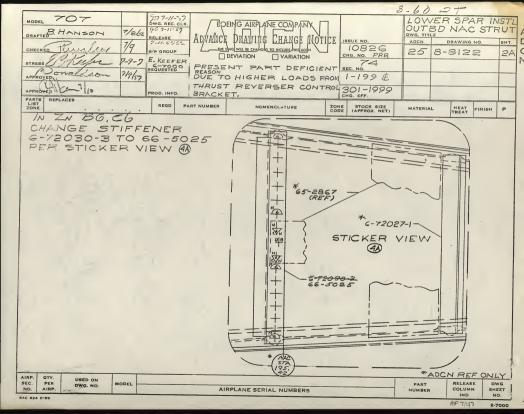
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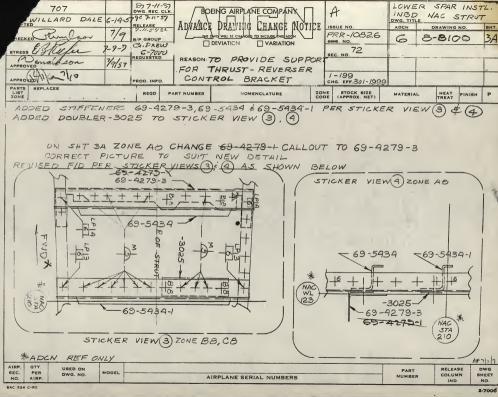
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AIRPLANE SERIAL NUMBERS

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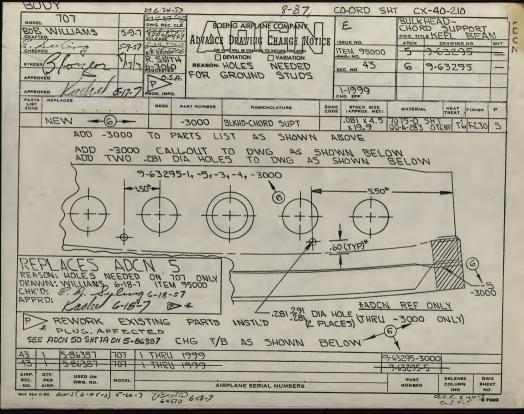
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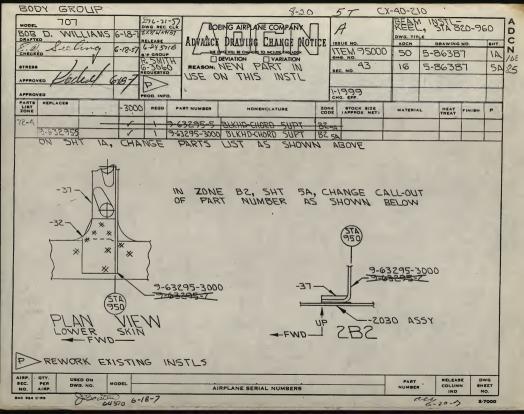




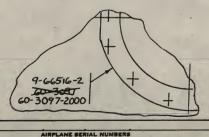
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		115	ADTON	11//	7-/0-57 B/P GROUI	er my much	DWG WILL BE CHANGED TO INCLUDE THIS ADON	1 1	TEM 7255		DRAWING NO	7 I
		26	5/10/	11,	ZOH	2/	DEVIATION VARIATION		HG. NO.	3 65	730	77.6
	STRESS		churs	11/57	4-87	REASON:	ROHP DOES NOT	5	THRU 199			
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	PARTS	REPLACES	rehast	11.10	PROD. INF	o. ALTACI	HIANGLES IN ONE PIEC	E.	HG. EFF.	1 - A	eran.	1
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	NEW	-3		V	1	-803	ATTACH ANGLE FWD	B22	063×10 ×72.			2,20
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	NEW	-6	V		1	-806	OPP-805					
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ı	NEW	-6	V		1	-808	OPP-807		1			<u></u>
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	APP	B: R	why.	フーア-5	-7	ALIAL FILLS	ADCH'S	4	\$ R-25	HTZ.		
t		DELIA	DI E	VICTI	ND DITT	ONAL FINIS			ETTER .	6-4475.3-	5121	
		FLFYC		V1211	74	77121	MS KEP D	AC		ATED 12-20		HP7/5/7
	AIRP. SEC.	PER DI	SED ON WG. NO.	MODEL						PART	RELEASE	DWG
. 1	NO.	AIRP.		-			IRPLANE SERIAL NUMBERS		581-2		IND	NO.
				1					201.6	25	Fr + 18	





	G OSTERLOH	6-6-57	ET 6-21- OWG. REC. EZH 4/21	TYS7 A DUME	EING AIRPANE COMPANY	T.E.	ESUE NO.	INBD NACELLE DWG. TITLE STRUT ADDN DRAWING NO. 8			
CHECKE	F. M. DONNEH	4/7/57	L.24.59	-	DEVIATION VARIATION	P	RR 95000	15	4-5175	1A	
882PT			DNALD	SOU REABON!	TO ADD SKYDR	DL .	EC. NO. 72	17	4-5175	3,	
APPROVE	10) Voralison	5/18	- COURTER	RESIS	TANT FLANGE		THRU 199				
APPROVI	to	-	ROD. INFO			3	OI THRU	1			
LIST ZOME	REPLACES	. 300	8600	PART NUMBER	NOMENCLATURE	ZONE		MATERIA	AL HEAT FINISH	P	
	NEW	1	1	60-3007	FLANGE					-	
	60-3097	4		2000	FLANGE		1				
		OF	60	-3097	1 ON ADON RZ, TO 60-3097-	200	O AS SH	OWN	ABOVE.		



6/20

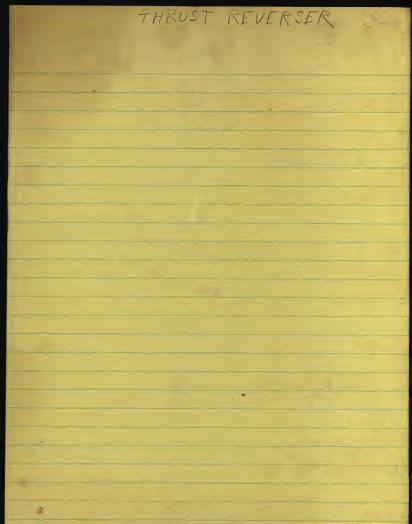
BAC 924 C-RS

6-4510

PART NUMBER RELEASE SHEET NO. IND

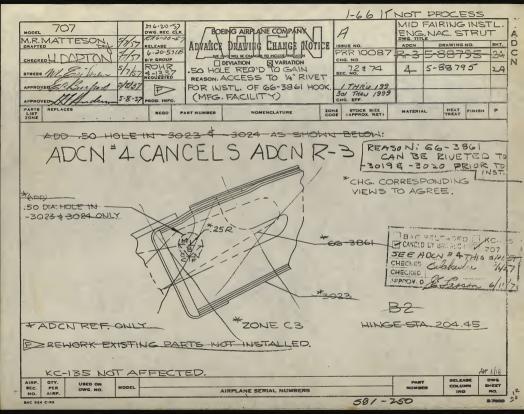
50-8738 Diagram. H - KATE Fr Ext 24 707 Tubing instal Fixtinguisher 182 wing 65-1636 Door Fext access 65-2111 Fr. Detect Main WW 65-2981 4-5177-IA Fire detector inst. 50-10307 Dectect, Inst, Fud cargo 50 - 8253 System Diagram Eng F xting. not released. clamp, detector into strut,

69-3161



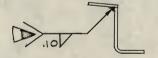
MOST 707 877-17-57 5		/	303	di		
DWG. REC. CKK BOEING AIRPLANE COMPANY	7		IN	LAN	ASHE	
PRAFTED R. HARDING PALLAGE ADVANCE DRAWING CHANGE NOT	The .		DWG. TITE	THR	UST I	KEVER
CHECKED & LOSS OF THE GROUP LANGE TO INCLUDE THIS ADON	The L	TEM: 7815	ADCN 3		WING NO.	SH
DEVIATION VARIATION	- 1	HE NO.	, 3	65	-425	, 2
PLI & CALL OLITE		EC. NO.				
APPROVED PETERSON 116/5)						
APPROVED PROD. INFO.		HG. EFF.			-	
PARTS REPLACES LIST ZONE CONE CONE CONE CONE CONE CONE CONE C	ZONE	STOCK SIZE	1 1	-		_
	CODE	(APPROX. NET)	MATERIAL	TR	EAT PINI	5H P
100 STANING	_					
DEAKING						_
	BOV	E:				
CHANGE CALLOUTS IN ZN'S AB AS	45	SHOW	N BE	ELOV	N: -	
		*				
(66-3718	-37	-				
66-3718-1	3718	3-1				
66-3718	1		180	-37	10-	
66-3718-1	/	1 \	/ 66	-37	18-1	
	\mathbf{V}					
6G-3715*	Π					
000/10	111			-		
		-				
	Ш					
Warnell Second			11			
-66-3715t	UI.					4
ZN AB -65-6394-1*	1	- V	A			
	ZH	A =	5-63	94-	2*	
		~				
SEC. PER DWG. NO. MODEL		1 1	PART		LEASE	DWG
NO. AIRP. AIRPLANE SERIAL NUMBERS	-		NUMBER		LUMN	BHEET NO.
and the second s		10 2 2	The state of the s	00mm 14	6.5	2.7000

SPER TA

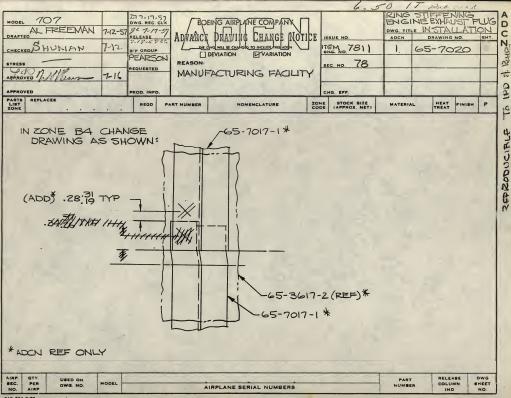


			J.P. M.	2700			6-	50	//			
DRAFTED ALFREDIAN CHECKED HUMAN STRESS AFFROVED APPROVED	DIT 7.17-S) DVG REC CLE PG 1719-G EASE TO THE FORE TO	1	DRAWING D	VIDE OF	AUTHORIZATION DE CHANGED PTIONAL N	6H6. I	No. 1 7811 No. 78	DDA NO.	TAKE!	RAWING	PLU	5
PARTS REPLACES LIST ZONE		QD.	PART NUMBER	NOM	MENCLATURE	CODE	STOCK SIZE	т) м.	ATERIAL '	HEAT TREAT	FINISH	Р

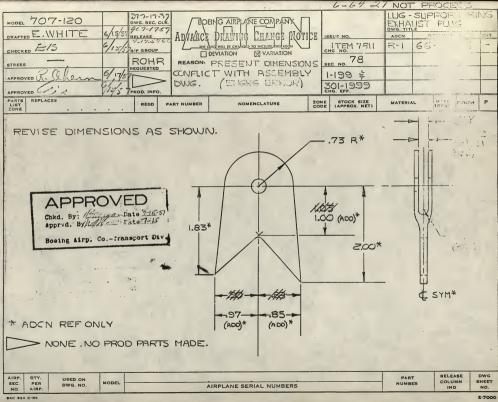
-1, -2, -3 SEGMENTS MAY BE MADE FROM TWO PIECES.



INERT TUNGSTEN ARC WELD PER BAC 5932

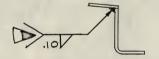


2-7000

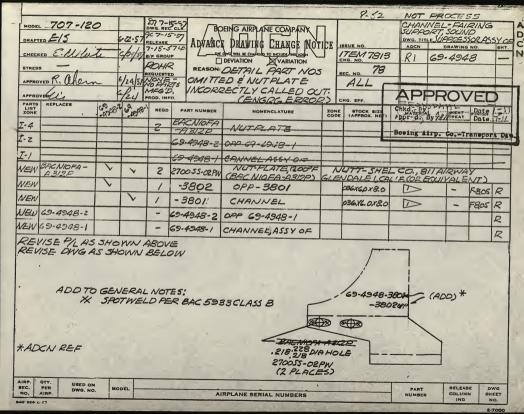


AFPROVED	ALFREMAN ALFRED OF GROUP HUMAN OF GROUP REQUESTED PROD INFO		VIDE OPTIONAL		-	RING, WG TITLE DDA NO.	型版	RAWING	PLU	6
APPROVED APPROVED PARTS REPLACES LIST ZONE	ELR OR DCR	EQD. PART NUMBER	z	CHG EF	STOCK SIZE	M	ATERIAL .	HEAT TREAT	FINISH	P

-1, -2, -3 SEGMENTS MAY BE MADE FROM TWO PIECES.



INERT TUNGSTEN ARC WELD PER BAC 5932



1-54 HREPRODUCIBLE TO IPD & ROKE

MODEL 707	177-15 DWG REC	CLK'			IG AIRPLANE COMPANY			DIRECTIONAL VALVE ASSY EXTEND DWG TITLE THE UST. REVERSE DDA No. DRAWING NO.				
DRAFTED TP. WEED	RELEASE	,			DEPARTURE AUTHORIZATION	ISSUE	No.	DDA No.	D	RAWING	No.	
CHECKED & Vilake JIV	7-15-57 7 B/P GROUP			REASON:	W HI-TEMP	CHG.	.783Z	1	69-4	490	Z	,
STRESS	PEARS	800	۷		IG NOT AVAILABLE	-						
APPROVED 7-11	PROD INFO)		AT TH	IIS TIME.	1	>					
APPROVED PART 7-11	ELR OR DCR				. 3	CHG E	FF					
PARTS REPLACES	(60	7902	REQD.	PART NUMBER	NOMENCLATURE	ZONE	STOCK SIZE (APPROX. NE		TERIAL	HEAT TREAT	FINISH	P
	-	V	-	RAP 3MS-5	(BAS-BIOA-680)		MARLIN					
		V	1	RA3M5	BEARING ROD END BALL		FAFNIR NEW BRIT			214.)		



REMOVE NOW-METALLIC SEALS & REPACK WITH SHELL 21176A SILICODE GREASE.

OPTIONAL: REPLACE NON-METALLIC SEALS WITH

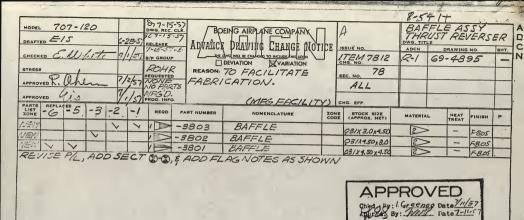


> FIRST TWO UNITS MEGD BY ROHR ONLY

TEFLON SEALS.



FIRST FOUR LINES MEG'D BY IPD ONLY



1 -3803 OPTIONAL TO-78-10

-3802 OPTIONAL TO-8E-11

-3801 OPTIONAL TO - 9 É-12

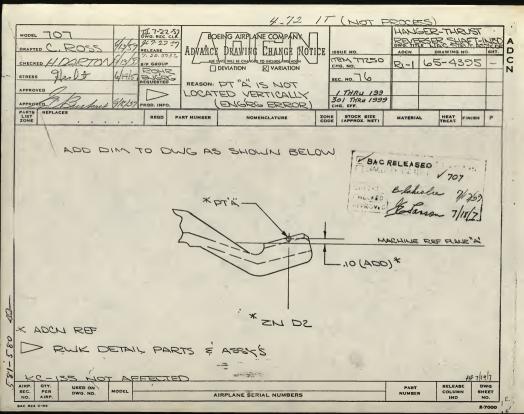
06 P *

* ADCN REF

TYP FOR-3801,-3802,-3803 (SECT 10-10 IDENTICAL TO SECT A-A EXCEPT FOR ONE PIECE CONSTRUCTION >*

AIRP QTY. USED ON PFR MODEL RELEASE pwg DWG. NO. PART AIRP AIRPLANE SERIAL NUMBERS COLUMN SHEET NUMBER IND BAC 924 C-R5 NO.

Boeing Airp. Co.-Transport Div



4-54 17

PARTS REPLACES LIST ZONE		REOD	PART NUMBER	NOMENCLATURE	ZONE		MATERIAL	HEAT FINISH	. P
	7-18-57	PROD. INFO				HG. EFF:			
AFPROVED		1	MEASON	BLOCK UP TO DATE		NOTED			
STRESS		REQUESTED				EC. NO. 51			
CHECKED		BIP UNIT		HE DWG WILL BE CHANGED TO INCLUDE THIS ADON		PRR 9500	2	63-1440	-
DRAFTED CHRISTENSEN	7-17-57	94 7- 22	/ A DALLAND	CE DRAWING CHANGE NO	ICE L	SSUE NO	ADCH	DRAWING NO.	SH
MODEL 707		917-22 DWG. REC.	CLK B	DEING AIRPLANE COMPANY	7	H		RSE THRUST	NO

CHANGE TAE BLOCK TO READ AS SHOWN:

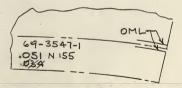
						A	F 7/19/17
	_						
					1		
				<u> </u>			
			_				
51		65-2121	707				
AIRP	QTY-	USED ON DWG NO	MODEL	*	PART	RELEASE	DWG.
NO.	AIRP.	DWS NO		AIRPLANE SERIAL NUMBERS	NOMBER	IND	NO.

MODEL 707		DY 6-21- DWG. REC. 9 26-21-	57 BO	650 2 T REP			DOOR DWG. TIT	THRU	ST	REVER	SSER
CHECKED SHUMAN	6-17-57	BENNET	T INTE	DEVIATION VARIATION	ا	TEM 7813 CHG. NO. 78	ADCN	69-3	354	-	внт.
APPROVED APPROVED	6/19/7	PROD. INFO	ASSE	TO FACILITATE MBLY		CHG. EFF.					
PARTS REPLACES		REQD	PART NUMBER	NOMENCLATURE	ZONE		MATERIA	AL H	EAT	FINISH	P
				ANGLE - LWR	_	.034×10.7			-	F-805	R
		-	-1	ANGLE -LWR	-	.051×10.7			-	F-8.05	R

IN P/L CHANGE STOCK SIZE AS SHOWN ABOVE.

AIRPLANE SERIAL NUMBERS

ON FID CHANGE 69-3547-1 AS SHOWN:

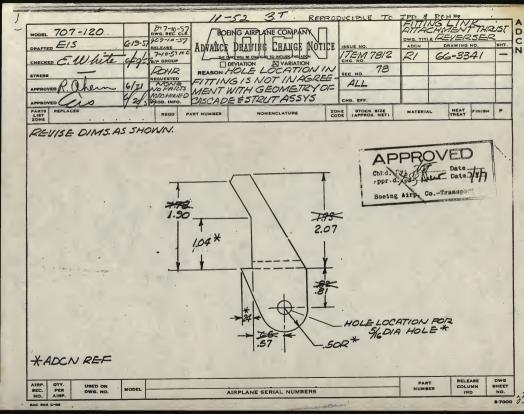


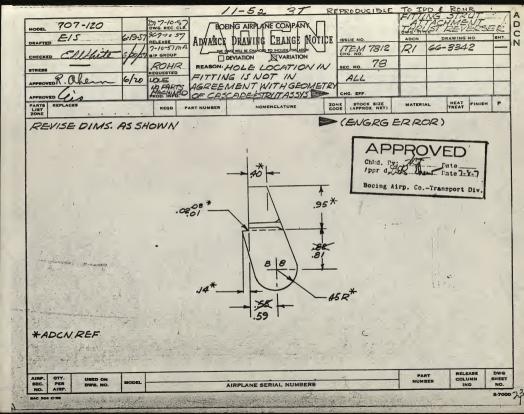
AIRP.	QTY.
BEC.	PER
NO.	AIRP.
725 40	C+00

USED ON

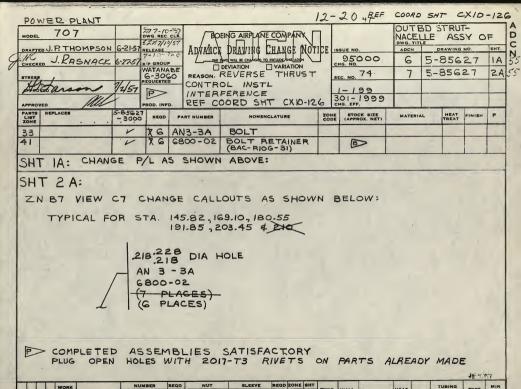
DWG. NO.

MODEL





TO IPD ONLY 4-60,7 REDEADICIRIE BEAM - SUPPOR 277-11-37 DWG REG CLK BOEING AIRPLANE COMPANY 707 MCR No. THRUST REVERSER 817-11-57 DRAWING DEPARTURE AUTHORIZATION SEC NO. 78 DRAFTED M. PUNCO RELEASE DDA NO. DRAWING NO THE DWG WLL NOT BE CHANGED 69-3531 CHECKED Sociale B/P UNIT ITEMT812 REASON: PRODUCTION LPD. TO FACILITATE STRESS/ REQUESTED MANUFACTURE PROD INFO STANDARDS SHOP INFO ALL DCR NO. PARTS STOCK SIZE HEAT ZONE MATERIAL REOD PART NUMBER NOMENCLATURE FINISH LIST (APPROX.) 3041718 69-3531-BEAM x 2.02 69-3531 69-3531-1 BEAM ASSY OF .06 x 12.2 x 2.02 .125x.20 x 8.60 v -2 BEAM V -3 FLANGE ADDED TO P/I AS SHOWN ABOVE! ADDED OPTIONAL ASSY METHOD, AS SHOWN ADDED DIM. TOLERANCES & DA FLAGNOTES. .125 (REF.) OD MISMATCH ALLOWED -3(2PLACES) RY FIRNACE BRAZE ALL MATING SURFACES & INSPECT PER AMS 2675A WITH A - AAMS 4775 HEAT RESISTANT BRAZING ALLOY. TACKWELD (HASTELOY "W" INERT TUNGSTEN ARC) THIS AREA, APPROX 2 SPACING & ENDS. GRIND FLUSH AFTER BRAZING L.20 9.32 9.35 10.35 5.65 5.625.59 10.3210.29



PRESS. TUBE ASSY END FITTINGS PER TUBE ASSY CODE THICK

MATERIAL TREAT

IDENT-IFICATION

TYPE STOCK

			7-5		21				
	77-10-5) WG. REC. CLA.		EING AIRPLANE COMPANY			HING DOO!	R THRUS	REV:	
DRAFTED M. PUNCOCH 6-27-57	ELEASE	1 Antimor	DRAWING CHANGE MOTI	CE Is	SUE NO.	ADCN	DRAW	ING NO.	SHT.
T 111 1/1-1	HOSTINB	The ne	DEVIATION VARIATION		16. NO. 7815	1	65-6	394	-
STATES 11/1/2 7 7/5/21	MO2SA3			SI	C. NO. 18				1.
STANDARDS	E COUESTED	REASON:	FACILITATE PROCUREME	NI					
408 811 7/	ROD. INFO.			cı	HG. EFF. ALL				
PARTS REPLACES	REQD P	ART NUMBER	NOMENCLATURE	ZONE	STOCK SIZE (APPROX. NET)	MATERIA	AL HI	AT FINISH	Р
	- 6	5-6394-1	HINGE FITTING		1.5 ×11.0 ×5:0			F-8.05	2
		ADP :	STOCK SIZE & FLAG A.	s the	DWN:				

CHANGE FLAGNOTE AS SHOWN BELOW:

N-155 CORROSION RESISTANT STEEL BAR PER AMS 5768 B. OPTIONAL HASTELLOY 'X' PLATE PER AMS 5536 A.

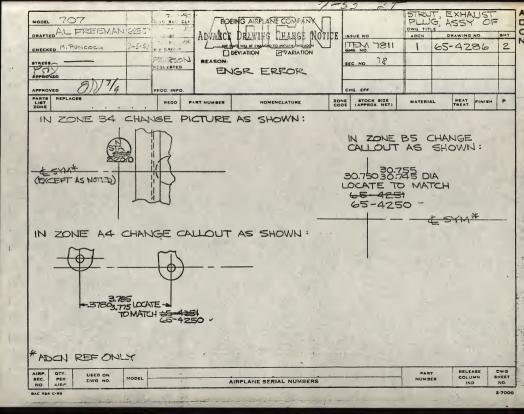
MATERIAL PURCHASED BY P.R. 218848

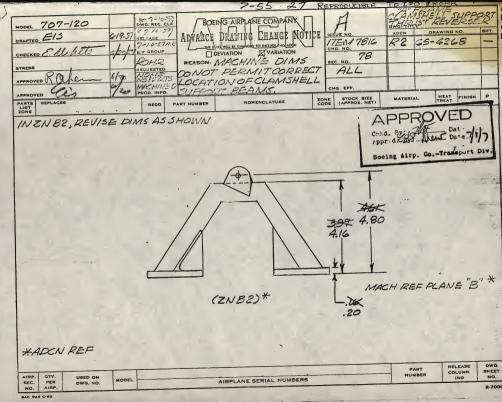
1								-									
ı	Т	Т	WORK	NUMBER	REQD	NUT	SLEEVE	REQD	ZONE SHT	TUBE	WALL		HEAT		TUBING	TYPE	MIN
4			PRESS.						ZONE	OD	THICK	MATERIAL	TREAT	FINISH	IDENT-	ENDS	LGTH
1			PSI	TUBE ASS	Υ	END FITTIN	GS PER TUBE AS	SY	CODE			1			IFICATION		LGIR

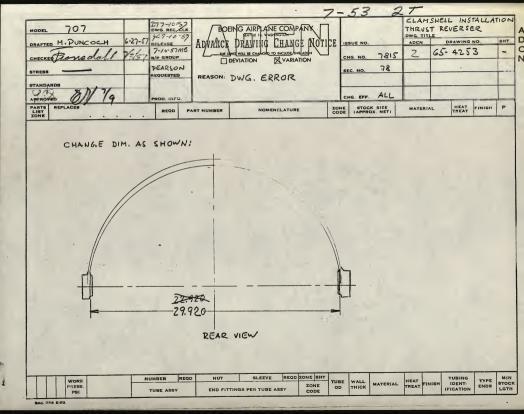
BAC 924 E-R2

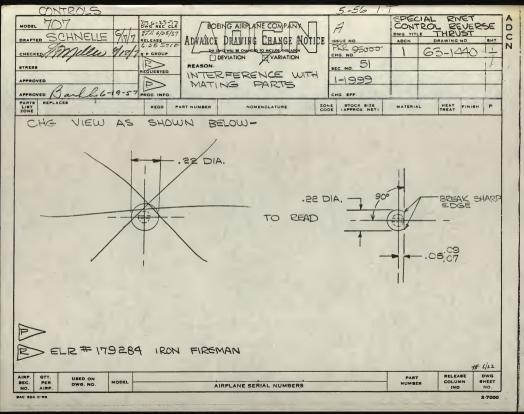
				7-3	55		7				
THRUST MODEL REVERSER	0	WG REC	ER BO	EING AIRPLANE COMPANY	1	4	SLEE	ST	REV	ERSE	
DRAFTED D. KREINER 7-	5-7	ELEABE	A DELANCE	DRAVING CHANGE MOTI	PE	ISSUE NO.	DWG. TIT	LE AS	SSY	OF	SHT.
1	- 63	7-10-5	7416	DEVIATION VARIATION		ITEM 7813	1			90	1
STRESS .		EARSO.	NEASON:	DEVIATION WARRATION		SEC. NO. 7.8			~		
Approved	RE	QUESTE	STRESS	RELIEF NOT REQUIRED.	1	SEC. NO. 7,4			<u> </u>		
APPROVED ON 9/	PE	OD. INFO	o.			CHG. EFF. ALL					
PARTS REPLACES ! /		REGD	PART NUMBER	NOMENCLATURE	ZONI	STOCK SIZE	MATERIA		HEAT	FINISH	P
		-	65-4290	SLEEVE DOOR, ASSY OF	4		1	-		-	
NOTE: CH	ELE	GE	P/L AS RELIEF	SHOWN ABOU	101 VE	NN BEL	ow.				

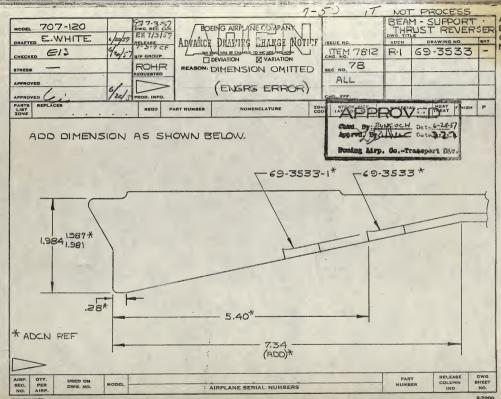
AIRP. QTY. USED ON DWG. NO. RELEASE DWG PART SEC. PER MODEL AIRPLANE SERIAL NUMBERS COLUMN SHEET NUMBER AIRP. IND NO.

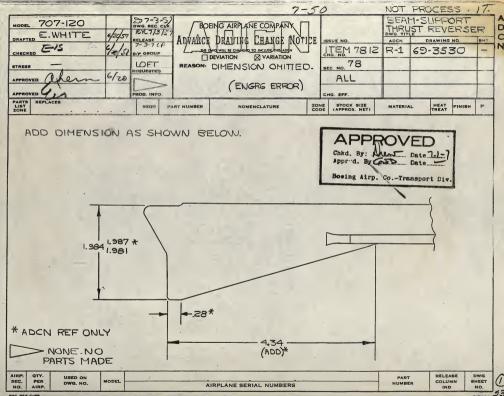


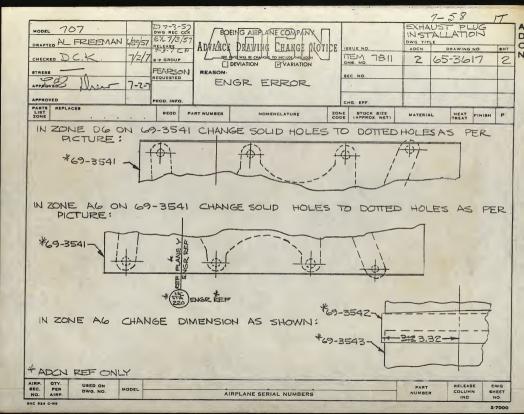


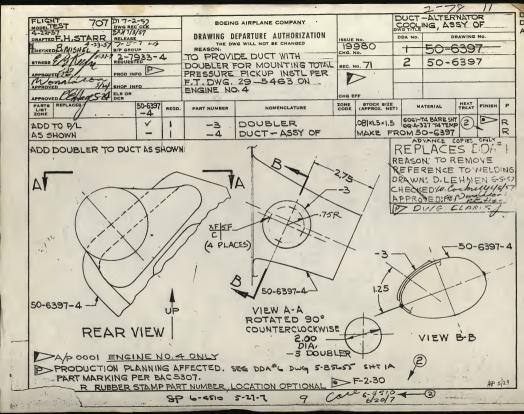


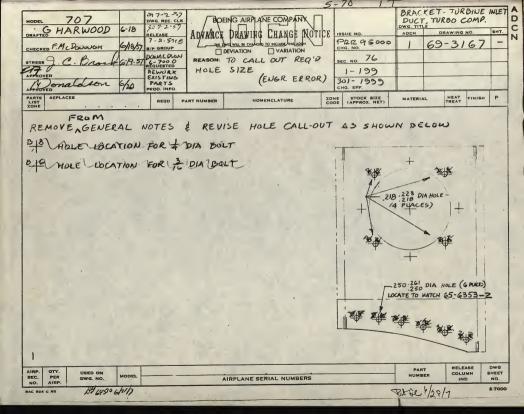


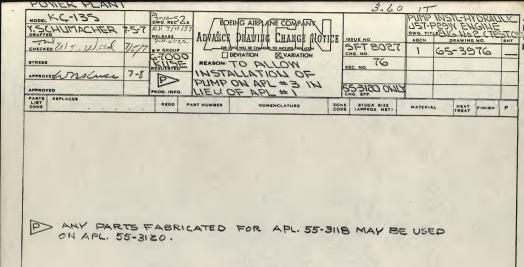








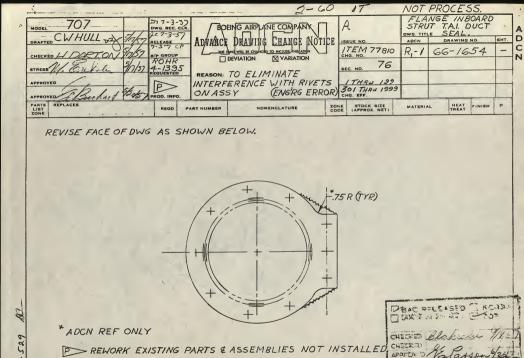




REVISE TAB BLOCK AS SHOWN BELOW TO 1 DG-1029 KH35 55-3120 ONLY

MODEL	AIRPLANE SERIAL NUMBERS	PART NUMBER	RELEASE COLUMN IND	DWG SHEET NO.
		02-2210		
-2 40133	22.211.P. CMF.L	CE SSTC		
		62-22(6		
?			65-3976 65-3118 ONLY 65-3776	25 KC135 55-3118 CN11X

wm 7-9-7



AIRP. SEC.

NUMBER

PART

COLUMN SHEET ALC. 28 7 2.7000

DWG

RELEASE

USED ON DWG. NO. AIRP. NO.

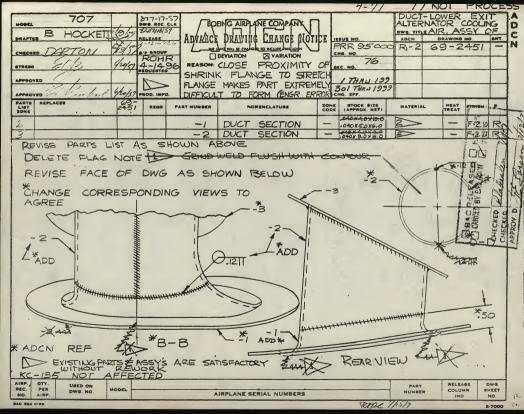
KC 135 NOT AFFECTED.

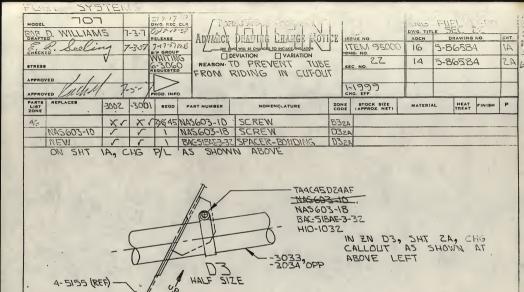
MODEL

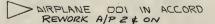
AIRPLANE SERIAL NUMBERS

PER

OTY.



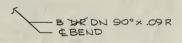




-INBD

AIRP. QTY. RELEASE DWG USED ON PART SEC. PER MODEL COLUMN SWEET DWG. NO. NUMBER AIRPLANE SERIAL NUMBERS NO -Files 7-5-7

5. 63 / THOT PROCESS SUPPORT BRACKET-277-17-57 707 DRAIN TANK, COMBUSTION D BORING AIRPLANE COMPANY MODEL DWG. REC CLK M.R. MATTESON SHT. ADCN DRAWING NO ISSUE NO. DRAFTED PRR 95000 63-1822 CHG. NO CHECKED DEVIATION N VARIATION ROHRO SEC. NO. 76 REASON SENDIIP INFO. CAUSES STRESS PART TO BE FORMED INCORRECTLY 1 THRU 199 APPROVED RELATIVE TO ADJACENT 301 THRU 1999 STRUCTURE (ENGRIG FRROR) PROD. INFO APPROVE STOCK SIZE ZONE MATERIAL FINISH LIST REGD PART NUMBER NOMENCLATURE REVISE BEND CALLOUT AS SHOWN:





P> EXISTING PARTS MAY BE USED BY REMOVING AS APPLICABLE -2 \$ STAMPING -1 \$ REMOVING -1 & STAMPING -2.

. KC-135 NOT AFFECTED.

AIRE QTY. USED ON MODEL SEC. PER DWG. NO. AIRPLANE SERIAL NUMBERS 40 7/4h RELEASE COLUMN IND

PART

NUMBER

DWG SHEET NO

NO. BAC 924 C-RB

AIRP

2-7000

	-		4-79 1-	_		
MODEL 707 DWG REC CIK DRAFTED S. Berry 6-187 Product 7 MECKED MANN HOUND 1-1-7 Product 7 STRESS STRESS APPROVED AND MANN HOUND 1-1-7 PRODUCTED APPROVED AND MANN HOUND 1-1-7 PRODUCTED APPROVED AND MANN HOUND 1-1-7 PRODUCTED PROD. INFO.	ADVANCE DRAWING	CHANGE NOTICE IN A PROCESSION OF CABIN STROLL NOTICE IN A	B PRR 10797 MST NO. EC. NO. 79	DWG. TITLE	DRAWING NO.	D. SHT.
PARTS REPLACES	ART NUMBER NOMEN	CLATURE ZONE	STOCK SIZE	MATERIAL	HEAT E	NISH P
NEW VVVV MS	21913B10 PLUG	CODE	(APPROX. NET)	MATERIAL	TREAT	RISH P
NEW YYY I ISO	1701-10 PACKING (BA	CPIIK-10)	ST	ILLWAN	RUBBER	CO OR EQU)
ADD TO PLAS SHOW	N					

SEC. QTY. PER AIRP. USED ON DWG. NO. RELEASE COLUMN IND PACH/22/7 DWG SHEET NO. MODEL PART NUMBER AIRPLANE SERIAL NUMBERS BAC 924 C-R5

MODEL 707		716-25 DWG. REC	CCK. BC	DEING AIRPLANE COMPANY	П	A	INBOARD NACELLE DWG. TITLE STRUT						
DRAFTED S. Berry	61	11/7	MILEASE	ADVANC	E DRAWING CHANGE ONC	ISSUE NO.	ADCN .	DRAWING		SHT			
Jan Senbuch	11/57	6-27-5- B/P GROU	THE DWG WILL BE CHANGED TO INCLUDE THIS ADON		PRR 10747	6 50-554		7	1				
1 ==		AIR CO	DEVIATION VARIATION CHG. NO.							-			
Samuel St.	1	12	REQUESTE	REASON: RELOCATION OF SEC. NO.									
APPROXED 6/191	Miss				PRESSURE CONTRO	7							
APPROVED THA CLEEN		PROD. INF		MPR		1-133-7 301- CHG. EFF. 1999							
PARTS REPLACES	-3	-1	REQD	PART NUMBER	NOMENCLATURE	ZO	NE STOCK SIZE DE (APPROX. NET)	MATERIA	L HEAT	FINISH	Р		
			SEE	CABIN	7 FOR REST			AME	- - E,				
NEW	-	~	2	MS21908D10	ELBOW-ET, BH. 90°								
. .	-	~	2	OIDTOCISZM	ELBOW-FT,BH. 45°								
	-	~	7	19161-096NY	WASHER								
	-	V	: 1	C-9523-163	FLEXIBLE TUBE ASS	Y			>				
	v .	V	4	DOI PSENA	NUT-JAM								
	~	~	1	8262605-24	CLAMP TUBE SUPPOR	Τ.			>				
	-	1	3	8262605-10	CLAMPTUBE SUPPORT	7			>				
	-	V	1	NO-1038	NUT (BAC-NIOBY-53)								
	~	~	: 1	82626CS-20	(BAC-CIDBH-ZOA)				>				
*	-	~			SCREW-MACHINE								
NEW	-	V	١	150701-10	PACKING-O-RING (BAC PILK -10)				-				
ADD TO GE	ENERA	YL N	OTES		ADD TO P/L	AS	SHOWN						
- KAYNAR	CO. Bx	20	OI TE	RMINAL	ANNEX, LOS ANG	ELE	S 54, CALI	=					
AVICA C													
							OUIEN			/			
-					ALS CORP, 10777 \				IN CALIF	COK EQ	(V)		
STILLMAN R	UBBER	3 CO	::5811	MARILYN	AVE, CULVER CITY		LIF COR EQ	(V.					
WORK PRESS. PSI			BE ASSY	REQD NUT	SLEEVE REQD ZONE SH TINGS PER TUBE ASSY ZONE CODE	TUBI		HEAT TREAT	IFICATION	ENDS ST	MIN FOCK GTH		
								-	3776 4126/2				

DOM

5-85 27 6-25-37 DWG. REC. CLK. PLUMBING INSTL MODEL 707 BOEING AIRPLANE COMPAN INBOARD NACELLE ma 6-16-57 STRUT 6/11-DRAFTED S. Betty DWG TITLE ISSUE NO. ADCN DRAWING NO. 6.27.57CB Sandenbish dup PRR 10747 B/P GROUP DEVIATION **⊠** VARIATION CHG. NO. 50-5547 AIR COND REASON: RELOCATION OF SEC. NO. 77 REQUESTED CABIN PRESSURE CONTROL SYSTEM APPROVED 1-199 6 301-PROD INFO CHG. EFF. 1999 PARTS REPLACES LIST -4 -3 -2 -1 REOD PART NUMBER ZONE STOCK SIZE NOMENCLATURE MATERIAL HEAT FINISH

PACKING

(BAC PILK -10)

PLUG

"O" RING

C

STILLMAN RUBBER CO

CULVER CITY CAILF (UR FQUIV)

CHANGE P/L AS SHOWN ABOUT.

NEW

NEW

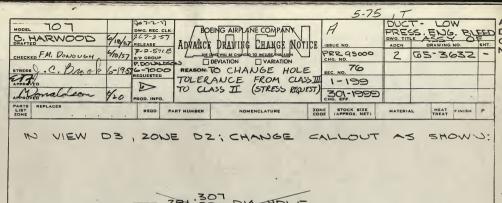
SEE ADON G FOR REST OF THIS CHANGE

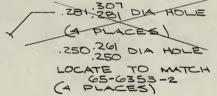
MS21913D10

150701-10

ADD TO TUBE ASSY AS SHOWN

V V 50	-57	2	OIDISEISZM	MS-21922-10	2		.625	.035	3>			BAC-TIHA	I	
V V 50	-56	2	NESIDE	01-55C15-2M	N		.625	.035	1			BAC-TILAA	I	
WORK	NUMBER	REQD	NUT	SLEEVE	REQD	ZONE SHT							_	-
PRESS. PSI	TUBE ASSY		END FITTING	S PER TUBE ASS	Y	ZONE	OD	WALL	MATERIAL	HEAT	FINISH	IDENT- IFICATION	TYPE	MIN STOCK LGTH
muc and E- Ka								_				MELL . VI.		

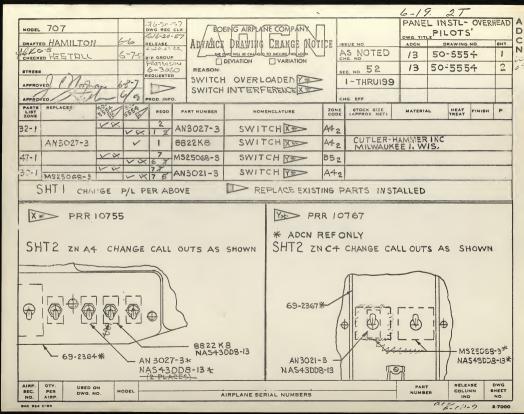




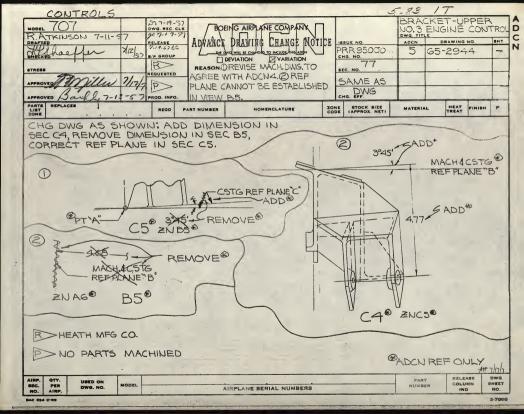
ANY EXISTING PARTS. MAY BE USED AS IS.

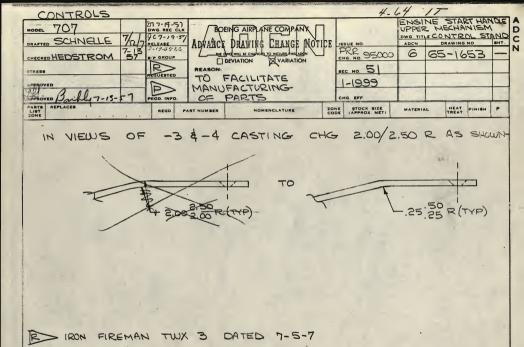
L								
	AIRP. SEC. NO.	QTY. PER AIRP.	USED ON DWG. NO.	MODEL	AIRPLANE SERIAL NUMBERS	PART NUMBER	RELEASE COLUMN IND	DWG SHEET NO.

BAC 924 C-RS AY68570 6/21/7

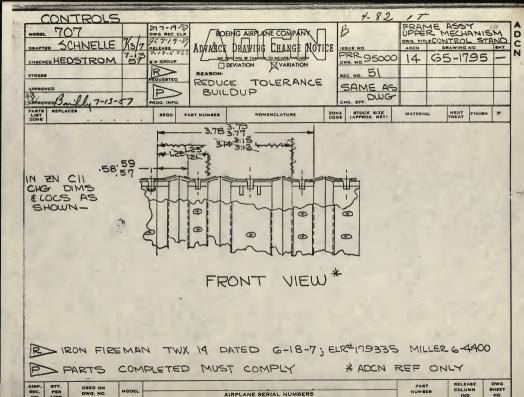


	- 11				5.65				-			=	3-20	5 47	-1.6
MODEL		70	7		87-18 DWG. REC	57 CLK	DEING AIRPLANE C	OMPAN'S F	7	4			ERATO		A
DRAFT	ED F.	H. Corse	or t	7-12-57	EW7-22	57 - / 1	11011	V		/ 1	DWG. TITI	LE	PEED		
None	/	ulluan		3/2-	RELEASE		CE DRAWING CH	ANGE NOT		PRR 10731	ADCN		RAWING N	-	H1.
CHECK	EF/CL	Muna	Le	\$22	B/P GROU			ARIATION		HG. NO.	17	50	1-975	0	J.
STRESS					6-700	- KENSO	N. TO PROVID		UCE S	EC. NO. 76	6	50	-975	0 :	2 51
APPRO	VED	tleider	- 7	10/12	REGUESTE	- FOR LA	TCH HOUSING			1-199				2.	
APPRO	ven.	1.					COWL PANE	<u></u>		301-1999		-			-
PARTS		ACES		1 50-	PROD. INF				C	HG. EFF.					
ZONE			-1.	9750	REQD	PART NUMBER	NOMENCIA	TURE	ZONE	STOCK SIZE (APPROX. NET)	MATERIA	ı.	HEAT F	INISH: F	
42				1	. 2	MV-02	NUT BAC NIC	ET-3)	10B				1 -	100	
42			~	-	5	H1032	NUT (BAC-NIC		103	1	SAYWAR	NUT C	ORE	QUIV.	
57				-	-1-	5140-97-9			4A						
58				1	1	5/40-97-9		BAC-G10T-9)	4A	K	ARKER .	APP C	o. OR	EQUIV.	
41			*V	Dev	37	66-2975	BRACKET		OB						
55				20	34	ANS 20-10R			108 8A						
18	-			-	1	10001-105	EXIT CUCT		6A SA	_					_
18	-			IN	180	65-35-72-300	The second second	-ASSY-OF							_
59			V	V	-	65-5890-300									_
-	CHA	NGE P/	LAS	ABO			1			5655 (REF)		7		. 0	-
N.	6	6-2975	BRKT	TO	PICTUR	E			6	A COLO		10	5-3572		
1100	11	7 00	NIC	FIC	11	DCN6		5	11-	9			5-5890		2
MUC	-17							1		11/2		1 6		- 1	
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100	اب 747 ر	GHANE	100	ANIZ	7 1L				KO		/	1			
liv .	210 7	10 CITAINE			4=103Z	AN 3-3 TO HID-103	110 -10 ///		114	WL 81.07 (R	55	- 1			
IN Z	MA	CHANGE:		ANS		AN960-			111	Will		1	BAC-C	1085-14	(A)
		65-3572-300			9665)		ES) MJ-02	-0110-	11/181	13.67 X	1	4	MJ-0	2	
	10	65-5890-30	000	> (CEPTIFIC	AN 520-1	0610-	L) (RE	F)		. 1	H 10-10		
		4	()	ZU A	S AD): 66-297s	5 BRKT & CALLOW	7			1	1	166-29		,
		GEN N	DIES	2			WZNAH CH		i,	(ZN BID)	1//	1		79	3
00	LIMI	TED - SEE	P/L	FOR RE	ELEASE	E . 19 117	BAC-CIOBS-148		-148	FRONT VI	SWX	/			1
10					70 00			H10-1032			,		V320-		0)
Mary Control	05-35	72-3000 IS	ANES	1 TH	RU 6 0	-5890-3000 NLY	MISEO IDRIO	AUSZO-IOR	10				10-103		1/4 1
AIRP.	QTY.	USED ON									PART	T	RELEASE	DWG	-
SEC. NO.	PER AIRP.	DWG. NO	MO	DEL			AIRPLANE SERIAL N	UMBERS			NUMBER		COLUMN	SHEET NO.	-
BAC 924 C	-R5								-		Done 2	1101		.,	- 7-





COMPLETED PARTS SATISFACTORY 14 71.7/2 RELEASE DWG AIRP. OTY. PART USED ON COLUMN SHEET MODEL NUMBER SEC. PER DWG. NO. AIRPLANE SERIAL NUMBERS NO. AIRP 2.7000



gel'1-17-7 2.7000

4-66 17 00 KNOB CONTROL LEVER DRAWING NO. ADCN ISSUE NO PRR 9500 65-2343 SEC. NO. 51. NOTED

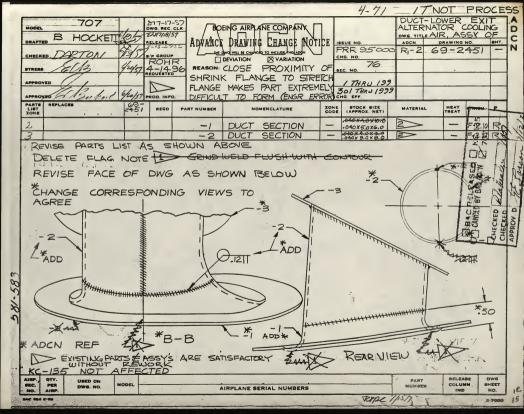
MATERIAL

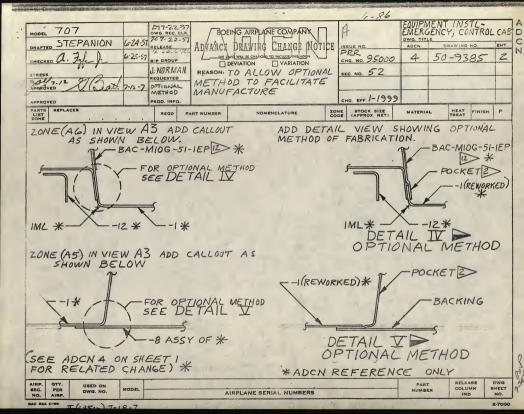
HEAT FINISH

PARTS REPLACES	REGO	PART NUMBER	NOMENCLATURE	ZONE		ı
an Sudditto	7-1757 PROD. INI	ro.	UP TO DAT	_	CHG. EFF.	
APPROVED	REQUEST	REASON:	TO BRING TAB		NOTED	
STRESS		.			SEC. NO. 51.	
CHECKED	2-19-51 8/P UNIT	net	THE WILL BE CHANGED TO INCLUDE THE	SADON	PRR 950	(
DRAFTED V. LEVACK	7-16-57 867-1		DRAWING CHANG	E NOTICE	SSUE NO	
MODEL 707	917-19 DWG. REG	CL'K / PO	EING AIRPLANE COMP	ANK []		

CHANGE TAB BLOCK TO READ AS SHOWN

AIRP. SEC. NO.	QTY. PER AIRP.	USED ON DWG. NO.	MODEL	AIRPLANE SERIAL NUMBERS	PART NUMBER	RELEASE COLUMN IND	DWG. SHEET NO.
		65-1388					
				`			
					-		





4.83 17 EXIT DUCT -ALT COOLING, ASSY OF DRAWING NO SMT PRR 10731 65-3572 76 65-3572 THRU 199 8 301 THRU 1999

SRF-2.104

MATERIAL

MODEL 707 BOEING AIRPLANE COMPANY HOPPER 6-7-7 6413=22-57 6-2-7 B/P GROUP [] DEVIATION M VARIATION 6-7000 REASON DUCT AND REQUESTED LATCH HOUSING INTERFERE PEOD INFO REPLACES LIST

PART NUMBER NOMENCLATURE 65-3572-300 EXIT DUCT-ASSY OF DUCT DUCT

REPLACES ADON 3

ISSUE NO

CHG FFF

STOCK SIZE

TO RELEASE OPTIONAL PART REASON: DRAWN! PH. CORSER 7-12-57

CH'D : Heineman 7-12-57

Monaldean 1-13-57 CHG EFF! I THRU G

PRR 10731

CHANGE TAB BLOCK AS SHOWN BELOW

ADD TO P/L AS SHOWN ABOVE

(NOTE: -3000 SAME AS 65-3572.)

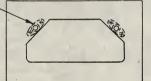
OPTIONAL 50-9750 707 AIDR USED ON PART RELEASE DWG MODEL SEC. PER DWG. NO COLUMN NUMBER SHEET AIRPLANE SERIAL NUMBERS AIRP IND NO.

BAC 924 C-RS

Rxpe 7/17/9

8-672T NOT PROCESS BOX-SLEEVE COOR D17-15-57 MODEL 707-120 BOEING AIRPLANE COMPAN' ASSY DRAFTED E15 6-21-57 DWG. TITLE ADCN DRAY JG NO. SHT ITEM 7813 CHECKED C. Mylite 69-3548 DEVIATION DEVARIATION 78 REASON STRESS NUT PLATE INCORRECTLY ALL CALLED OUT. (ENGRG ERROR) CHG. EFF. APPROVED 4 REPLACES ZONE STOCK SIZE MATERIAL LIST PART NUMBER NOMENCLATURE 69-3548 BAC MIDLE NUTPLATE I-4 -ABBCP 70LHA40IP NUT-PLATE FLOATING BAC NIOLC -AEECP (BAC-NIOLC-A38P) REVISE PL AS SHOWN ABOVE REVISE DWG AS SHOWN BELOW APPROVED

TOLHA 401P-02 (2PLACES)



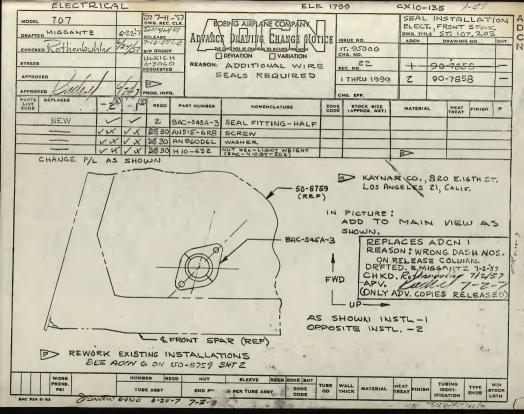
Approd. By March Date 7-10-57

Boeing Airp. Co.-Transport Div.

RELEASE DWG AIRP. QTY. PART USED ON COLUMN SHEET PER MODEL NUMBER DWG. NO. AIRPLANE SERIAL NUMBERS NO. NO. AIRP

BAC 924 C-R

L-ZOOC

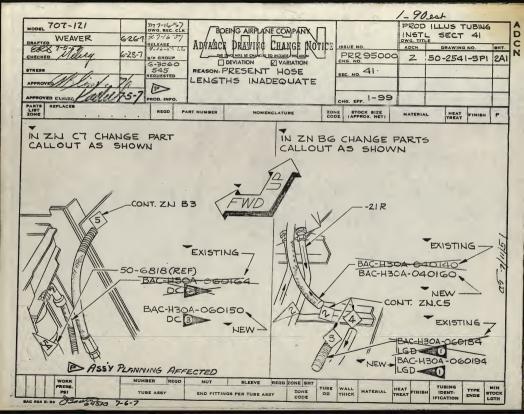


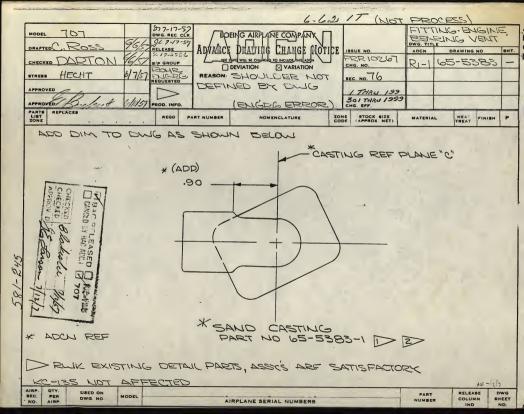
CONTROLS	3-68	17
MODEL 707 ST. 16.55 DWG. REC. CLK	I. / TIME	MECHANISM IT
CHECKED Shaeffer 19/57 RELEASE	ADVANCE DRAVING CHANGE NOTICE ISSUE NO. DOWNS. THE CHANGE NOTICE ISSUE NO. DOWNS. THE NO. DOWNS.	DRAWING NO. SHT.
STRESS REGUESTED	REASON:	65-2395 4 N
APPROVED CONTRACTOR 7-9-57	PART WAS CANCELLED 1-199	3.
PARTS REPLACES	CHG. EFF. ART NUMBER NOMENCLATURE ZONE STOCK SIZE MATERI	AL HEAT FINISH B
	CODE (APPROX. NET) MATERI	AL HEAT FINISH P
IN ZONE	AZ REMOVE 65-5919	
	7.44	
-1		

P FLR# 179336 MILLER 6-4400 (7-2-7) IRON FIREMAN
P DRAWING CLARIFICATION ONLY - PARTS NOT AFFECTED

AIRP. OTV. BEED ON DWG. NO. MODEL PART NUMBERS PART NUMBER NO. AIRP.

RELEASE DWG COLUMN SHEET IND NO.





DETAIL PLANNING AFFECTED

AP 6/20

AIRP OTY BEC ON DWG NO. MODEL AIRPLANE SERIAL NUMBERS PART HUMBER COLUMN NO.

C

4-75 2T

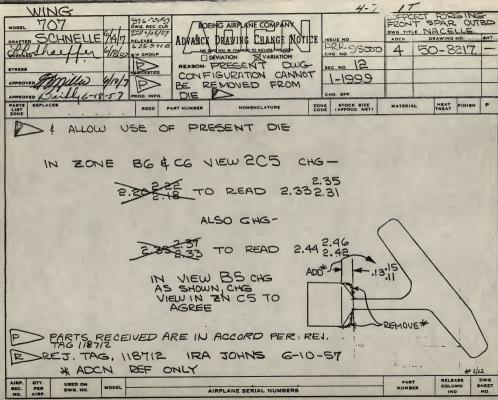
MODEL 707	12-57	DWG. REC	5-57 BC	DEING AIRPLANE COMPANY	/	A	DWG. TITL	WER S STALLA COUTED	STE	74
CHECKED DIAM LEON	9/8	6.25.57 B/P GROU	ADVALLE .	DRAVING CHANGE ITOTI		10764 Hg. No.	ADCN 13	S-SIZ		IA.
Densidson PROVED	118/57	G-700	OF TH	TO ALLOW REMOVAL E TOP ENG TEMP WITHOUT REMOVA	1,	-199 d				
PROVEDENMERSON	6/19	PROD. INF		NOINE	L'O	501-1999				
ARTS REPLACES	8-8122 -3000	REQD	PART NUMBER	NOMENÇLATURE	ZONE	STOCK SIZE (APPROX. NET)	MATERIA	HEAT TREAT	FINISH	P
NEW	/	1	-3023	REINFORCEMENT PLATE	A4 ZA	×7.0	3>	-	F-8-05	R
NEW	/	1	69-4032	CAP	ZA					

ADD TO P/L AS SHOWN ABOVE:

> .036 OPT .042

> REWORK EXISTING ASSYS

RP. GTY. USED ON DWG. NO. MODEL AIRPLANE SERIAL NUMBERS NUMBER COLUMN IND NO.



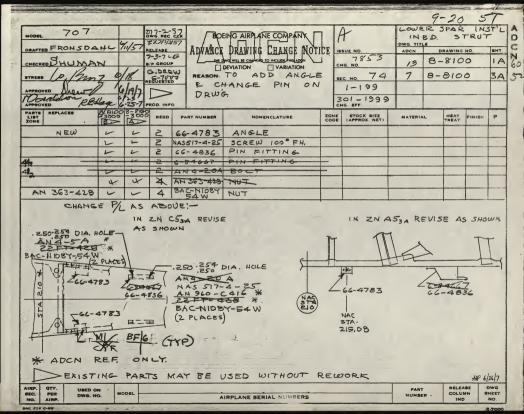
2-80 IT

FLIGHT TOT	77-3-57 DWG REC OLK \$ZN1/5/57			G AIRPLANE COMPANY	B		WOSE L	LE, AS	SY OF	INE	_
4-26-57 DRAFTED F. H. STARR	RELEASE		DRAWING D	EPARTURE AUTHORIZATION	ISSUE	No.	DDA No.		DRAWING	No.	
L. J CARPENTER	7-5-723 B/P GROUP		REASON:	WG WILL NOT BE CHANGED	CHG. I		5	5-85	655	SHT	A
STRESS	2-7933- REQUESTED			CE DUCT 50-6397 F WHICH HAS		10. 71					
APPROVED PLANE 6.28	SHOP INFO	>	NSTRUMENT ON ENGINE	ATION PROVISIONS, NO. 4	CHG E	>					
PARTS REPLACES	85655 -3000	REQD.	PART NUMBER	NOMENCLATURE	ZONE	STOCK SIZE (APPROX. NET	М.	ATERIAL	HEAT	FINISH	Р
59-5 DELETS 50-6397	· ·	1	50-6397 50-6397-4	DUCT ASSY							

APOODI ENGINE NO4 ONLY

POPLANNING AFFECTED

PRR 19980 INSTALL 50-6397-4 DUCT ASSY



1.2		الد درما			3 9-7017	
1	DRAFTED TIFL JIOKA D	DWG. RC. CLK BOE! ZESSERELEASE ADVANCE	DRAVING CHANGE NOTICE	Hew Issue No.		OF
	CHECKED Plumplan	10/4 B/P GROUP	O WILL BE CHANGED TO INCLUDE THIS ADON	ITEM 7ZII		ТНа
	STRESS	BEOUFSTED P		SEC. NO. 72		IA
	Monaldson ,	REASON: 1	L INCORRECT NEW PART	1-199		
		65 PROD. INFO.	*	301-1999 CHG. EFF.		
	LIST ZONE	595617 REQD PART NUMBER	NOMENCLATURE	ZONE STOCK SIZE CODE (APPROX. NET)	MATERIAL HEAT FINISH	P
	5-88444-3003	V 5-88444 -2003	STIFFENER LH SIDE			
	5-88444-3064	V 1 5-88444	STIFFENER LA SIDE	to the second company of the second company		-
	5-08447-3000	V 1 5-88447 -3006	STIFFENER RUSIDE			
	5-88441-3002 NEW	V 1 5-88447	STIFFENER RYSIDE			
-						
-	CHANGE BY					
	REPLACES A REASON: TO MAKE DWG CHG ON 5-88447 READ: SAFFELL 6-3060 DRAFFED: GLENN R. DOO CHECKED: Rothogulpha APPROVED: Lacker G	DCN AGREE WITH SHT IA & ZA REF (COORD SHTCK 10-93) WINING 6-13-57 WJ24/57	ADCN NOTE: SEE ADO	HANGE, JZ ON 5-88447 SH SHTZA FOR COM	HTIA & DON B PLETE CHANGE	-
	SEC. PER DWG. NO. MODE	DEL AIR	DI ANE CEDIAL ANNADES	-1	PART RELEASE DWG	

AIRPLANE SERIAL NUMBERS

NO. AIRP.

BAC 924 C-RE

756850 6-24-7

SHEET

NO.

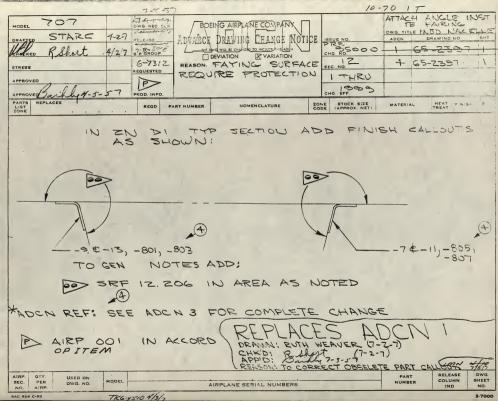
IND

NUMBER

				/	0-8	80 IT	NOT	PROCES	55
(4)	NODEL 707 DRAFTED HOCKETT OF CHECKED ATON STRESS Ses Cechanial APPROVED ALTERNATION APPROVED ALTERNATION	5/13/57 FROD. INFO.	ADVANCE REASON Z	EING AIRP ANE COMPANY DRAWING CHANGE NOTI DRAWING CHANGE NOTI DEVIATION VARIATION EXTRUSION CANNO ECHASED (VENDOR ENCY) ***	5	ESUE NO. PRE 10087 MG. NO. TH RU 195 GO 1 THRU 199 MG. EFF.	FIREWINACELLE DWG. TITLE ADCN R,-1	DRAWING NO.	LATION E
	LIST ZONE	5-365 REGD	PART NUMBER	NOMENCLATURE	ZONE	STOCK SIZE (APPROX. NET)	MATERIAL	HEAT FIN	ISH P
	1-9		7	CTRAC		BAC - 1527-6	1020 OR 1025 NI	I-5-	20 7
0	1-4	1211	-3	STRAP	-	142.0 LONG	1952 COLD BO	(E-1)	
581-480	PAGAC RELEASED OF CHECKED BLANCIE BLANCIE BLANCIE BLANCIE BLANCIE CHECKED BLANCIE CHECKED APPROV DI ROJANO	RUSION, 102 ET STOCK 1 KC-135 (200) 707	20 OR 10	DING OR SHT STOR	T	NNEALED DER QQ	COLD -5-63	ROLLED	0.50
	* ADCN REF KCI35 NOT AFFE S EXISTING		-	*D6 FULL SIZE E SATISFACTORY	•	XX FINIS	H CHEL	AT RESIS	
I	AIRP. QTY: USED ON						PART	RELEASE	DWG
	SEG. PER DWG. NO.	MODEL	A	IRPLANE SERIAL NUMBERS			NUMBER	COLUMN	SHEET

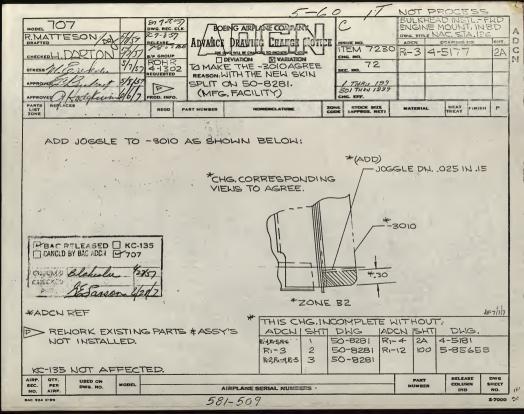
BAC 924 C-RS

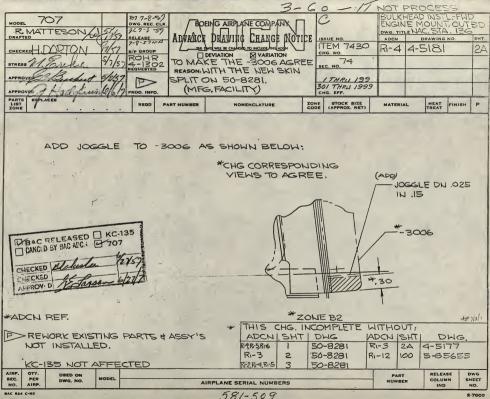
2-7000



2-7000

					11-	65	SIT	NOT	PROCES	35	
STRESS APPROVED	TOT TTESON DES DARTON Grakertun	\$16/57 \$16/57	DWG. REC. CLI 9C.7-3-57 RELEASE B/P UNIT ROHR 4-1384 RECUESTED PROD. INFO.	ADVANCE REASON: S	EING AIRPANE COMPANY STATE THE STATE OF THE	OR	ISSUE NO. PRR 10087 CHG. NO. 71 SEC. NO. 71 THRU 199 CHG. EFF.	ENGI DWG. TITLE ADEN	HALF NE NACT DRAWING N 36-38	ELLE	SHT.
PARTS RE	PLACES		REQD	PART NUMBER	NOMENCLATURE	ZON	E STOCK SIZE	MATERIAL	HEAT	FINISH	P
BAC Z CANCLI SEE ALC CHECKED APPROV I	REE AS S RELEASED D BY 300 APON D W 3 7 7 17 1/2 3 Blakuslu N REF.	HOWN KOTS TO PROV STING	ISSYSE WILLIAM SET'S	ELDING C	OPERATION IS SATISF	ACT	07/03/	THE	12 12	AMP 7/2	13/7
						_		1111		1	-
										-	7g
AIRP. QT SEC. PE NO, AIR	R DWG. NO.	MODEL			AIRPLANE SERIAL NUMBERS			PART		MN SH	WG.





581-509

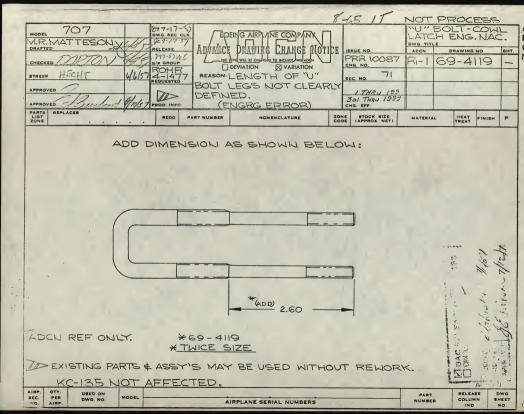
-				5 -	76	, 27				
MODEL 707	6-13-57	21 7-3- DWG. REC		DEING AIRPLANE COMPANY		A	1175 1175	WEST STE	4017	
DRAFTED G. MODES		7-8-57	ADVANC.	PRAVING CHANGE NOT		SSUE NC.	ADCN	DRAWING		SHT.
CHECKED TELESTAGE		E/B GROU		DEVIATION VARIATION	١ إ	PRR 10764	15	8-8	100	IA
STRESS / / Masker	-	6-70	n l	TO ALLOW REMOVE	-	SEC. NO. 7Z				-
No 1	6/15		PROE	HE TOP ENG TEMO BE WITHOUT REMO	VAL	1-199				
APPROVED CARIN		PROD. INF	OF E	NGINE		CHG. EFF.	1		apar orona com	-
PARTS HEPLACES	8.810	REQD	PART NUMBER	NOMENÇLATURE	CODE	STOCK SIZE	MATERIA	L HEAT	FINISH	Р
nen	~	t	-Z3	REINFORCEMENT PLATE	A7 3 A	×7.0	3>	-	F-8.05	~
NEW	/	1	69-403Z	CAP	A7 AE					
ADD	7	D 7	P/L AS	SHOWN AB	07	=:				-

036 OPT .042

REWORK EXISTING ASSY'S

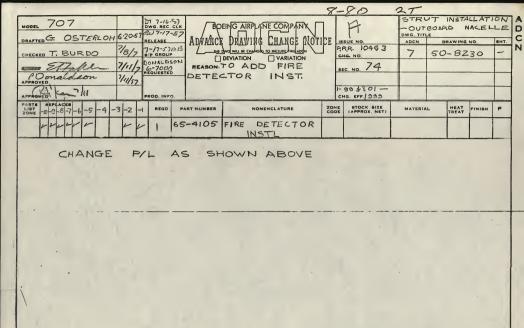
						A	P 6/2!
AIRP.	SEC. PER	USED ON	MODEL		PART	RELEASE	DWG
NO.	AIRP.	DWG. NO.	MODEL	AIRPLANE SERIAL NUMBERS	NUMBER	IND	NO.

BAC 924 C-R5



			8-80	27	Section of section to the section of
MODEL 707 ORAFTED GT. OSTERLON 9/20/7 CHECKED T. BURDO 7/8/7 ANDONE ET-TOLL 7/11/2 APPROVED TO 1/11/2 APPROVED TO 1/11/2 APPROVED TO 1/11/2 APPROVED TO 1/11/2 APPROVED TO 1/11/2	RELEASE 7-17-57)## 6-7000 DONALDSON REASON RESOURTED	EING AIRPLANE COMPANY DRAWING CHANGE MOTI DRAWING CHANGE MOTI DEVIATION VARIATION TO ADD FIRE COOR INST.	ISUE NO. PRR. 10 4 5 3 CHG NO. BEC NO. 72 1-99 \$ 301- CHG. EFF. 1999	STRUT INC. A INBOARD INC. CL OWG. TILLS ADON DHAWKIN IN 5 50-84	о внт.
PARTS REPLACES -7 -6 -5 -4 -3 -2	_ REQD PART NUMBER	NOMENCLATURE	ZONE STOCK SIZE CODE (APPROX. NET)	MATERIAL HEAT	FINISH P
	1 65-4105	FIRE DETECTOR			
CHANGE	P/L AS	SHOWN ABO	OVE		

	AIRP. SEC. NO.	PER AIRP.	DWG. NO.	MODEL	AIRPLANE SERIAL NUMBERS	PART NUMBER	COLUMN	SHEET NO.	J
ľ								2.7000	



AIRP. QTY. SEC. PER NO. AIRP.

MODEL

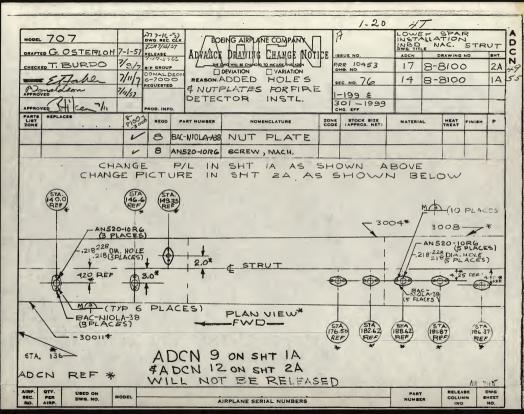
USED ON

DWG. NO

AIRPLANE SERIAL NUMBERS

PART RELEASE NUMBER COLUMN

LEASE DWG DLUMN SHEET IND NO.



					1-74 17			
DR	R. MATTESON	77-17- DWG. REC 6/12/57-17- RELEASE 1/2/57 ROHR 4-14-5- RECUESTE	ADVIACI	DRAVING CHANGE NOTI	PRF95000 CMG. NO. SEC. NO. 71.	L.H. SIDE	ENG. NAC BRAWING NO. 85637	
APP	ROVED	PRODUESTE	HOME	BER CALLED OUT. NGRG.ERROR)	J THRU 199 301 THRU 1999 CHG. EFF.			
PAI Lit ZO	TS REPLACES	REQD	PART NUMBER	NOMENCLATURE	ZONE STOCK SIZE	MATERIAL	HEAT FINISH	P
TEC CHG	ADCN REF. > DWG CLARIE	*CHG		LEAS	CHEKED AS SWAED INTO THE TOTAL CHEKE WITH THE THE THE THE THE THE THE THE THE T	The state of the s		
;	KC-135 NOT	AFFECTE	ED.			-	*** 7/11	h
AIR:	P. QTY. USED ON DWG, NO.	AFFECTE		AIRPLANE SERIAL NÚMBERS		PART NUMBER	RELEASE	DWG SHEET NO.

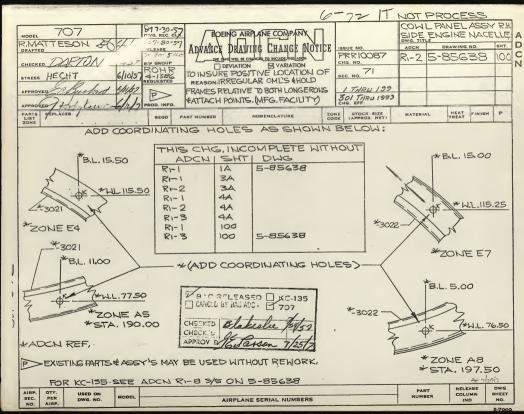
-		WHOMPSON .				-				8-80 1	T				
	707			-26-	D	77-9- WG. REC	CLK / BOI	EING AIRPLANE COMPANY	1	В	PLUN OUTB	DN	G II		
DRAFTS	G. OSTERL	01	-		R	ELEASE	ADVANCE	DRAWING CHANGE MOT		SUE NO.	ADCN	THE PERSON NAMED IN	RAWING		SHT
CHECK	T. BURD	0	6	28		P GROU	XHE C	DEVIATION VARIATION] F	RR. 10218	6	50-	554	8	
STRESS					D	ONALD	ON REASON:	ADDED PARTS FOR	. [EC. NO. 79					
511	7 -1 /	11.		11	R	EQUESTE		E DRAIN SYSTE	44	301-1999					
APPRO	- 1		-	_	7		CHAN	GED FLAG NOTE	3.	1-199	+	-			-
APPRO		ng.c	- 1	1-2-	7 -	ROD. INF	o		c	HG EFF	1				_
PARTS LIST ZONE	REPLACES	-4	-3	-2	-1	REQD	PART NUMBER	NOMENCLATURE	ZONE	STOCK SIZE	MATERIA	L	HEAT	FINISH	P
11		~	-	~	-	21	M\$21907-8C	ELBOW-TUBE-450		,					
16		~	-	-	1	3+	AN924-8C	NUT- BLKD							
17		~	~	-	-	6 8	MS29512-8	"O" RING						L	
18		1	~	v	V	3 *	AN806-C8	PLUG						L	
49		-	1		0	1	10-60104-	HOSE ASSY (DRAIN)			2	الم			
14		X	×	4	2	1	MS21908-8C	ELBOW 90°			·				
15		X	X	X	4	1	MS21902-8C	UNION							
10	-	-	-	_	-	1	AN924 8	NUT BLKD	-	1					
50		×	~	-		. 1	10-60104-1	HOSE - ASSY			<u> </u>	100			
CHANGE PL AS SHOWN ABOVE REMOVE 3> AS SHOWN BELOW.															

COLOR BAND PER BAC 5001 WITH TAPE BAC-THS-SEF

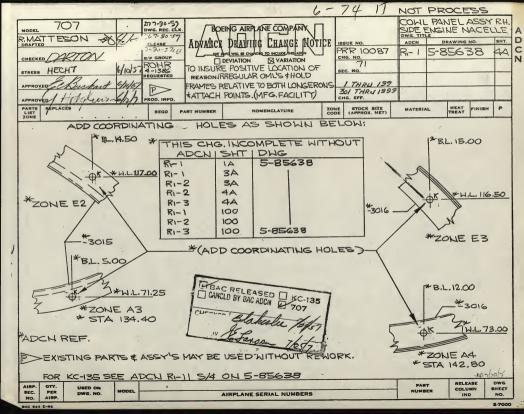
DADEN REF ONLY - REPLACING PART WILL BE SHOWN ON ENGINE PLUMBING INSTL

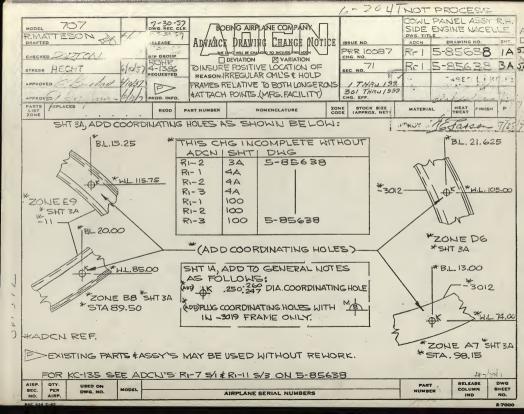
							7/8/57
SEC. NO.	PER AIRP.	USED ON DWG. NO.	MODEL	AIRPLANE SERIAL NUMBERS	PART NUMBER	RELEASE COLUMN IND	SHEET NO.

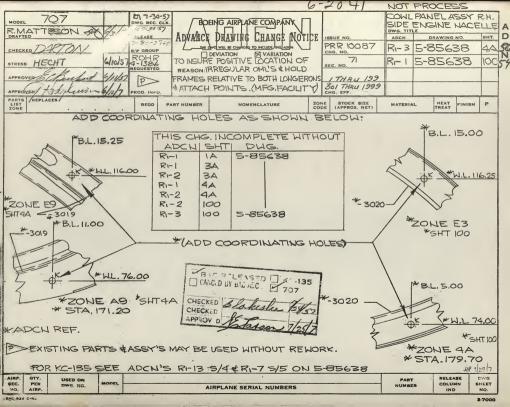
-1			*			v			6	-76	17			
MODE			5		317-29 SWG. REC	-57 - / BO	EING AIRPLANE COMPANY		A		アンド			1
DRAFT	ED /	BUR	00	7,76	7. 30-3	ADVANCI	DRAWING CHANGE MOTI		ISSUE NO.	ADCN		ING NO.	_	нт.
CHEC	ال	yyle	-	1/22	B/P GROUP		DEVIATION VARIATION	, [PRR 10453	2	50-3	337/	1	A
STRES	6				6-700	REASON:	TO BRING	L	SEC. NO. 7/					
APPRO	took	Box 1	than !	7/22	HEGOESIE	P/	L UP TO DATE.		1-99.301-19	4				
APPRO	- F	511		7-23-7	PROD. INF			ı	101-199 CHG. EFF.				_	
PARTE										1	не	1		-
ZONE		15			REQD	PART NUMSER	NOMENCLATURE	CODI	STOCK SIZE	MATERIAL	TRE	AT FIN	SH P	
<u>.</u>	-	YV	VX	VX	+1	50-8281	FAIRING ASSY FWD.	A-5						
	ļ	V	VX	VX	+1	65-6487	FAIRING INSTL-AUX							
	NEW	1			1	5-85638 -3096	R.H. SIDE PANEL ASSY	C7					,	
	NEW	V			1	5-85637 -309 <i>5</i>	L. H. SIDE PANEL ANY	36						
			VH	W	1	5-85637	LH SIDE PANEL ASSY		1					
			14	14-	1	5-85638 -3000	R.H SIDE PANEL ASSY							
CHANGE T/B AS SHOWN BELOW:														
71	4	50-8	200	703	17	HRU 9	9	_		50-33	711	-	P7/26	17
Easter		NAME OF TAXABLE PARTY.		707	U.SERTEMENT	MICHARITATION OF WORLD	~			- 300	7/ 5		-	-
71	4	50-8	-			HRU 199				-300	00 1	\geq		
71	4	50-82	20 1	707	101 111	E- 661-08	301 THRU 1999			50-337 -3000		3>		
SEC. NO.	PER AIRP.	DWG. N		ODEL		À	IRPLANE SERIAL NUMBERS			PART		LEASE DLUMN IND	SHEE NO.	ET

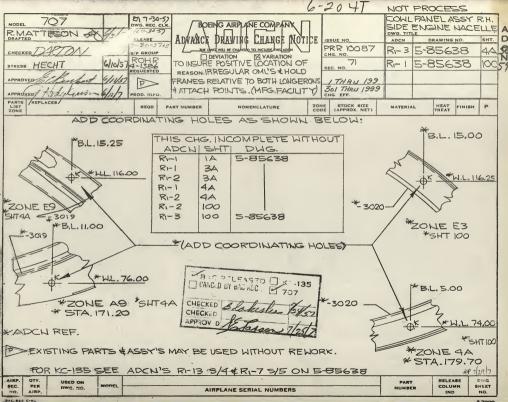


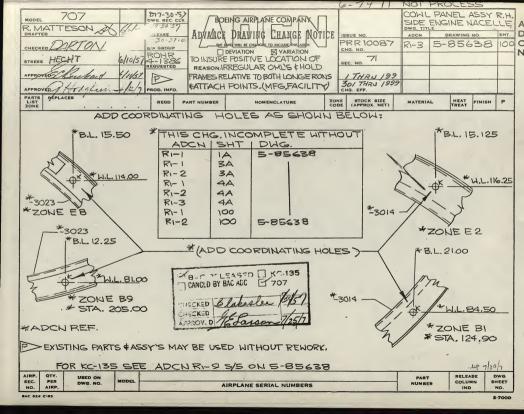
		6-74 IT	NOT PR	OCESS	
MODEL 707 57.30-57 R.MATTESON 08 11-1-30-57	1. \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		COWL PAN SIDE ENG DWG. TITLE	INE NACE	LLE
DRAFTED RELEASE	ADVANCE DRAWING CHANGE NOT	PRR 10087		5638	SHT
STRESS HECHT 410/5 7-1386	DEVIATION VARIATION	CHG. NO.	1 2 -		+
APPROVED SUBJECTION 411/57 P	REASON: IRREGULAR OML'S & HOLD	SEC. NO.			\top
APPROVED P HANKERS 6/12/7 PROD. INFO.	#ATTACH POINTS. (MFG. FACILIT				
PARTS SEPLACES REQD PARTS LIST LONE	ART NUMBER NOMENCLATURE	ZONE STOCK SIZE CODE (APPROX. NET)	MATERIAL	HEAT FINISH	P
ADD COORDINATING	HOLES AS SHOWN E	SELOW:	, while	B.L. 14.50	
*B.L. 14.50 *THIS	CHG, INCOMPLETE WITH	OUT	,	D.L. 14.50	,
ADC	CNISHTI DWG.				
Ri-I	IA 5-85638		W Vs		
K *H.L.117.00 R1-1	3A			*W.L.1	17.00
*-3017 - RI-1	14A		17 de	Harris	17.00
· // P/ 51-3	44	×-3018	-//)	
ZONE EG RI-1	100	·		M	
RI-3	100 5-85638		/- *	ZONE E	8
-3017 *B.L.5.00	(ADD COORDINATING H	11 550			
5.2.5.50	A D COOR DINA ING A				
- 2 4*W.L.71.625	GAC RELEASED [] KC-135 CANCLD BY BAC ADC : [2707		* B.L. 5	,00	
*ZONE A7	CANCED BY BAC ADC: 12707	*			
*STA 150 75 CH	ECKED Blowsler /2/52	*-3018 —		4	
ADG	PROV. D. To To		DK.	J* W.L. 72	2.00
*ADCH REF.	16 Gargon 1/23/1	3	*70		
PEXISTING PARTS & ASSY'S M	MY BE USED WITHOUT REM	IORK,		JE A8	
FOR KC-135 SEE ADON RI-	2 SA ON 5-85(28			-147/29	12
AIRP. QTY. USED ON "	2 2/ + 5/4 3-65630		PART	RELEASE	DWG
SEC. PER DWG. NO. MODEL	AIRPLANE SERIAL NUMBERS		NUMBER	COLUMN 1	NO.

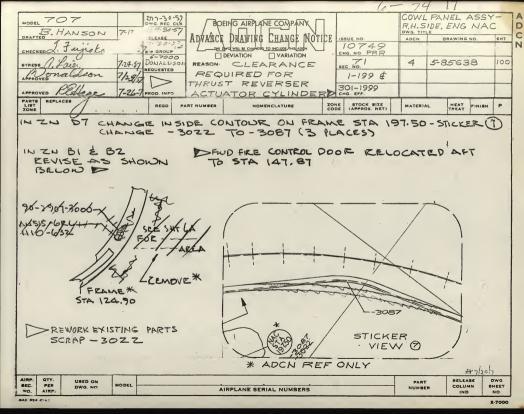


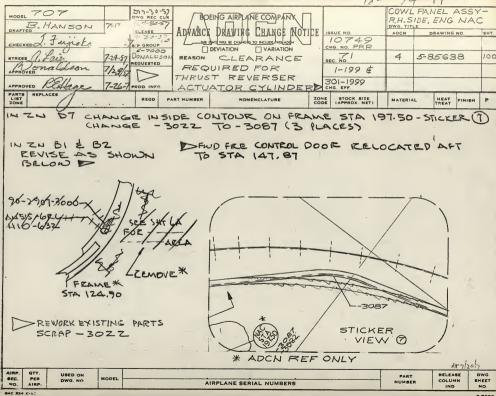




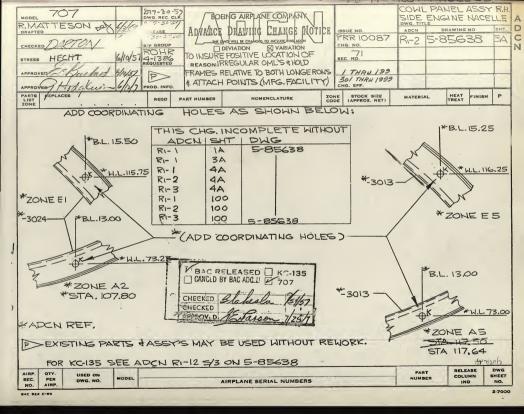




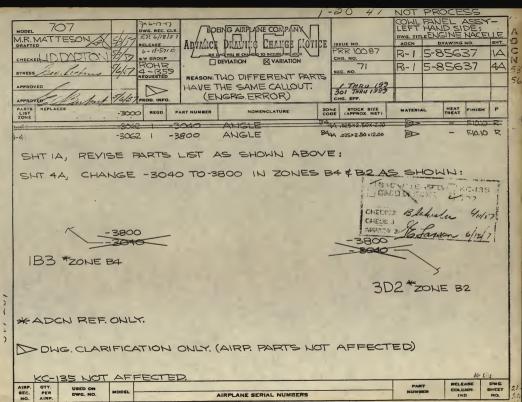




C



A . T ORDER NUMBER	SECTION 28 .	PAA-121 D6-1048	AA-123 D6-2757	CAL_124 D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2,760	TWA-331	LUFT-130 D6-276L	BOAC-136	A11-437 D6-2762
212-1	Fuel System Fuel CARTES III LATING AAlic														
28-2	Dual Fuel Check Valve	ę, 🗵													
28-3	Wing Ce.ter Jection Tubing and Equipment Locations Diagram	δπ 🔀			L							L_			
2n-4	Brip Stick Fuel Level Indicator	100		L	L_						1				
2° - 5	Fuel Tank Fillor Can Installa- tion Details	×													
28-26	. Fuel Tank Arrangement	P" A	X	X										-	
28-7	Internal Puel Tank Structure Seals	0 11 🗙													
28-8	Fuel Tank stemovable Component Seals	A									L_				
28-9	Main Tank Baffle Check Valves	IA A													
28-10	Wing Center Section Tank Aft Cells	X							<						
28-11	Wing Center Section Tank Cavity Drains	Sr X	P.U- X		X			X							
Section 2010	August and the second s														



BAC 924 C-R5

2.70

DRAFTED F. M. DONOUGH CHECKET The Source Source ETRESS (1, FAMEL POONE LISON APPROVED REHOUSE APPROVED REHOUSE	5/21/57 R 6/11 B 6/11/57 R	WG. REC.	ADVANCE	DRAWING CHANGE NOTION TO SUPPORT SKIN AT HOLE CUT-OUT ! TO EAR COWL FRAME			DWG. TITL	ENG.	, NA	CELLE NO.	
PARTS REPLACES	85,3000	REQD	PART NUMBER	NOMENCLATURE	ZON		MATERIA	L H	REAT	FINISH	Р
NEW	V	1	-3085	DOUBLER	C62/	4 .040×3.5 DIA	502	>	-	SRF-2115	R
NEW	~	1	65-6411-1	FRAME INSTL	482	A					
American described a management of the second of the secon				2 (A. 213,73							

ADD TO P/L AS SHOWN ABOVE

MODEL	707 F. M. DONOUGH		PC 6-17-57 DWG. REC. C E2 (6/18/	CLK. / BO	EING AIRPLANE COMPANY	111	EM	COWL RIGH	PANEL T HANG	ASS SI NAC	ELL	E
DRAFTED		1//	4-18-57	ADVANCE	DRAVING CHANGE MOTI	CE IS	RR 10087-1	ADCN	-	ING NO		SHT.
CHECKE	Stulken	9//	B/P GROUP		DEVIATION VARIATION		IG. NO.	2	5-85	63	8	IA
STRESS			DONNEDSO	, N		SE	c. NO. 71					
10	onaldse	6/11/	REQUESTED	NEASON:	TO ADD REAR COWL	-						
APPROVE	PGHL	6-12-7	PROD. INFO	FRAME		1-	199,301-1999 IG. EFF.					
PARTS LIST ZONE	REPLACES	2.000	REQD	PART NUMBER	NOMENCLATURE	ZONE	STOCK BIZE (APPROX. NET)	MATERIA	AL HI	AT EAT	INISH	P
							_ نسخت					
i	NEW	V	1/1	65-6911-2	STA, 213,75	B102A						

Ap 6/13 AIRP. QTY. RELEASE DWG USED ON PART SEC. PER MODEL COLUMN SHEET DWG. NO. NUMBER AIRPLANE SERIAL NUMBERS AIRP. IND NO.

BAC 924 C-RS

MODEL 707 DRAFTED HULL, C.W. DRAFTED HULL, C	SELLE OF. No.	SHT.	ALIC					
CHECKED DARTON SS 12 GROUP ADVANCE DRAWING CHANGE NOTICE ISSUE NO. ADEN DRAWING CHECKED DARTON SS 12 GROUP AND ADVANCE DRAWING CHANGE NO. ADEN DRAWING CHECKED	55	IA						
CHECKED DATION 757 8/P GROUP DEVIATION WARRATION TOT SPLICE PLATE DIFFERS		-	1					
2 / ROARS 707 SPLICE PLATE DIFFERS 1/1 1/1-7 3-8363	55	101	TI IT					
REQUESTED REASON FROM CORRESPONDING		1	15					
WC 135 PART & THEREFORE REQS THAN 199			4					
APPROVED Leeshart \$11/57 PROD. INFO. A3000 SERIES NO. (ENG'RG ERROR) CHG. EFF.			1					
PARTS REPLACES LIST REPLACES L	FINISH	Р						
1-33 V 2 38 SPLICE PLATE. 050×160×20.0 1	F-2.115	A	1					
1-39 V V 2 -3823 SPLICE PLATE .050N.60x26.0 => -	F-2.115	R	-					
- F-2116 D								

DWG. NO.

REWORK EXISTING PARTS NOT ASSEMBLED.

KC135 NOT AFFECTED. QTY. USED ON

MODEL

AIRPLANE SERIAL NUMBERS

CHECKED Blakesta 9/157 CHECKED APPROVIDE APPROVIDE AFERDAMENTO RELEASE PART COLUMN NUMBER

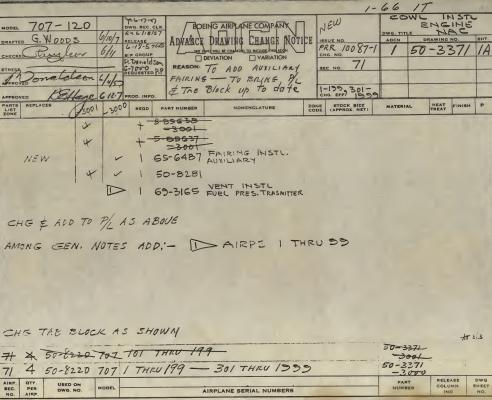
DWG SHEET

AIRP SEC.

IND

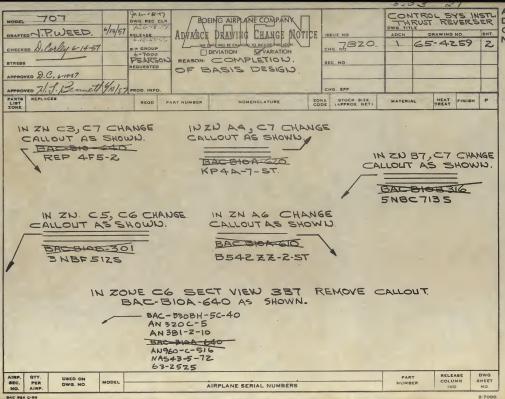
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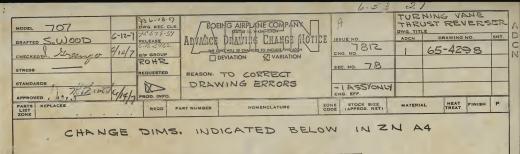
AIRP.



BAC 924 C-RS

C





ASSY NO	DIM"A"E,O	DIM "B"	DIMX'	DIM"Y"
-81	3.070	3.128	.030	.035
-83	3.050	3.128	.035	,050
-85	2.957	851.8	-,025-	.1250
-87	2.950	3.128	,IZ50	.054
-89	3.820	3.905	.064	.025
-91	4.177	4.231	.054	.000

NO PARTS MADE - PART NUMBERS NOT CHANGED

	WORK	NUMBER	REQD	NUT	SLEEVE	REQD	ZONE SHT	TUBE	WALL		HEAT		TUBING	TYPE	MIN
	PRESS.	TUBE ASSY		END FITTING	GS PER TUBE AS	sy	ZONE		THICK	MATERIAL	TREAT	FINISH	IDENT- IFICATION	ENDS	LGTH

TRANSPORT DIVISION GA MIC AIDS WEEKLY REPORT

707

The following new and revised transparencies were released during the week ending June 27, 1957.

NEW

121-22-6 121-23-1 121-21-40 121-73-10 121-21-39 121-77-1 436-21-25	PB-20D Autopilot Rudder Control Circuit Electronic Rack Electrical Cooling Circuit Cabin Pressurization - Rate Control and Jet Pump Operation Puel Pressure Indicating System Schematic Cabin Pressurization - Safety Relief Operation Engine Pressure Ratio System Schematic Pressurization System
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REVISED

121-21-24	Rev B	Turbocompressor Operational Flow Diagram
121-22-1	Rev A	PB-20D Autopilot Power Supply
121-26-1	Rev C	Engine Fire Detector
138-21-25	Rev A	Pressurization System
121-21-25	Rev D	Pressurization System

The following Art Orders and Change Art Orders were received during the week ending June 27, 1957.

ART ORDERS

121-SP15	Selecte	d 707	System	ms Chart (2)
121-26-6	Engine	Fire	Switch	Schematic	

CHANGE ART ORDERS

121-82-1	Rev C	Engine Water Injection System
121-27-15	Rev A	Wing Flap System Schematic
121-82-3	Chg 1	Water Pump and Drain Valves
121-79-5	Chg 1	Engine Oil Tank
121-24-26	Chg 2	Radio and T-R Circuit Breaker Panel (P5)

During the week ending June 27, 1957 additional time was requested for incorporation of the following Master Changes on Graphic Aids Transparencies.

MC	HOURS	MC	HOURS
460-4	10	445-4	35
460-5	10	448	20
460-6	10	508-3	140
460-8	10	508-2	140
460-9	10	496-23	35
659-23	20	496-22	35
560-3	30	TOTAL -	

707 Weekly Report (June 27, 1957) Page Two

707 STATUS

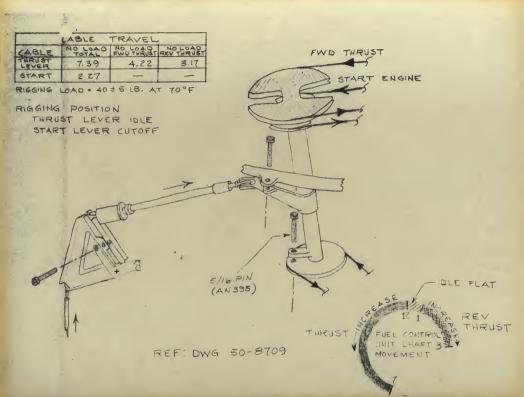
Backlog Status as Follows:	NUMBER	TO COMPLETE
Art orders unassigned Art orders in work	14	840
Change A.O. unassigned	69	2070
Change A.O. in work	5	20 50
Customer A.O. unassigned	2	100
Customer A.O. in work Customer C.A.O. in work	13	260
The state of the s	-	10
		Total Hours - 3350

D. D. True Graphic Aids Group

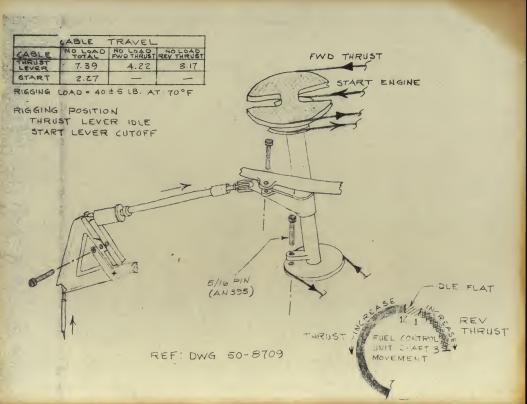
	N.							
	CABLE	TRAVEL						
CABLE	NO LOAD	NO LOAD FWO THRUST			FWD T	unue T		
THRUST	7.39	4.22	3.17		FW6 1	HRUSI		
START	2.27	******	-		1000	ART EN		
RIGGING I	DAD = 40	± 5 LB. A	70°F	1	3 51	APCI EN	AINE	
PIGGING	POSITIO	. 1						
THRU:	ST LEVE	RIDIF				5		
START	LEVER	CUTOFF				7		
3	4,			9	1			
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				1		ASE	Alineus.	
	1			1		2	12 1 1 8	REV
	11				THRUST	3	The Park	THRUST
					HL(0.2)		CONTROL ME	,
		R	EF: DW	G 50-8709	'	MOVE	MENT	
						M.		
						7		

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41 -7 10 1 9

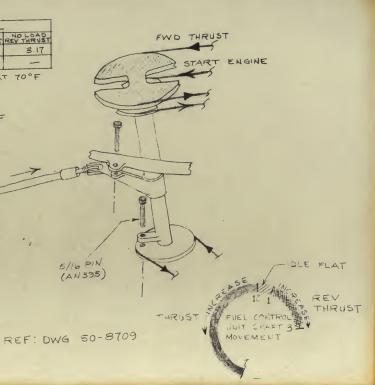


CABLE TRAVEL	
CABLE NO LOAD NO LOAD NO LOAD FWO THRUST	FWD THRUST
TARUST 7.39 4.22 3.17	
RIGGING LOAD = 40 ± 5 LB. AT 70°F	START ENGINE
RIGGING POSITION THRUST LEVER IDLE	5
START LEVER CUTOFF	
9	
or Mile	
The state of the s	
	-
7	
5/16 PIN (AN395)	DLE FLAT
(AN333)	SE V
A	22 12
V.T	THRUST THRUST
DEF: 000 =0 0700	THRUST FUEL CONTROLLER
REF: DWG 50-8709	MOVEMENT



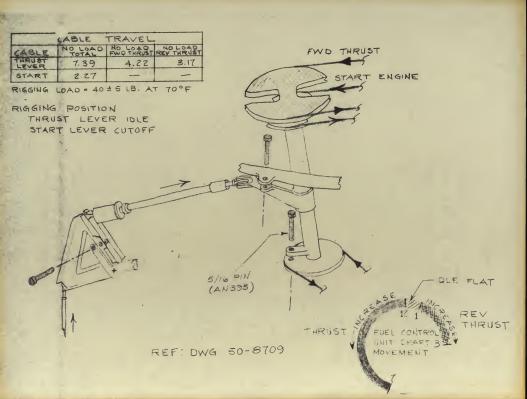
۰	CABLE TRAVEL									
	CABLE	NO LOAD	NO LOAD THRUST	REV THRUST						
	THRUST	7.39	4.22	3.17						
	START	2.27	-							
	RIGGING LOAD = 40 ± 5 LB. AT 70°F									

RIGGING POSITION THRUST LEVER IDLE START LEVER CUTOFF



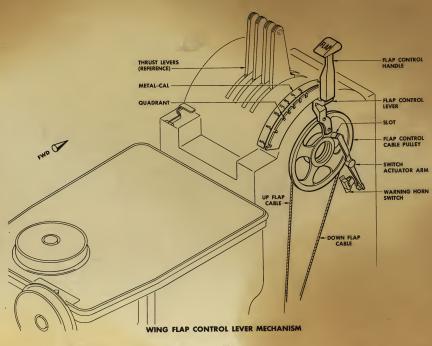
	CABLE	TRAVEL					
CABLE	NO LOAD	NO LOAD	REV THRUST		WO THRUST	r	
THRUST LEVER	7.39	4.22	3.17		141(05)		
START	. 2.27		_	1000	START	ENGINE	
RIGGING I	DAD = 40	± 5 LB. A-	70°F	CHI E	3 3121	CHOINE	
RIGGING	POSITIO	N			7		
THRUS	T LEVE	R IDLE			Charles on the same of the sam		
START	LEVER	CUTOFF					
	š.			9			
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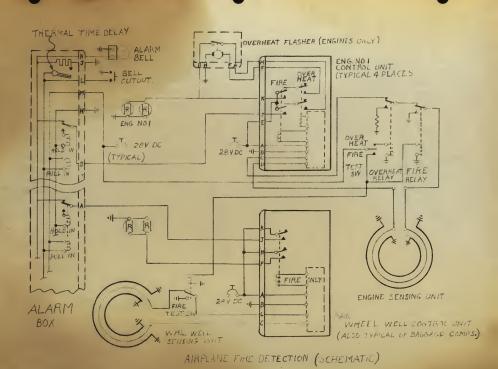


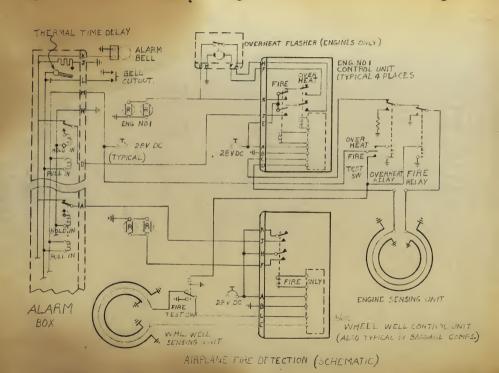
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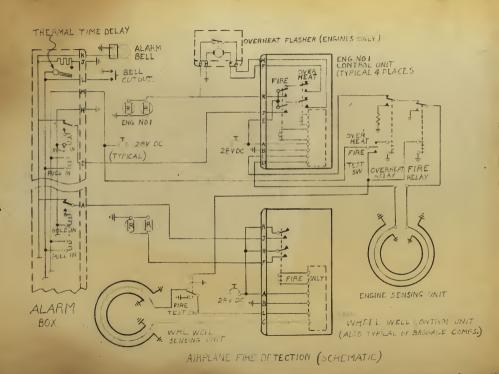
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TRANSPORT DIVISION GRAPHIC AIDS WEEKLY REPORT

707

The following new and revised transparencies were released during the week ending July 11, 1957.

MEW

121-31-8	Pilots' Instrument Panel - Center and Right Shield
121-25-14	Forward Lavatory Compartment
121-23-12	Audio Selector Panel - Microphone Switching
121-31-7	Pilots' Instrument Panel - Left
121-23-4	Essential Electronic and Radio Power Distribution
121-31-9	Pilots' Instrument Panel - Right
707-138	Page 21 - Fuel Tank Arrangement
707-138	Page 29 - Pressurization System
138-82-4	Engine Driven Water Injection Pump
123-21-8	Vapor Cycle System Installation
121-23-13	Interphone Amplifier - Telephonies 20035
121-22-4	PB-20D Autopilot Elevator Control Circuit I
121-82-3	Water Pump and Valve Details
123-28-27	Pressure Fueling Station
120-26-5	Engine Fire Extinguishing System
121-25-9	Cargo Webbing

REVISED

121-32-14 Rev A Main Landing Gear Actuator Schem 121-35-1 Rev B Oxygen System	matic	System stor Sche	ction Sys Actuator	Gear	anding	Main I	r A	Ret	121-82-1 121-32-14 121-35-1
--	-------	---------------------	-----------------------	------	--------	--------	-----	-----	-----------------------------------

The following Art Orders and Change Art Orders were received during the week ending July 11, 1957.

120-34-10	Bendix Flight Director System -2
120-34-11	Bendix Flight Director System -3
120-34-12	Bendix Flight Director System -4
120-34-13	Donata Firent Director System -4
120-34-14	Bendix Flight Director System -5
	Bendix Flight Director System -6
120-34-15	Bendix Flight Director System -7
328-25-5	Interior Arrangement
328-8P-16	Cover Page (Front) Air France Brochure
329-8P-16	Cover Page (Front) Sabena Brochure
328-SP-17	Back Cover Page - Air France Brochure
329-8P-17	Back Cover Page - Sabena Brochure
328-6-1	Principal Dimensions-AF Brochure
329-6-1	Principal Dimensions-Sabena Brochure
328-25-5	Tricapar Dimensions-Sabens Brockire
329-25-5	Interior Arrangement-AF Brochure
	Interior Arrangement-Sabena Brochure
328-25-6	Control Cabin Arrangement-AF Brochure
329-25-6	Control Cabin Arrangement-Sabena Brochure
328-51-1	Section Breakdown AF Brochure
329-51-1	Section Breakdown Sabena Brochure
138-91-1	Typical Flight Profile Sydney to Madi (Brochure)
121-25-30	Passenger Service Unit
121-25-31	Passenger Service Unit Details
	TARREST PETATOR OUT PROPERTY

707 Weekly Report (July 11, 1957) Page Two

CHANGE ART ORDERS

121-24-24	Rev B	115V AC Circuit Breaker Panel No. 3(P3)
121-24-22	Rev A	28V Service and 115V AC Circuit Breaker Panel No. 1 (Pl)
121-28-8	Rev A	Fuel Tank Removable Component Seals
121-24-23	Chg 1	115V AC Circuit Breaker Panel No. 2 (P2)
121-24-25	Chg 1	115V AC Circuit Breaker Panel No. 4 (P4)
121-24-27	Chg 1	Essential 28V Circuit Breaker Panel (P6)
121-24-28	Chg 1	28V AC Circuit Breaker Panel (P7)

During the week ending July 11, 1957 additional time was requested for incorporation of the following Master Changes on Graphic Aids transparencies.

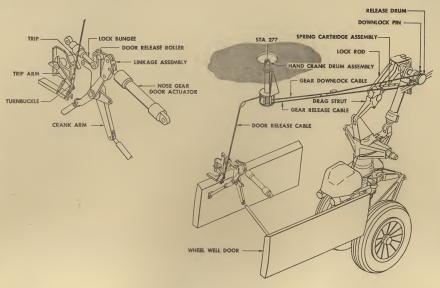
MC	HOURS
733 517-3 264-1	20 55 20
496-7	215
TOTAL.	310

707 STATUS

Backlog Status as Follows:	NUMBER	TO COMPLETE
Art orders unassigned Art orders in work	9	540 21.00
Change A.O. unassigned Change A.O. in work	1 7	20
Customer A.O. unassigned	8	70 240
Customer A.O. in work Customer C.A.O. in work	22 1	140 10
		Total Hours - 3420

D. D. True Graphic Aids Group





EMERGENCY NOSE GEAR AND DOOR RELEASE

13 JULY 1956

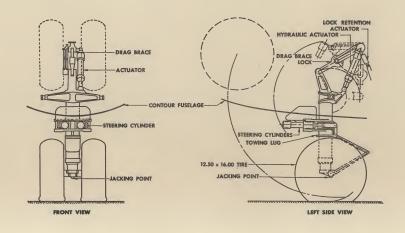
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7G19

7G10 REV A

REV 2 OCTOBER 1956

707-121 1 THRU 99

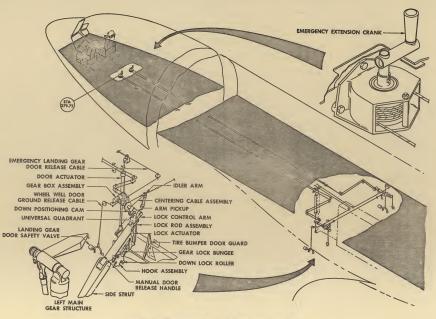


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REV 2 OCTOBER 1956

707-121 1 THRU 99

7G2 REV A

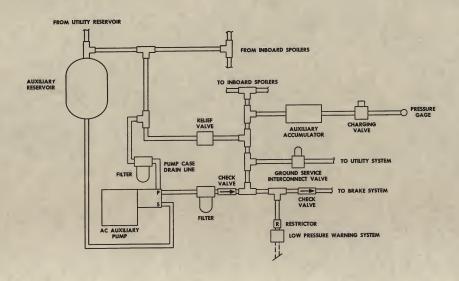


MAIN GEAR EMERGENCY EXTENSION SYSTEM

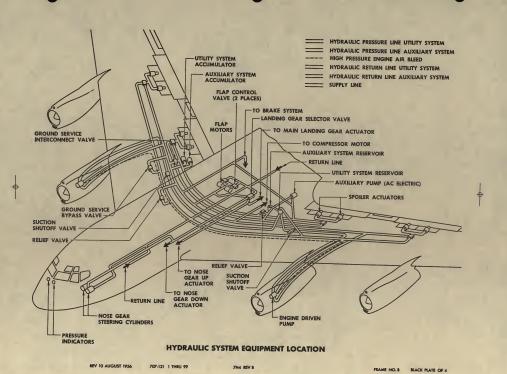
13 JULY 1956

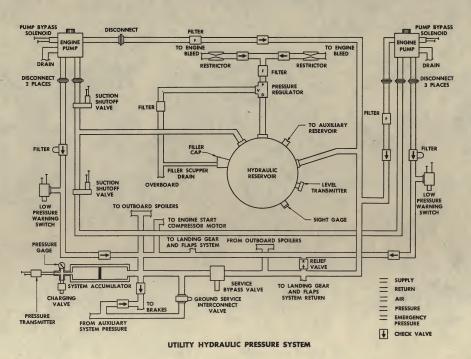
707 1 THRU 1999

7G18

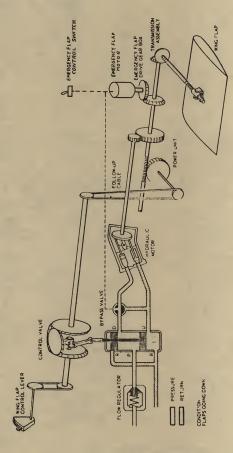


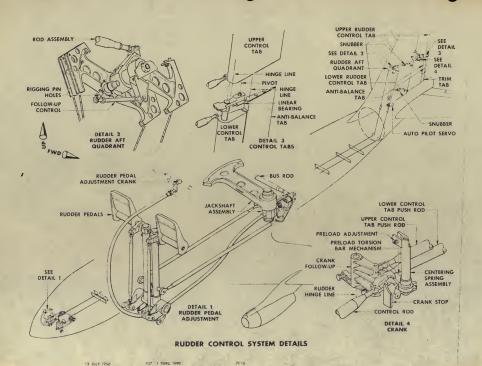
AUXILIARY HYDRAULIC PRESSURE SYSTEM





REV 31 AUGUST 1956 707-121 1 THRU 99 7H2 REV A FRAME NO. B BLACK PLATE OF 4





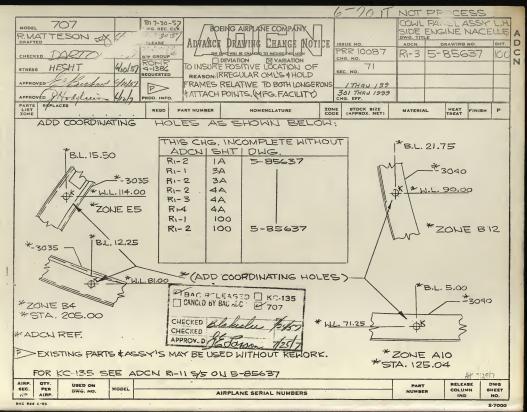


TABLE OF CONTENTS

Prefacea
Introductionb
LANDING GEAR
Main Landing Gear1
Main Gear Doors5
Nose Landing Gear7
Nose Gear Boors9
CABLE CONTROL & DRIVE SYSTEMS
Cable Control System Components11
Landing Gear12
Control Stand16
Control Columns21
Ailerons22
Aileron Trim26
Elevator28
Rudder30
Rudder Trim3h
Stabilizer Trim35
Spoilers39
Speed Brakes
Engine Controls42
Brakeshlu
Nose Wheel Steering
Wing Flaps
Wing Flap Drive47
FLIGHT CONTROL SURFACES
Ailerons
Mevator52
Horisontal Stabilizer53
Rudder55
Fin
Wing Flaps
Cove Lip Doors60
Fillet Flaps62
Spoilers63
DOORS AND WINDOWS
Sliding Windows65
Forward Entry Door66
Aft Entry Door
Forward Galley Door (1-99, 201 and on)68
Forward Galley Door (101-199)70
Aft Galley Door71
Forward Cargo Door73
Center Cargo Door74
Aft Cargo Door75
Emergency Hatch76
EQUIPMENT
Air Conditioning (Vapor Cycle)
Air Conditioning (Air Cycle)78
Windshield Wiper79
FUEL
Fuel Dumo Chute80

Table of Contents (Continued)

HYDRAULICS Gear Box, Auxiliary Hyd. System Pump
POWER PLANT JT3C-6 Engine .81 JT6LA-3 Engine .81A Generator Constant Speed Drive .82 Fuel Air Starter .83 Air Compressor, Starter Air Bottle .81
Gear Box. Water Injection Pump

BAC 1546 L-R3

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ITEM OR COMPONENT DETAIL LUBRICATION LIST FOR 707 AIRPLANES PAGE NO. 1 OF __ PAGES. MFGRS. NO. D 6-1539 MAIN LANDING GRAR LH AND RH BOEING AIRPLANE COMPANY DATE LAST REVISION SEATTLE 14, WASHINGTON DATE APPROVED ITEM NO. OF BEARING METHOD OF LUBRICATION POINT LUBRICATION APPLICATION NO. LUBRICANT TYPE APPLICATION INTERVAL REMARKS POINTS 1 Wheel Bearings R MIL-1-3545 Hand Pack At tire Clean axle and bearing of old grease. Repack bearing and chance grease bearing cup only. Apply no grease to hub. (Drawing 50-5530) 2 Exposed inner SS MIL-0-5606 Noted Post Flight Wipe clean and apply a light cylinder piston film of oil. surface Truck Pivot. MIL-G-3278 #1 1 zerk fitting on each side of inner cyl. fork (Drawing 50-9710) Torsion Links P MIL-G-3278 Gum 6 #1 3 zerk fittings on each link (Upper and lower) (Drawing 50-9723) Centering Cylinder P MIL-G-3278 2 #1 Zerk fitting in end of each Assy attaching bolt. (Drawing 50-9760) Smubber Assembly P MIL-G-3278 Gun 2 #1 Zerk fitting in end of each attaching bolt. (Drawing 50-9760) Brake Collar P MIL-G-3278 #1 2 serk fittings in each a collar (Drawing 90-8658)

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	COMPONENT	BOEIN	L LUBRICATI G AIRPLANE		PAGE NO. <u>1.</u> OF PAGES MFGRS. NO. D 6-1539 DATE LAST REVISION DATE APPROVED		
ITEM NO.	LUBRICATION POINT BEARING TYPE LUBRICANT APPLICATION POINTS LUBRICATION INTERVAL						REMARKS
22	Crank Assembly Lock	P	MIL-G-3278	Gun	1	#1	Zerk Fitting (Drawing 9-63252)
23	Link Assembly, Crank to hook con- necting lirk	ND	MIL-G-3278	Gun	2	#1	Flush Type (Drawing 6-73382)
24	Hook Assembly Support structure	P	MIL-0-3278	Gun.	2	#1	Zerk Fitting (Drawing 5-85682) for lubrication at hook pivot point.
25	Bungee, lock	SS	MIL-G-3278	Gran	2	#1	Flush Type (Drawing 66-4092)

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*								
		COMPONENT	BOEIN	L LUBRICATION G AIRPLANE (LE 14, WASHI)	COMPANY	PAGE NO. 7 OF PAGES MFGRS. NO. D6-1539 DATE LAST REVISION DATE APPROVED		
=	ITEM NO.	LUBRICATION POINT	BEARING TYPE	LUBRICANT	METHOD OF APPLICATION	NO. OF APPLICATION POINTS	LUBRICATION	REMARKS
	1	Wheel Bearings	R	MII-G-2545	Hand Pack	ļŧ	At tire change	Clean axle and bearing of old grease. Repack bearing and grease bearing cup surface only. Apply no grease to hub. (50-5531).
	2	Exposed inner cylinder piston surface	SS	MIL-0-5606	Noted	-	Post Flight	Wipe clean and apply a light film of oil. Drawing (5-83069 Sht. 1A)
	3	Lock Assembly (Drag brace & lock rod)	P	MIL-G-3278	Chun	6	#1	5 exposed flush type fittings and 1 flush type inside of drag brace accesible only by removing plug in side plate (Drawing 65-h829).
	Ł.	Oleo to drag brace	P	MIL-G-3278	Gun	2	#1	2 zerk fittings in steeple of outer cylinder (Dwg. 65-4854).
	5	Torsion Links	Р	MIL-G-3278	Gun	h	#1	3 zerk fittings on lower link and 1 on upper link.(Drawing 5-72334).
	6	Connecting Link towing and steer- ing, nose gear	Р	MIL-0-3278	Gun	1	#1	Flush fitting (Drawing 90-5288)

ITEM OR COMPONENT

CONTROL SYSTEM ALLERON - OUTED DETAIL LUBRICATION LIST FOR

707 AIRPLANES

PAGE NO. 25 OF PAGES
MFGRS. NO. D6-1539
DATE LAST REVISION
DATE APPROVED

BOEING AIRPLANE COMPANY SEATTLE 14, WASHINGTON

NO.	LUBRICATION POINT	BEARING TYPE	LUBRICANT	METHOD OF APPLICATION	NO. OF APPLICATION POINTS	LUBRICATION INTERVAL	REMARKS
n	Bevel Gear Shaft Brg.	В	MII0-5606	Oil Bath	1 LH 1 RH	Overhaul	Used in oil filled box. (Dwg. 5-87199)
12	Bevel Gear Brg.	BD	MTL-0-5606	Oil Bath	1 LH 1 RH	Overheul	Used in all filled box. (Dug. 5-87199)
13	Locksut Mach. Gearbox	SS	MIL-0-5606	Can	1 LH 1 RH	Overhenl	Maintain oil level at fill plug. (Dwg. 5-87199)
14	Torque Tube Splined Joints	88	MIL-G-3278	Hand	2 LH 2 RH	Overhaul.	Clean & lubricate all splined joints. Wipe off excess. (Deg. 9-49684)
15	Lockout Mech. U-Jeints		MIL-L-7E18	Hand	1 LH 1 RH	Overhaul.	Apply a light cost of lubricant (Dwg. 6-72hhl)
	Bevel Gear Splined Joints	88	MIL-G-3278	Hand.	1 LH 1 RH	Overhaul	Clean & lubricate all splined joints. Wipe off excess. (Dwg. 5-87199)
17	Brg. Retainer		MIL-G-4343	Hand.	1 LH 1 RH		Light coat prior to instl. (Dwg. 6-72442)
18	Seal Plate		MIL-G-4343	Hand.	1 LH 1 RH		Light coat prior to instl. (Dug. 9-61767)
	Cables, Pullays & Pres. Seals				1		Refer to Page 11

ITEM OR COMPONENT

CONTROL SYSTEM RUDDER TRIM

(50-8706)

DETAIL LUBRICATION LIST FOR

707 AIRPLANES

PAGE NO. 31 OF PAGES
MFGRS. NO. D 6-1539
DATE LAST REVISION _____
DATE APPROVED _____

BOEING AIRPLANE COMPANY SEATTLE 14, WASHINGTON

HEM CN	LUBRICATION POINT	BEARING TYPE	LUBRICANT	METHOD OF APPLICATION	NO. OF APPLICATION POINTS	LUBRICATION INTERVAL	REMARKS
1	Brake Mechaniam	-	MIL-G-3278	Hand	1	Overhaul.	Disassemble, wipe clean & grease plate teeth rachet plunger, spring & saturate felt washer with grease. Avoid getting lubri. on brake surfaces. (Dug. 9-16057.)
2	Act. Support Brgs. (In Hang.)	В	MIL-G-3278	Prepacked	2	None	Prepacked Brg. (Dwg. 50-6294.)
3	Cable Drum Brg	В	MIL-G-3278	Prepacked	2	None	Prepacked Brg. (Dwg. 60-2873.)
4	Brake Plate Brg.	В	MIL-G-3278	Prepacked	3	None	Prepacked Brg. (Dwg. 50-629h.)
5	Rudder Trim Rod End Brg.	BD	MIL-G-3278	Prepacked	3	None	Prepacked Brg. (Dwg. 9-67646-6, 9-48057.)
6	Linkage Arm Brgs.	В	MIL-G-3278	Prepacked	2	None	Prepacked Brg. (Dwg. 50-6311 on 5-97693.)
7	Actator Screw	BS	MIL-G-3278	Hand	1	#14	Wipe clean apply light coat of grease, operate one cycle & wipe off excess (Dwg. 50-629h.)
8	Cables, Pulleys & Press. Seals						Refer to Page 11.
9	Tab Damper Crank Brg.	В	MIL-G-3278	Prepacked	2	None	Prepacked Brg. (Dwg. 69-4752.)
	LT .						

ITEM OR COMPONENT DETAIL LUBRICATION LIST FOR AIRPLANES PAGE NO. 39.0F PAGES MFGRS, NO. D 6-1539 CONTROL SYSTEM DATE LAST REVISION _1/1/58 BOEING AIRPLANE COMPANY SPOILER - INBOARD (50-8701) DATE APPROVED _____ SEATTLE 14, WASHINGTON NO. OF ITEM BEARING METHOD OF LUBRICATION APPLICATION LUBRICANT APPLICATION LUBRICATION POINT REMARKS TYPE NO. INTERVAL POINTS MTT.-G-3278 Prepacked 2 LH None Prepacked Brg. (Dwg. 5-97095. Follow-up Crank Brgs B 3 60-2739). 2 RH Prepacked Brg. (Dwg. 5-97628). Differential Support В MTT.-G-3278 Prepacked L LH None 2 h RH iArm Bres. Prepacked Brg. (Dwg. 90-2906). MIL-G-3278 2 T.H None Spring Cartridge BD Prepacked 2 RH Rod End Brg. Disassemble, wipe clean and SS MIL-G-3278 Hand T.H. Overhanl h Spring Cartridge 3 RH grease control rod & ID of casing (Dwg. 90-2906). Prepacked Brg. (Bwg. 90-1512.) Valve Crank Arm Brg В MIL-G-3278 Prepacked 3 LH None 3 RH #), Apply few drops (Dwg. 30-3551). MIL-L-7870 Can 7 T.H 6 Valve Soring Swivel SS 3 RH Bushing Prepacked Brgs. (Dwg. 5-98321. MIL-G-3278 Prepacked 8 LH Linkage Rod End Brg BD None 5-97095. 5-98319.) 8 RH Refer to Page 11. 8 Cables, Pulleys & Pressure Seals MTL-G-3278 Prepacked 2 LH None Prepacked Brgs. (Dwg. 50-6875.) 9 Centrol Valve Inbd В 2 RH MIL-0-5606 Can 1 LH Overhaul With slide in any position, fill gear box to level .75 ± .10 in. 1 RH OT below surface of vent plug boss. Skydrol 11500H FAR Refill if level drops 1.25 in. below boss. (Dwg. 65-7018, 50-Applicable 6875, 5-98319).

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	CONTROL SYS	R COMPONENT (STEM SPOILER - OUTBD (50-8701)	BOEIN	IL LUBRICATION OF THE 14, WASHIN	COMPANY	707 AJRP	PLANES	PAGE NO. <u>10</u> OF PAGES MFGRS. NO. D 6-1539 DATE LAST REVISION 11-18-57 PAGES
	ITEM NO.	LUBRICATION POINT	BEARING TYPE	LUBRICANT	METHOD OF APPLICATION	NO. OF APPLICATION POINTS	LUBRICATION	REMARKS
	1	Spring Cartridge Rod End Brg.	BD	MIL-G-3278	Prepacked	2 LH 2 RH	None	Prepacked Brgs. (Dwg. 90-2906).
	2	Spring Cartridge	SS	MIL-G-3278	Hand	1 LH 1 RH	Overhaul	Disassemble, wipe clean & grease control rod and ID of casing (Dwg. 90-2906).
	3	Valve Crank Arm Brgs	В	MIL-G-3278	Prepacked	3 LH 3 RH	None	Prepacked Brgs. (Dwg. 90-1512, 5-98386).
	4	Valve Spring Swivel Brg.	SS	MIL-L-7870	Can	1 LH 1 RH	#4	Apply few drops (Dwg. 30-3551).
		Diff. Support Arm Brgs.	В	MIL-0-3278	Prepacked	4 LH 4 RH	None	Prepacked Brgs. (Dwg. 6-84607, 5-98304).
	6	Linkage Rod End Brgs	BD	MIL-0-3278	Prepacked	9 LH 9 RH	None	Prepacked Brgs. (Dwg. 50-1514, 5-98304).
	7	Idler Arm Brgs.	В	MIL-G-3278	Prepacked	2 LH 2 RH	None	Prepacked Brgs. (Dwg. 9-67067).
	8	Follow-up Arm Brgs.	В	MIL-0-3278	Prepacked	2 LH 2 RH	None	Prepacked Brgs. (Dwg. 9-67511, 50-1514).
		Cables, Pulleys & Pressure Seals						Refer to Page 11.
R	10=	Control Valve Outbd		MIL-0-5606 er Skydrol #500# (As Applicable)		1 LH 1 RH	Overhaul	With slide in any position, fill gear box to level .75 ± .10 in. below surface of vent olug boss. Refill if level drops 1.25 in. below boss. (bwr. 50-6875, 65-
				MIL-G-3278		2 LH 2 RH	None	7018, 5-98386).

ENGINE	OR COMPONENT CONTROL SYSTEM 50-8709)	BOEIN	IL LUBRICATION OF THE 14, WASHII	PAGE NO. 12 OF PAGES MFGRS. NO. 16-1537 DATE LAST REVISION DATE APPROVED			
METI CN	LUBRICATION POINT	BEARING TYPE	LUBRICANT	METHOD OF APPLICATION	NO: OF APPLICATION POINTS	LUBRICATION INTERVAL	REMARKS
1	Engine Start Shaft Brgs.	В	MIL-G-3278	Prepacked	8 (2/eng.)	None	Prepacked Brgs. (Dwg. 65-2318, 65-2445).
2	Eng. Throttle Control Shaft Brgs.	В	MIL-G-3278	Prepacked	8 (2/eng.)	None	Prepacked Brgs. (Dwg. 65-2318, 65-2445.)
3	Fuel Shutoff Valve Rod End Brgs.	BD	MIL-G-3278	Prepacked	8 (2/eng.)	None	Prepacked Brgs. (Dwg. 65-6616.
<u> 1</u> 4	Eng. Start Control Rod End Brgs.	BD	MIL-G-3278	Prepacked	16 (lt/eng.)	None	Prepacked Brgs. (Dwg. 69-29hh, 60-29h3, 69-29h2.)
5	Switch Reset Cam Brg.	В	MIL-G-3278	Prepacked		None	Prepacked Brgs. (Dwg. 65-2173)
6	Switch Reset Cam	SS	Dry Film	-		None	No lubrication necessary. (Dwg. 65-2173)
7	Thrust Reverser Control Shaft Brgs.	В	MIL-G-3545	Hand	8 (2/eng.)	None	Remove seals, clean & repack (Dwg. 65-29h2, 65-2867.)
8	Eng. Start Control Rod Brg.	BD	MIL-0-3278	Prepacked	ц	None	Prepacked Brgs. (Dwg. 69-2943.
9	Eng. Throttle Contri	. В	MIL-G-3278	Prepacked	Ţ	None	Prepacked Brgs. (Dwg. 65-2868
10	Eng. Throttle Control Pulley Brgs.	В	MIL-0-3278	Prepacked	8	None	Prepacked Brgs. (Dwg. 69-2594

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Spagnal "Laudin		R COMPONENT SYSTEM WING FLAP	BOEIN	IL LUBRICATION OF THE PROPERTY	COMPANY	PAGE NO. <u>16</u> OF PAGES MFGRS. NO. D6—1539 DATE LAST REVISION 11—18—70 DATE APPROVED 1758						
ness	ITEM NO.	LUBRICATION POINT	BEARING TYPE	LUBRICANT	METHOD OF APPLICATION	NO. OF APPLICATION POINTS	LUBRICATION INTERVAL	REMARKS				
	1	Valve Support Brgs	В	MIL-G-3278	Prepacked	2 LH 2 RH	None	Prepacked Brgs. (Dwg. 5-97267.)				
-	2	Cable Drum Crank Brgs	В	MIL-G-3278	Prepacked	2 RH only	None	Prepacked Brgs (Dwg. 5-9587h on 65-6889).				
	3	Linkage Rod End Brgs	BD	MIL-G-3278	Prepacked	lı	None	Prepacked Brgs. (Dwg. 5-97267).				
	4	Flap Position Trans- mitter Arm Brg.	В	MIL-C-3278	Prepacked	1 LH only	None	Prepacked Brg. (Dwg. 66-3515 on 5-97267).				
		Cable Pulleys & Pressure Seals						Refer to page 11.				
	6	Flap Control Valves		MIL-0-5606 or Skydrol 500 (As Appli- cable)		2	overhau1	With slide in any position, fill gear box to level .75 ± .10 in. below surface of vent clug boss. Refill if level drops 1.25 in. below hoss. (Dwg. 50-6875, 5-97267).				

7	•	J. S.	7-1		•		<i>*</i> 8	-
ta	CONTROL SY	R COMPONENT STEM FLAP DRIVE 8708)	BOEIN	L LUBRICATION OF THE 14, WASHI	COMPANY	PAGE NO. <u>1.7</u> OF PAGES MFGRS. NO. D6 <u>1539</u> DATE LAST REVISION <u>11-18</u> -57 DATE APPROVED		
***	MBT! .CM	LUBRICATION POINT	BEARING TYPE	LUBRICANT	METHOD OF APPLICATION	NO. OF APPLICATION POINTS	LUBRICATION	REMARKS
R	1	Power Unit Brgs	В	MIL-0-5606	Oil Bath	6/unit	Overhaul	Used in oil filled box (1 unit LH, 1 unit ?W) (Dwg. 5-88130).
R	2	Power Unit	SS	MIL-0-5606	Oil Bath	1 LH 1 RH	#14	Check oil level and fill to oil level limits indicated. (Dwg. 5-88130).
	3	Ball Screw Transmiss- ion	SS	MIL-0-5606	Oil Bath	5 LH 5 RH	#4	Maintain oil level with fill plug (Dwg. 5-84049).
	4	Ball Screw Transmiss- ion Brgs	В	MIL-0-5606	Oil Bath	5/unit		Wased in oil filled box (1 unit LH 1 unit RH)(Dwg. 5-84049.)
	5	Bell Screw	SS	MIL-L-7870	Brush	5 RH	#h	Wipe clean, apply light film of oil, operate one cycle and wipe off excess (Dwg. 5-84049).
	6	Fillet Flap Trans. Support Bushings	P	MIL-G-3278	Gun	2 LH 2 RH	#4	Flush Fitting (1 fitting per bushing) (Dwg. 5-97896).
		Fillet Flap Ball Screw Trunnion Supp. Bushings	P	MIL-G-3278	Gun	2 LH 2 RH	#h	Flush fitting (1 fitting per bushing) (Dwg. 5-80049).
	8	Flap Transm. Supp. Bushings	P	MIL-0-3278	Crun	8 LH 8 RH	#u	Flush fitting (1 fitting per bushing)(Dwg. 5-84049).

CONTROL S	OR COMPONENT SYSTEM FLAP DRIVE -8708)	BOEI	ALL LUBRICAT NG AIRPLANE TLE 14, WASH	COMPANY	PAGE NO. 18 OF PAGES MFGRS. NO. D 6-1539 DATE LAST REVISION DATE APPROVED		
ITEM No.	LUBRICATION POINT	BEARING TYPE	LUBRICANT	METHOD OF APPLICATION	NO. OF APPLICATION POINTS	LUBRICATION INTERVAL	REMARKS
9	Flap ball screw trumion support bushings	P	MIL=G=3278	Gun	8 LH 8 RH	#4	Flush Fitting (Dwg. 5-84019).
10	Fillet flap takeoff gearbox brgs.	В	MIL-0-5606	Oil Bath	6/box	#u	Used in oil filled box (2 gear
п	Fillet Flap T.C. Gearbox	SS	MIL-0-5606	Oil Beth	1 LH 1 RH	#h	boxes) (Dwg. 5-96770 on 5-96771). Check to see that oil is level with fill plug. (Dwg. 5-96770 on 5-96711.)
12	Flap Angle Gearbox BRGS.	В	HIL-0-5606	Oil Bath	lı/box	#)4	Used in oil filled box (2 gear boxes)(Dwg. 5-06771).
13	Flap Angle Gearbox	SS	MIL-0-5606	Oil Bath	1 LH 1 RH	#4	Check to see that oil is level with fill plug. (Dwg. 5-96711).
24	Double Angle Fillet Flap Gearbox Brgs.	В	MIL-0-5606	Oil Bath	8/box	#4	Used in oil filled box (2 gear-boxes)(Dwg. 5-97896.)
15	Double Angle Fillet Flap Gearbox	SS	MIL-0-5606	Oil Bath	8/box	fla	Check to see that oil is level with fill plug(Duy. 5-97896).
	Outbd Torque Tube Support Brgs. (W.S. 615) (W.S. 360)	В	MIL-G-3278	Prepacked	6 LH 6 RH		Prepacked Brgs. (Dwg. 50-8708).
17	Offset Gearbox Brgs	В	MIL-0-5606	Oil Bath	5/Beac	#ls	Used in oil filled box (2 gear boxes)(Dwg. 5-84048).

ITEM OR COMPONENT DETAIL LUBRICATION LIST FOR 707 **AIRPLANES** PAGE NO. 49 OF __ PAGES CONTROL SYSTEM FLAP DRIVE MEGRS, NO. 06-1539 (50-8708) BOEING AIRPLANE COMPANY DATE LAST REVISION SEATTLE 14. WASHINGTON DATE APPROVED ITEM NO. OF BEARING METHOD OF LUBRICATION LUBRICATION POINT APPLICATION LUBRICANT APPLICATION NO TYPE INTERVAL REMARKS POINTS 18 Offset Gearbox SS MIL-0-5606 011 Bath #). 1 14 Check to see that oil is level 1 RH with fill plug (Dwg. 5-84048). 19 Position Transmitter В MIL-0-3278 Prepacked 2/unit None Prepacked Brgs (Dwg. 5-87819). Brgs. 20 Torque Tube Splined SS MIL-G-3278 Brush All. #1 Clean & lubricate all splined Jointa joints. Wipe off excess (Dug. 50-8703). 21 Outbd Torque Tube RD MIL-G-3278 6 LH Gum #4 Flush Fittings (Dwg. 5-731h2. Support Brgs. 6 RH 5-73143). (W.S. 615 & 360) 22 Inbd. Torque Tube RD MIL-3-3278 Gun 2 T.H #15 Zerk Fitting (Dwg. 5-9562h. Support Brgs. 2 RH on 4-5157). (W.S. 252) 23 Cables Refer to Page 11.

ITEM OR COMPONENT

DETAIL LUBRICATION LIST FOR

707

BOEING AIRPLANE COMPANY SEATTLE 14, WASHINGTON AJRPLANES

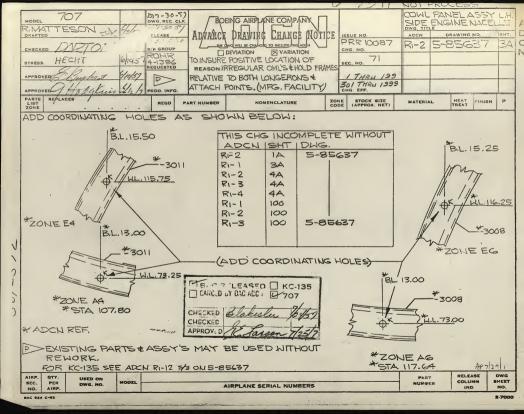
PAGE NO. 52 OF PAGES

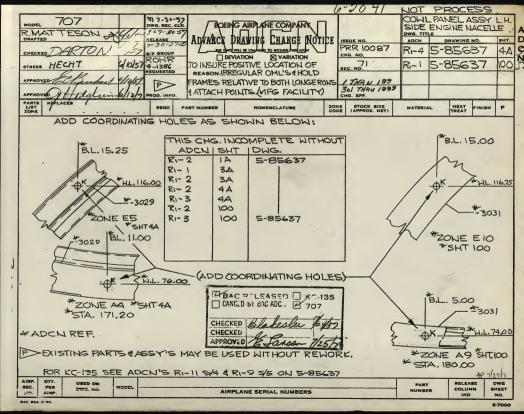
MFGRS. NO. D 6-1539

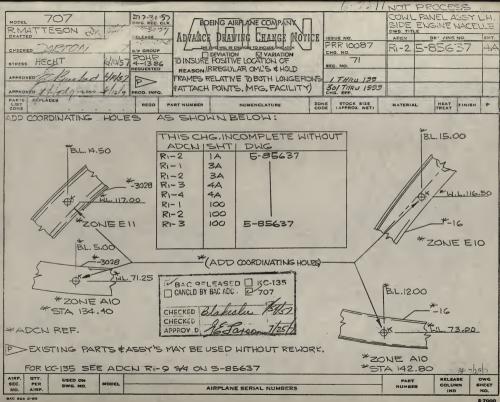
DATE LAST REVISION DATE APPROVED

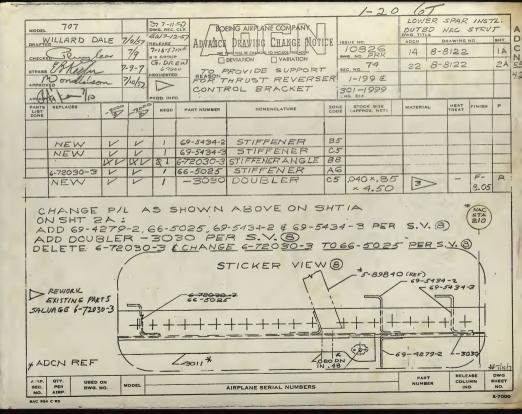
Mati .cn	LUBRICATION POINT	BEARING TYPE	LUBRICANT	METHOD OF APPLICATION	NO. OF APPLICATION POINTS	LUBRICATION INTERVAL	REMARKS
	Typical Elevator Control Tab Hinge Brgs.	1310	MIL-G-3278	Prepacked	8	None	Prepacked Rearing (Dwg. 5-87157)
	Elevator Control Tab Inboard Hinge Brgs.	R	MIL-G-3278	Prepacked	2	None	Prepacked Brg. (Dwg. 5-87157).
	Elevator Control Tab Outboard Hinge Brgs.	В	MIL-0-3278	Prepacked	2	Hone	Prepacked Brg. (Dwg. 5-87157).
	Typical Elevator Hinge Brgs.	RD	MIL-G-3278	Guma	10		Flush Fitting (Dwg. 6-83193).
	Elevator Thrust Hinge (Inbd. Hinge of Elevator)	RD	MIL-G-3278	Gun	1		Zerk fitting (Dwg. 9-65805).
	Elevator - Stab. Actuated Tab Piano Hinge	PH	Dry Film		2	None	No lubrication necessary (Dwg. 5-96311).
	Elevator Balance Penel Piano Hinges	PH	Dry Film		10	None	No lubrication necessary. (Dwg. 5-97214 thru 5-97218).
	Elevator Balance Panel Support Link Brgs.	R	MIL-G-3278	Prepacked	Тю	None	Prepacked Brgs. (Dwg. 5-9721h Thru 5-97218.)
9	Elevator Smabber Assy.	RID I	MIL-G-3278	Gun	2	Overhaul	Flush Fitting (Dwg. 50-1571).

ITEM OF	COMPONENT DER	DETAIL LUBRICATION LIST FOR 707 AIRPLANES BOEING AIRPLANE COMPANY SEATTLE 14, WASHINGTON					PAGE NO. 56_ OF PAGES MFGRS. NO. D 6-1539 DATE LAST REVISION DATE APPROVED		
NO.	LUBRICATION POINT	BEARING TYPE	LUBRICANT	METHOD OF APPLICATION	NO. OF APPLICATION POINTS	LUBRICATION INTERVAL	REMARKS		
9	Support Bearing Upper End of Con- trol Tab & Lwr End of Stability Tab (Tab Actuator Hinge)	ROD	MIL-G-3278	Prepacked	2	None	Prepacked Brg. (Dwg. 5-95502 & 5-95503).		
10	Stability Teb Upper Hinge Brg.	В	MIL-G-3278	Prepacked	1	None	Prepacked Brg. (Dwg. 5-95503.)		
11	Stability Tab Typical Hinge Brgs.	BD	MIL-G-3278	Prepacked	2	None	Prepacked Prg. (Dwg. 5-95503.)		
12	Trim Tab Pieno Hinge	PH	Dry Film		1-	None	Wo lubrication necessary. (Dwg. 5-95501.)		
13	Rudder Balance Panel Linke	R	MIL-0-3278	Prepacked	20	None	Prepacked Brg. (Dwg. 65-97658)		







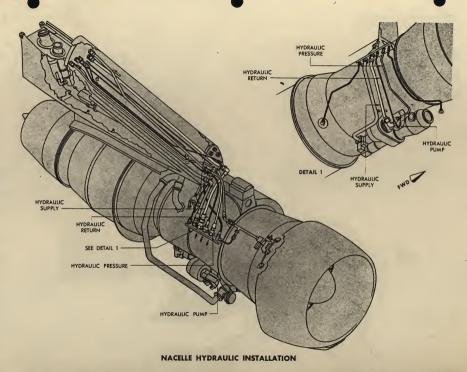


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[C	DE FARE DWG													
AIRP.	AIRP. GTY. USED ON PART COLUMN						COLUMN	SHEET						
SEC.	SEC. PER DWG. NO. MODEL AIRPLANE SERIAL NUMBERS						1		IND	NO.				

BAS 284 C-88

HIP 7/1017 2-7000

7K1 REV A FRAME NO. B YELLOW PLATE OF 3



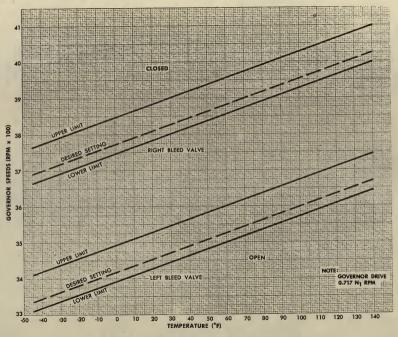
1-487 10.78

6 DECEMBER 1955 KC-135 55-3118 AND ON

5P43

FRAME NO. B

SLIGHT PLATE OF 2



ENGINE COMPRESSOR BLEED VALVE OPERATING LIMITS

4. Toilet System

The toilet is an improved, flushing type unit installed above the floor in the lavatory compartments. The toilet has a minimum capacity of 17 gallons in the space above the tank bottom and below the bottom of the upper bowl. The tank (sump) is made of stainless steel and has a bottom sloped and shaped to enable complete drainage and cleaning of toilet waste out through the drain connection. The toilet bowl is shaped for flush cleaning after each usage and is colored to be compatible with the dye used. A top cover forms the top of the toilet tank. It is attached in a manner that will allow its removal for maintenance and yet form an absolute seal against leakage of the toilet contents. A silicone separator is located in the region between the toilet bowl and tank to prevent the passenger viewing the contents. It also prevents tank contents from sloshing up out of the toilet bowl during flight or landing. The separator is cleaned by flushing of the toilet. A standard home type toilet seat and lid are used. A special handle on the seat and lid facilitate raising and lowering. Only toilet assemblies of the same part number are interchangeable.

B. Flushing Pump and System

The flushing system consists of an electrically driven pump, flushing ring and orifices. Flushing media is recirculated toiler liquid treated with deodorant, disinfectant and dye. Momentarily pressing a flush valve after each usage of the toilet causes the entire toilet bowl and separator to be flushed clean of solid material, toilet seat covers and paper. The toilet completes the flushing cycle and turn-off with no further action by the operator. The toilet cannot be flushed when a person is seated on the toilet seat. The flushing cycle is interrupted if the seat is loaded before the cycle is completed. The pump will drain when the toilet is drained to prevent freezing.

C. Ventilation

A connection on the toilet permits ventilation of the air volume above the liquid level in the toilet tank. During flight ventilation air normally enters under the toilet seat, passes down through the toilet bowl through the ventilation connection and then through plumbing to the outside of the airplane. A maximum cabin pressure differential of \$.6 psi will result in a ventilating rate of 40 cu/ft/min. The ventilation connection is so located that fluids cannot pass through with the ventilating air.

D. Drain Valve and Outlet

An internal bulb type valve is installed in each toilet to seal the toilet tank drain outlet. The valve mechanism is completely enclosed and protected from tollet wastes. A cable control connection is provided for drainage of toilet wastes from the tank when actuated on the ground from a remote panel.

E. Cleansing Spray System

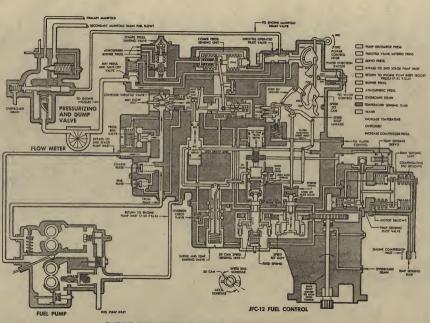
A cleansing spray system enables the tollet bowl and tank interior to be thoroughly flushed out. A connection on the tank permits cleansing solution to be pumped through the system from the tollets service panel on the outside of the airplane through a one inch heavy wall polyethelene pipe. The cleansing system is used to charge the tollet tank with clean deodorant, disenfectant and dye solution.

F. Ground Servicing

The toilets service panel accesses are located it approximately station 304, right side, for the forward toilets and at approximately station 1393, bottom center, for the aft toilets. Each service panel contains a drain connection, two flush line connections and two flush handles which are cable connected to the toilet valves. The connection fittings are equipped with cap covers.

D6-1198

25-18-0 Page 4



ENGINE FUEL METERING SYSTEM SCHEMATIC CUTAWAY

10.56

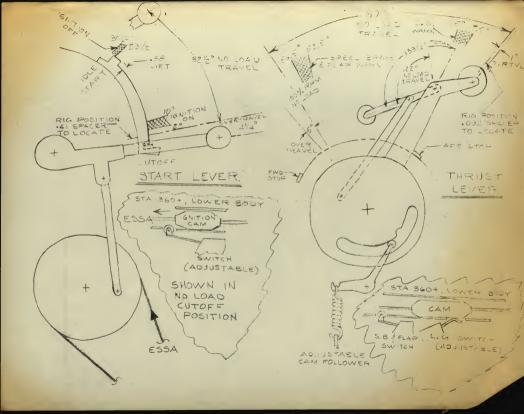
8 NOVEMBER 1955

KC-135 55-3118 AND ON

*077

FRAME NO. 8

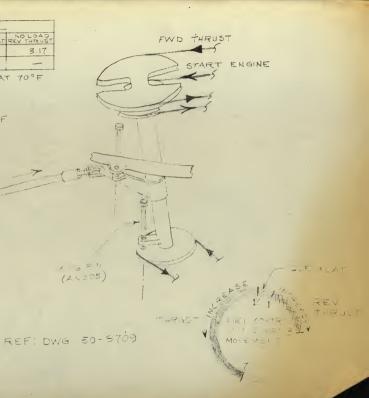
BLACK PLATE OF 5

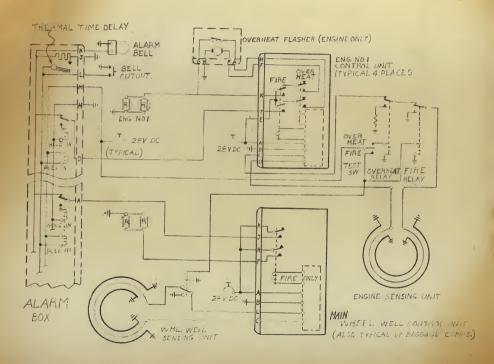


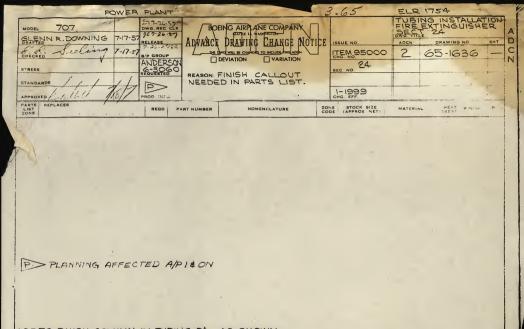
CABLE TRAVEL								
CABLE	NO LOAD	NO LOAD	REV THRUST					
THRUST	7.39	4.22	3.17					
START	227		_					

RIGGING LOAD = 40 ± 5 LB. AT 70°F

RIGGING POSITION
THRUST LEVER IDLE
START LEVER CUTOFF

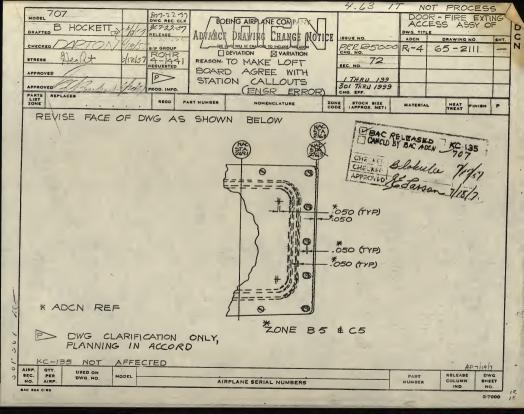


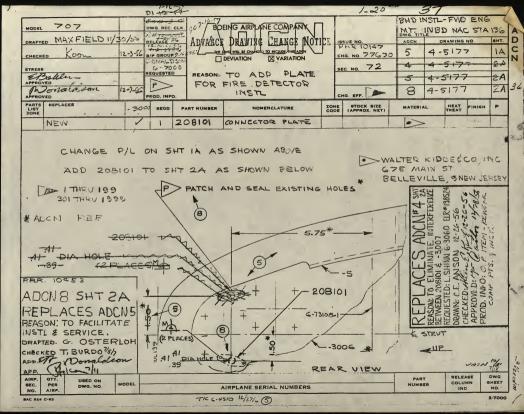




ADD TO FINISH COLUMN IN TUBING P/L AS SHOWN F-2.742 -6 F-2.742 -5 F-2.742 -4 F-2.742 -3 NUMBER REQD NUT SLEEVE REOD ZONE SHT WORK TUBING TREAT FINISH HEAT TYPE MATERIAL STOCK PRESS IDENT-ZONE OD THICK ENDS END FITTINGS PER TUBE ASSY TUBE ASSY IFICATION LGTH PSI CODE

BAL 224 E-82





	ARGO HANDLING		3				5	-80			6
ELR NO.	330 MODEL NO. 767	767-2-57 DWG. REC. CL	K / K	EING AIRPLANE C	ANGE NOTE	4	CILE NO	FIRE DE	ETECTO	E IN	157
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PROD. INFO. PLANNING IN ACCORD

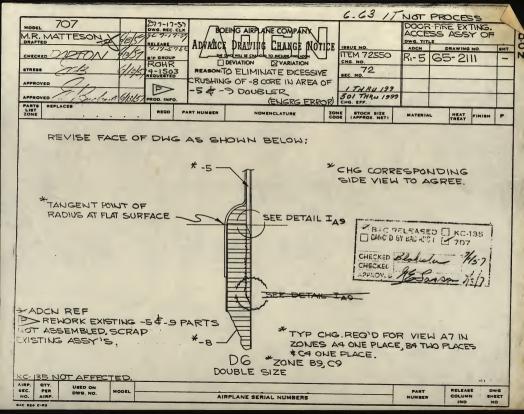
STATUS OF TOOLS

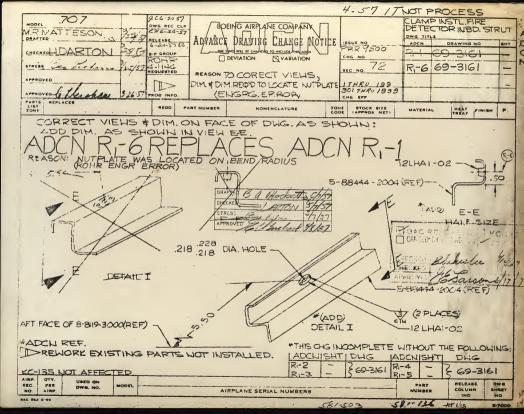
MOR. PLANNING

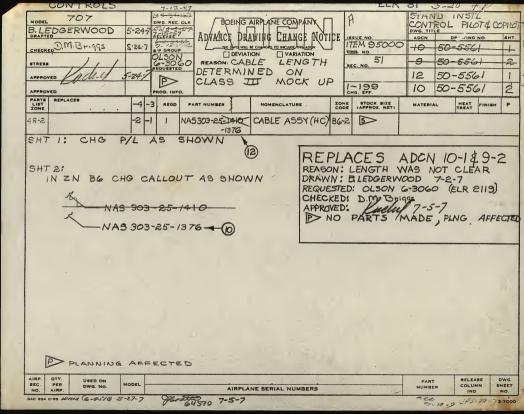
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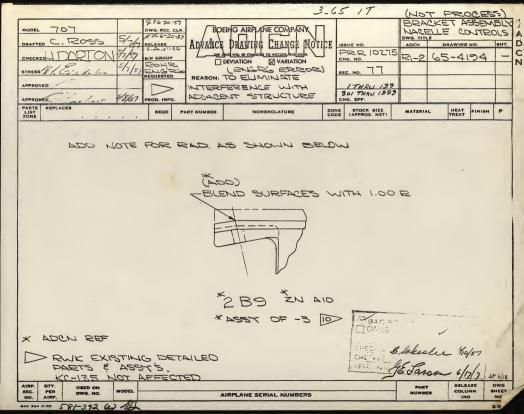
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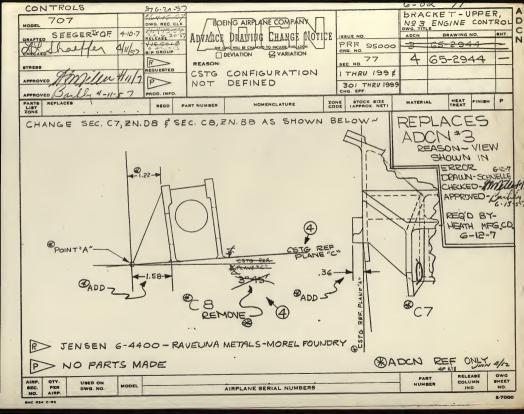
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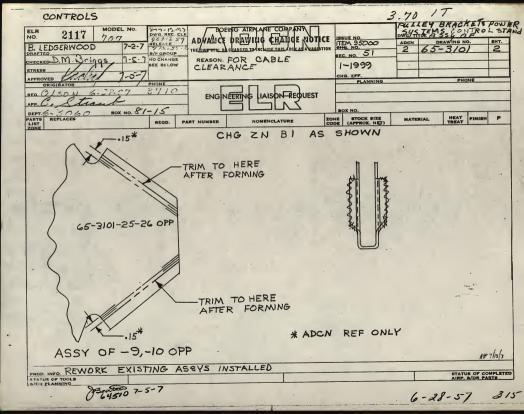












1_50 37 REPRODUCIBLE TO ITO ONLY CONTROL SYSTEM BOEING AIRPLANE COMPANY INSTALLATION DWG TITLE THRUST REVERSER DDA No. DRAWING No. ISSUE NO.

707 DWG REC CLK J.P. DEED DRAWING DEPARTURE AUTHORIZATION THE DWG WILL NOT BE CHANGED CHECKED B/P GROUP PEASON. J822 65-47.59 NEW HI-TEMP PEARSON R STRESS BEARING NOT SEC. NO AVAILABLE AT THIS TIME PROD INFO SHOP INFO ELR OR DCR 65 4259 PADTS REPLACES STOCK SIZE HEAT PART NUMBER MATERIAL. FINISH REOD. NOMENCLATURE CODE LIST BEARING-MARLIN ROCKWELL CORP B5477725 (BAC BIOA-610 IAMES TOWN HY (OF FOUND MORI IN ROCKWEN CORP. BEARING ROD END REPAFT-C3 HAMESTOWN D.Y (OR EQUIL) (BAC BIDA -640 TREARING A4 MARLIN ROCKWELL CORP KP4A-7-ST BAC BICA-GZO HAMESTOWN NY. (OR EQUIL) C7-B 542 BEARING FAFNIR BRG CO. NEW BRITIAN COUN (OR EQUIV.) BAC-BIOA-30 DD) RE 4F5 BEARING ROD END FAFNIR BRG CO. *> (BAC. BIOA-T) HEW ANZOIKP4A SINGLE ROW BALL BEARING



817-11-57

REMOVE NON-METALLIC SEALS & REPACK WITH SHELL. 21176A SILCONE GREASE. OPTIONAL REPLACE NON-METALLIC SEALS WITH TEFLON SEALS



FIRST OWT LINITS MFG'D BY ROHR ONLY



FIRST UNITS MFG'D BY IPD. OKLY FOUR

707 E. SEYMOUR 7-1-57	37 7-3-57 DWG REC. CLN RTL 7/3/57	1 - / . \	DEING AIRPLANE COMPAN'		3	END CONT	ROL S	STAND A	.55Y
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PPROVED PROVED PROVED PROVED 7-2-57	REQUESTED	REASON:	TO BRING TAB UP TO DATE	BLOCK	NO TED				
PARTS REPLACES	للثلث المساور بالأ	ART NUMBER	NOMENCLATURE	ZONE	STOCK SIZE (APPROX. NET)	MATERIA	r -	HEAT FINIS	e P
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	ана	NGE TA	AB BLOCK TO R	a dass	S SHOWN	:			
(ОНА	NGE TA	AB BLOCK TO R	a das	S SHOWN	:			18

AIRPLANE SERIAL NUMBERS

NUMBER

MODEL

DWG NO.

SEC. PER

AIRP.

7-20 247 KC-135 216-25-57 BOFING AIRPLANE COMPANY DWG. REC. CLK D W.L. SMITH CHANGE NOTICE ISSUE NO. ADCN SHT DRAWING NO. du. N PRR 9500 G/20/57 BIP GROUP 5-86801 CHECKED VARIATION CHG. NO. [] DEVIATION 6-7000 5-86803 REASON: TO COMPLETE SEC. NO. REQUESTED CABLE FINISH INFO IN 9 5-86804 GEN NOTES FOR COMPLIANCE 55-3118 40N 5-86805 64 WITH D-15280 (PAR. 3.10.4) CHG. EFF. ROD, INFO PARTS REPLACES ZONE STOCK SIZE PART NUMBER NOMENCLATURE REOD 5-86806 73 CHANGE THE GEN NOTE WHICH CALLS FOR CABLE 8 5-86807 LUBRICATION TO READ AS FOLLOWS : 17 5-86809 22 " LUBRICATE THOSE PORTIONS OF CONTROL CABLES THAT 5-86811 5 22 TRAVEL OVER DRUMS, PULLEYS, QUADRANTS, 5-86812 9 69 & THRU FAIRLEADS, GROMMETS, & SEALS PER BAC 5008 TYPE 9. 5-86814 APPLY PROTECTIVE COATING CONFORMING TO 50-2420 62 MIL-C-16173 GRADE I TO ALL OTHER PORTIONS OF CABLES. " 50-2423 10 5 50-2445 54 5-86813 11 8 5-86816 69

P EXISTING INSTL'S ARE SATISFACTORY

REF DON "B" ON 5-86810 SHEET I

SEC. NO.	PER AIRP.	USED ON DWG. NO.	MODEL	AIRPLANE SERIAL NUMBERS	PART NUMBER	RELEASE COLUMN IND	SHEET NO.
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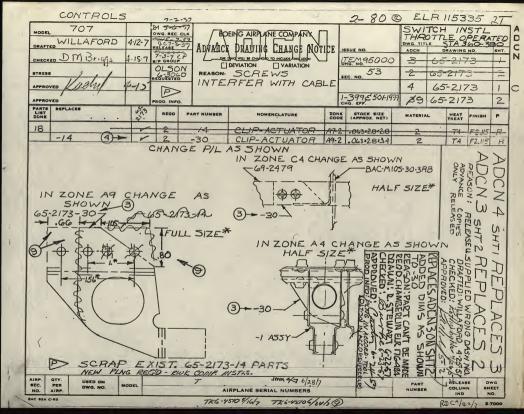
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5-86819

BODY				2.58		
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PARTS REPLACES LIST ZONE REQD	PART NUMBER		ONE STOCK SIZE	MATERIAL	HEAT FINISH	P
	-3	BRACKET		5 RF	2,115	4
CHANGE P/L AS S	+0WN:					

AIRD OOI & ON MUST COMPLY

RELEASE DWG PART AIRP. QTY. USED ON COLUMN SHEET MODEL SEC. PER NUMBER DWG. NO. AIRPLANE SERIAL NUMBERS IND NO. AIRP



	THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER.		TARREST TO STATE OF THE STATE O			titlet la Prince Anna - 165 1			1	0-7	75	IT	
MODEL			0	Sye 1 - 2 WG. REC XH 7/3	CLK BP	EING AIRPLANE COMPANY	1		CO Z	ST	ALLAT	5	A THE
1	CHECKED HELE TO TO THE CHARGE NOTICE ISSUE NO DEVENTION REVENDED TO THE CHARGE NOTICE ISSUE NO DEVENTION REVENTION REPORT NO NO. 291										7 50-870		
STRESS													
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APPROV	10 DEHag	16	-24.7	ROD. INF	> o.			NOTED HE					
PARTS LIST ZONE	REPLACES	-79	-7.7	REQD	PART NUMBER	NOMENCLATURE	ZONE	STOCK SIZE (APPROX. NET)	MATERIA		HEAT FIN	вн	P
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	NEW	8>		2	65-6416-1	VALVE INSTL.	08					-	
	CHANGE PARTS LIST AS SHOWN ABOVE; CHANGE NOTES AS SHOWN; BOUSE ON AIRPLANES 101-189 & 401-489 BOUSED ON AIRPLANES 101-189 & 301-1899												

10> USED ON AIRPLANES 1-994 301-399 4 501-1999

ADD TO ENGINE START SYSTEM RIGGING INSTRUCTIONS! 3. WITH RIGGING PINA INSERTED THRU 65-2320 &

65-2319-1 BRACKET & RIGGING PIN INSTALLED THRU 66-4449 ARM & 10-60003 VALVE, ADJUST & INSTALL GG-4450 ROD. TIGHTEN CHECK NUT & REMOVE RIGGING PINS. (THIS NOTE APPLIES TO AIRPLANE 101-199 & 401-499 OHLY).

> ADDITION OF BAJIC RELEASE FOR AA & TWA

AIRP. GTY. USED ON BEC. PER DWS. NO. OF THE DW	PART	COLUMN IND
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				1-0	06 1	17		
DRAFTED T. BURDO 7/1/67 CELLUS	ADVALCE DE	AIRPLANE COMPANY	FIGE		DWG. TIT		ONTRO	L
CHECKET Flule 7/10/-	- De dura was	HE CHANGE TO INCLUDE THIS ADDIN		PRR 10453.	ADCN	DRAWIN	3 NO.	SHT
1 1 - 11 6-7000	DEVIA	TION TVARIATION	- 1	CHG. NO.	2	65-41	94	-
STRESS 4. Faier /1457 DOWALDSON.		NUTPLATE FOR		SEC. NO. 77				
APPROVED 7/11/	FIRE DE	TECTOR ELEME	· · · — [1-199				
APPROVED CO 7/11			L			•		
PROD. INFO.				301 - 1999 CHG. EFF.				
A	ART NUMBER	NOMENÇLATURE	ZONI	STOCK SIZE	MATERIA	L HEAT	FINISH	P
WEW VVI WS	1-32-2 NUT	BAC-NIODZ-3-20						
			1					
CHANGE PLASE CHANGE PICTURE IN ZONE BG L.H. SIDE VIEW*	** -4* -4* -4*	IN ZONE B	5*		INDU	STERN STRIES, HAVWARD	P.O. BOX	F.
AIRP. QTY. LISED ON							AH 7/15/7	

ATT ANE SERIAL NUMBERS

PART

NUMBER

RELEASE

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DWG

NO.

BAC 924 C-RS

PER

AIRP.

USED ON

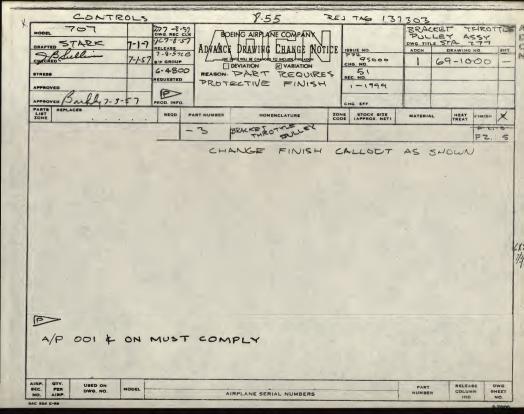
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CHANGE TAB BLOCK TO READ AS SHOWN			
	- 1	18	£ 6
	LEASE	01	OWG

AIRPLANE SERIAL NUMBERS

AIRP.



CONTROLS			5-70 17	COOP	D. SHT.	- OIX	04	
MODEL 707 DRAFTED W. SCHOLLHORN 8-8-57	D7 6-26-5) DWG. REC. CLK. EXA 6/26/57 RELEASE 4-26-5720 AD	/ v / T L	AIRPLANE COMPANY	TICE	SSUE NO.	BRA NO 4 DWG. TIT	CKET IN	CONTR
CHECKED J. KASNACE 6.18.57	BIS GROUP	DIE DWG WILL	BE CHANGED TO INCLUDE THIS ADON	F	P.RR. 9500	DO 1	65 - 28	
STRES9 ,	G-30GO RE	DEVIAT	ION EVARIATION RE ROUTIN		HG. NO.	-	03-20	/0 -
ATTROVED Gregory 9/19/57	P	ROVIS		s	ec. no. 79			
1/1/1/1/1/ 1/ 1/20-1	P			1-	- 105 \$ COI -	-		
PARTS REPLACES			D. SHT CX10 - 10	4) c	HG. EFF. 1999		,	
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INCREASE GTY AS SHOWN V			BOLT- CLOSE TOL					
(NEW)		366	WASHER ANGLE-BRACKET	-				
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ZNCDE AS SHOWN TO			REL:	COL	. ON	VEXT	PEVISIO	77
PICTURE AS SHOWN			7			261 DIA		
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P REWORK EXISTING	PAPTS	* <	_				0.261 DIA,	
ASSY. INSTALLED	>	-		4	-63-	360 A	AS 464-F	8
* ADCH REE				*C!	5	i	Z PLACES)	
AIRP. QTY. USED ON						ů		
NO. AIRP. DWG. NO. MODEL	-	AIRPLAN	E SERIAL NUMBERS			PART NUMBER	COLUMN	SHEET
BAC 924 C-RS 6490 6-20-7							IND	NO.

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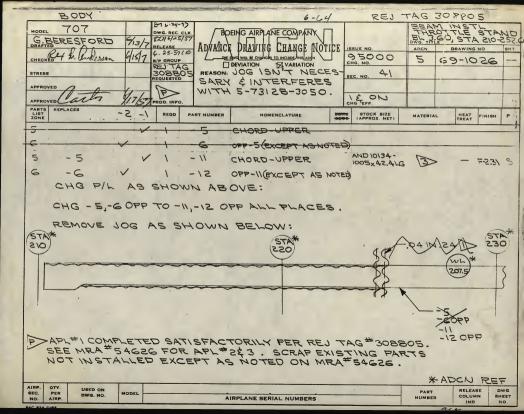
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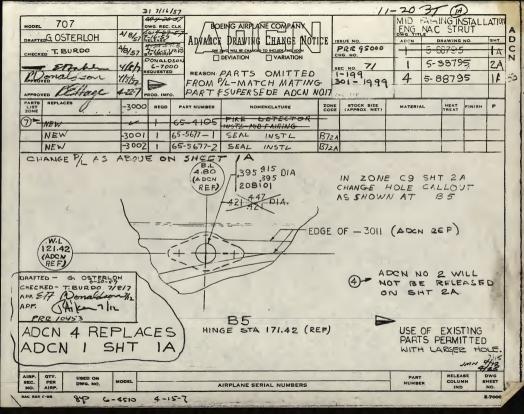
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CHECKED AMOLL 622	-17-9-76 MINION PINES	IG. NO. 95000		9160	-
Strange /27	WATANABE REASON SUPPORT NEEDED	с. NO. 24		-	+
APPROVED ////	PROD. INFO (REF. COORD SHT CX-10-40) CH	G EFF. 1-1999			
PARTS REPLACES	- REOD PART NUMBER NOMENCLATURE ZONE	STOCK SIZE (APPROX. NET)	MATERIAL	HEAT FINISH	P
	1 333945-1 SUMORT ANGLE	-			
EW 3-93945-1	VI GO-2590-1 SUPPORT ANGLE				
JEW 3-93945-2-1	1 60-2590-Z OPP 60-2590-1				
CHANGE P/L AS	TANGLE 3-93945 - 1 \$-2 OPP WITH SUF	PPORT ANGI	LE 60-2	:590-1 <u>&</u> -2	OF:-
IN REAR VIEW CHAN -20P PICT TO GO-25	T ANGLE 3-93945-1 \$-2 OPP WITH SUF	PPORT ANGI		590-14-2 3-61206 50-2590 - - 2 OPP.	(REF)
IN REAR VIEW CHAN-20PP PICT TO GO-755 PICTURE AS SHOW!	TANGLE 3-93945-14-2 OPP WITH SUE WE LH SIDE WE \$ 3-93945-1 URE & CALLOUT DO-1, -2 OPP CALLOUT STING: ASSEMBLIES CRAP EXISTING 3-93945-14-2 STALLED ON 707 AIRPS	PPORT ANGI	90-91	* 3-61206 50-2590 -	(REF)

BORN CONTROL STATE CONTROL STATE CONTROL STATE OF STATE O	CONTROLS	5-70 IT C	OORD. SHT. C	X10 -11	04	
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STREED SOUTH OF PROVISION BEC. NO. 79 SEC. NO. 104 SEC. NO. 79 SEC. NO. 109 SEC. NO. 79 SEC. NO. 79 SEC. NO. 109 SEC. NO. 79 SEC. NO. 109 SEC. NO	CHECKED JAMSHACE 618-5 / BIO GROUP	DEVIATION VARIATION		1	65 - 2870	0 -
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ANGED TO PL AS SHOWN ABOVE: ALSO ADD CHECK OFF TO EXISTING PARTS IN ZNCB & AS ADD TO PICTURE AS SHOWN ANGED COL. ON NEXT REVISION 250.250 DIA: HOLE NAS 464-PA-A9 (SPLACES) (SPLACES) (SPLACES) (USE 4 WASHELS IN SPOTFACE ** ASS. INSTALLED ** ANGED PARTS & ASS. INSTALLED ** AND REE AND REE AND REE ARR. DWG NO DWG. NO MODEL AIRPLANE SERIAL NUMBERS PART RELEASE DWG AIRPLANE SERIAL NUMBERS			-		P	
PICTURE AS SHOWN 250.260 DIA. HOLE NAS 464-P4-A (SPLACES) (SPL		BOVE N SO ADD CHECK	SEE TO FUE			
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SEC. PER DWG. NO. AIRP. USED ON DWG. NO. MODEL AIRPLANE SERIAL NUMBERS DWG COLUMN SHEET				0.5	PLACES)	SHOWN
NO. AIRP. AIRPLANE SERIAL NUMBERS NUMBER COLUMN SHEET						
BAC 928 C-RS (2017) (IND NO.)	SEC. PER DWG NO MODEL			PART	RELEASE	DWG

ADUZ

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	MODEL	70	, ,	,	PYL7/12	CLK. BOI	EING AIRPLANE COMPANY			ASSEM!	BLY OF	
a)	R. MA	TTE	20H 30	72957	RELEASE	ADVINCE			ISSUE NO.	The second secon	DHAWING NO.	SHT
עב			DOTON!	5/2/2	7.15.57	THE	WE WILL BE CHANGED TO INCLUDE THIS ADON		TEM 7142	R-6 50	-8281	1
	CHECKE	0/47	ELAV.	5/3/	ROHR	I CODE E	DEVIATION A VARIATION AFT SKINS SPLIT	T_	71			
	STRESS	11/2	OreFalia	128/57	4-130	5 LOKE &	MAINTAIN	10	I THRU 199			
	APPROV	FD	Charling.	1/20/57	1		ACTURING TOLERAL	CESL	301 THRU 193		*	
		1	1.12.	1		(M	FG. FACILITY)		CHG. EFF.			
	PARTS	REPLAC	tadigenes.	1/29	PROD. INFO	p	1	ZONI	1	MATERIAL	HEAT FINIS	нР
	LIST	REPLAC	5	0-8281	REQD	PART NUMBER	NOMENCLATURE	COD	STOCK SIZE	MATERIAL	TREAT	
						-22	DOUBLER-SKIN STAIL	.20 C6 2	1.040×1.60×43	2	2.115	5 R
	1-23			V	- 1	-55	DOUBLER-DOOR DIP STICE		.040 x 10.5 x15.0	2	2.115	3 13
	1.56					-66	FILLER FRAME STA 117.50	C5-6	2 - GIBKT-60X90.00	3	SRF	
	1-67					-65	FILLER FUD FRAME	B7-2	01 ta 2.10 x 34.00		9 RF	
	NEW	-22		V	1	-806	DOUBLER-SKIN STA III.20	A4-3	3 .040×1.60×41.20	2>	- SRF	
	NEW	-22		V	- 1	-807	DOUBLER-SKIN FLANGE	A4-	8.1 x00x1.60x1.8	3	- 58.5	
	NEM	-6E		V	1	- 808	FILLER-FWD FRAME		3.016×2.10×29.6		- SRE	
	NEW	-65		V	2	-809	FILLER-FWD FRAME FLAN	SE All-3	.016×2.10×2.20		- SRF	
	NEW	-66		V	1	-810	FILLER-FRAME STA 117.50		3 -016× 160× 35,20		- 5CE	
	NEW	-66		V	2	-811	FILLER-FRAME FLANGE	A2-3		3	- 12.2	
	NEU	-55		V	- 1	- 812	DOUBLER-DOOR DIP STICK		3 .040×10.5×14.20	2>	- SRF 2.11	
		- 55		V	1	- SPACE	DOUBLER-FLANGE	A4-	3 .040x10.5x2,0	2	- 585	is R
0.				CAT	SHOL	JAAT CANCID 8	Y BAC ADON 707			APLETE WIT	HOUTE	
500						707 STR.	Eskelle 6-257		CH SHT	DWG.		
10						CHECKED	Sakule Gaston	RI-TRI-		50-8281		
	* AD	CN.F	REF			CHECKED	260	Ri-		50-8281		
11						RAWROV: D	365araa 6/28/7	Rr2, Rr	·,··· -	4-5177		
Ų,			JORK EXIST			\$ ASSY'S	MOT METALLED	R1-4	2A	4-5181		
	KC-	-135	NOT AF	FECT	ED			R1-12	100	5-85655		
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				-							RELEASE	DWO
	AIRP.	QTY.	USED ON DWG, NO.	MODEL						PART NUMBER	COLUMN	L
-9	NO.	AIRP.	DWG. NO.		-		AIRPLANE SERIAL NUMBER	5			UND	1
-												

					0-10-2	NOI	PROCE	.00
	DRAFTED J.W. BESTO CHECKED DATEM STRESS MARGINETE	5/17/57 B/F GROUP 5/17/57 ROHP 4-1346 R	DVANCE DRAWING		17EM 7142 CHG. NO. 71 SEC. NO. 71	DWG. TITI ADCN	ARD FAIL ACELLE LE ASSEMI DRAWING 50 82 50-82	BLY OF NO. SH'
	APPROVED wifned	5/8/7 X 5/8/57 PROD. INFO.	(MFG	FACILITY)	301 THRU 199	9		
	PARTS REPLACES	50-8281 REOD PART	NUMBER NO	MENCLATURE	ZONE STOCK SIZE	MATERIA	L HEAT	FINISH P
•	1-6 1-8 1-28 1-29 1-30 *(ADD)	V	7 CHORD-12 7 WEB-FRAM 8 CHORD-UPR 9 CHORD-10M 1-7 PH BMS	OWER FWD FRAME I DESTA 117.50 (ER FRAME STA 117.50 (ER-FRAME STA 117.50 (T-12B SO 0,000 PSI	C5-2 055 190 C5-2 055 190 B5-2 055 190 FT TEMP	ORMI	NG.	\$2.207 R 12.207 R 12.207 R 12.207 R 12.207 R
581-509	BIC RELEASED FARROLD SY BIO APC. (707 27E. EPACE CMESKED BLANDS CHECKED BLANDS CHECKED BLANDS APPROV. D. A. F. Faro	27/1/7 RE				PLETE	WITHOU	- 7
	* ADON PEE ONL							

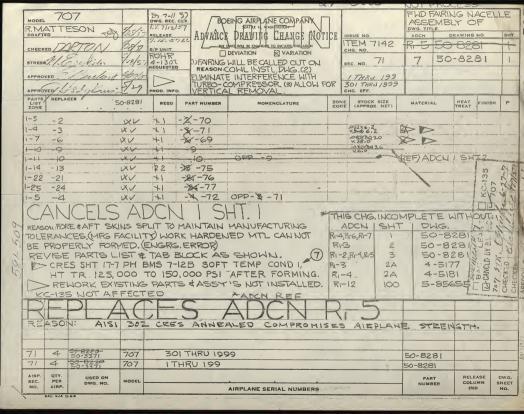
EXISTING PARTS & ASSYS MAY BE USED WITHOUT REWORK.

KC-135 NOT AFFECTED

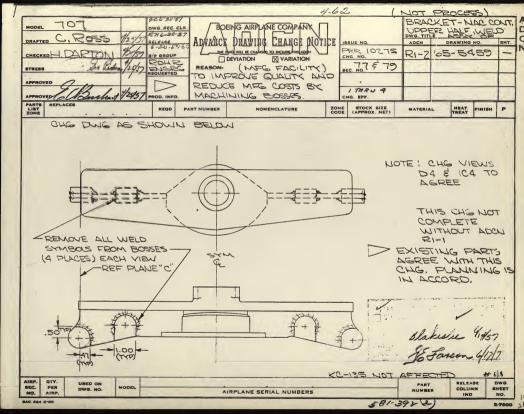
REF. BACTWY 6-4975, 3-1250-GIH DTD. 5-10-57

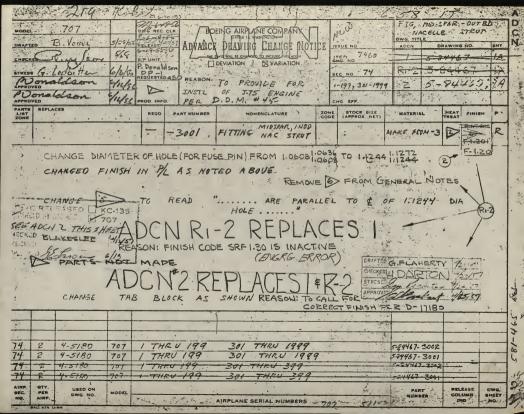
					49	7/3/7
AIRP. QTY. SEC. PER NO. AIRP.	USED ON DWG. NO.	MODEL	AIRPLANE SERIAL NUMBERS	PART NUMBER	RELEASE COLUMN IND	SHI

BAC 884 C-81

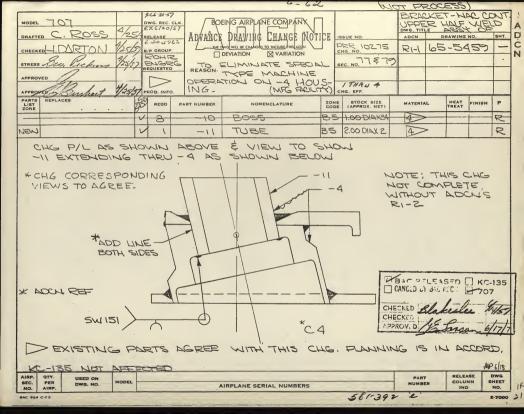


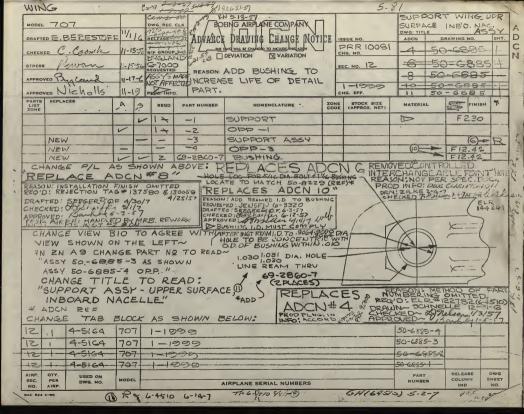
A					JPI	100re		,	5-63 2	TNOT F	ROCE	555	
B	MODEL R. DRAFT	MATTESON	5/1/57	27 7-11- DWG. REC. RX 7/12 RELEASE	CVK. BOULANCE	EING AIRPLANE COM	PANK T			FWD. FA ASSEM DWG. TITLE	IRING I	VACEI	LE
	CHECK	EDH METON P	5/7/59	7-15-57		DWG WILL BE CHANGED TO INCLUDE TO			ITEM 7142	ADCN	DRAWING		SHT.
		1.15	5/1	ROH F	5 0	DEVIATION VARIA	ATION	-	CHG. NO.	R1-4 =	8-03	281	
	STRESS	7.1. Que 16.6.	97/57	4-130		ORE EAFT SKIN			SEC. NO. 71				
	APPRO	VEO Buchard	5/2/57	1	10 WAIN	ITAIN MANUFAC	TURIN	G	1 THRU 19				
	APPRO	VED Blotak	6/6/2	PROD. INFO		ANCES. PG. FACILITY)		1.	301 THRU 19.				-
	PARTS LIST	REPLACES	- the second second	T				-	HG. EFF.			1	-
	ZONE	L	50-828	REQD	PART NUMBER	NOMENCLATURE	E	CODE	STOCK SIZE	MATERIAL	HEAT	FINISH	P
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												SRF 12,207	
	-52_	,	V		-51	SKIN-AFT		C52	×50.00	3>		12.207	R
Ì	NEW	-48	· ·		-800			A63	.032×11,00				
				1 .	-800	SKIN-FWD		3	x 45,00		T4	SRF 2.130 S.E.507	R
	NEW.	-48	· /	1	-801	SKIN-FHD FLA	IVE	A6	.032×5.00	F		SRE	
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- [1EM	-51	~	1	-805	SKIN-AFT	ŕ	2	025X 21.00 × 50.00	3>	_	SRF 12.207	R
,	VEW	-51					-	AQ -	.025x 5.00				
ľ	10074				-803	SKIN-AFT FLAN	VGE .	2	× 50,00	3>	-	SRF 12,207	R
1	1EM		V	1	804	OPP - 803		192					
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2.	-57			1	-56	SHIM- STA III	20 0	52	PIEXILIOX43 D	3		12,207	
	EW.	-56	·V	1	-814	SHIM - STA III, 2		52	.016×1,10×40.0	3>	11 12 13	205	-
1	IEK	-56	V	2	-815	SHIM - FLANGE ST	A111.20		-016x 1.10 x 2.0	3>	1 - 1		R
1.	KE/	ISE PARTS LI	ST AS	SHOW	N ABOVE :					1 1		-407	- /- 1
1	* AL	XN REF.		D.	BAC RELEAS	ED [KC-135+	THIS	CH	G. INCOM	PLETE WI	THOUT	707	
					ANCLD BY BAC A	DCN 707	ADC		SHT	DWG.			
1	>	REWORK EXIS	STAGE	707	STR BA	reefec 6-25-7	R1-5, R1-6	-		50-8281			
1-	IN	STALLED.			CKED Blake		RI-3	100	3	50-8281			
				2	OV D SEE	0 199	R-2, R-4	1 KI-2	2A .	50-8281			-
-		C-135 NOT A	FFEC	ED	165	aroon Gra	R1-3 R1-12		12A	4-5177			
	BEC.		MODEL							PART	RELEAS		
-	-	AIRP.			All	RPLANE SERIAL NUME	BERS			NUMBER	COLUM	N SHE	
					1. 3	581-509			4			2-70	000

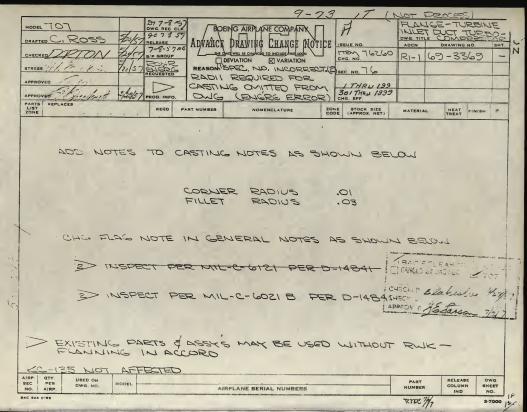


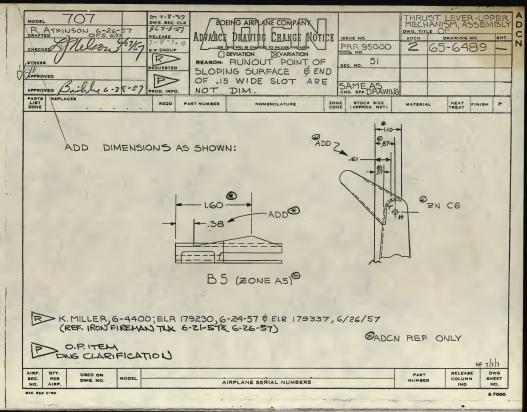


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	170				DWG. REC	CLK. B	DEING AIRPLANE COMPANY	П	Now-	INSOA	NO-S	LATIC	CAC	Plic
DRAFT	TED CO.	<u> Woo</u>	DS	/ .	RELEASE	ADVANC	E DRAWING CHANGE MC	TICE	ISSUE NO.	ADCN		AWING N		SHT.
CHECI	KED J. T	ujiok	a 13	12/50	KIP GROL	P - 10 - 10	E DWG WILL BE CHANGED TO INCLUDE THIS ADON		DI	- 8		175		
STRES	- 100	4 Jan		7-15	SOON	LD301-5	DEVIATION VARIATION	-	CHG. NO.	- 0	-			12
79	-	dia	/ 7 -	-	EQUEST	D REASON	TO PROVIDE FOR PLUMBING RUNS A		SEC. NO. 7Z	16	4-5	5175		IA
PRO	VED	recommenda	12	1/13		PEOV	EN BY MOCKUPED	LEC						
-PPRC	OVED				ROD. IN	INSTL		-	SOI THEU 199					
ARTS	REPLAC	ES		4-5175	BEOD	PART NUMBER	No.							-
ONE				-3,000	REGD	PART NUMBER	NOMENCLATURE	CODI	STOCK SIZE (APPROX. NET)	MATERIA	- T	REAT F	INISH	P
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2	NEW		16-	14	X2	-3004	BACKING PLATE	DZ 3A	.040x 2,60 DIA				INS	RF
P	NEW			V	١	-3006	BACKING PLATE	CZ SA	.040x 2.10x4:10				.115	RF
2	-300)Z		世	XI	-3008 -3002	WES							
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			TEMS) KE	PEA	TED FRO	M APCHZ TO OF -3005	CHO	5. EFF. 1-1	99 € 30	1 - 19	aa		H-18
			2.0	` `		- 1010	- 5005		RGE NO.		. ,	.03		··
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									PROVED:					_
										PE	Hase	6-13.	-7	
								PRO	DD. INFO	REWO	BK	EXIS	STIM	VG
AIRP. SEC.	QTY. PER	USED ON	MODE							PART		RELEASE	D	owg
	AIRP.	DWG. NO.				A	IRPLANE SERIAL NUMBERS			NUMBER		OLUMN	SH	HEET NO.
BAC 924 (C-RS							400		THE FLOOR	15.0	1110	, ,	لستتر





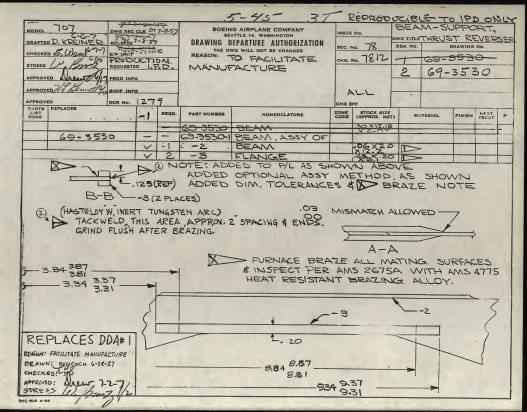


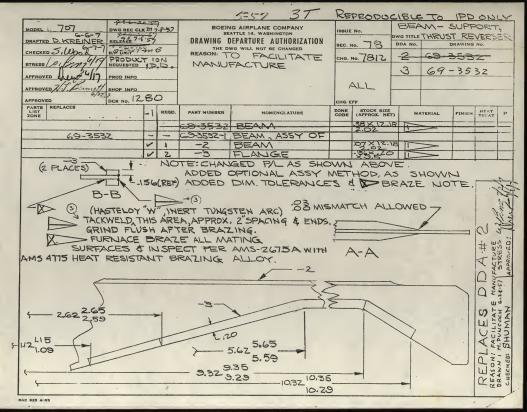


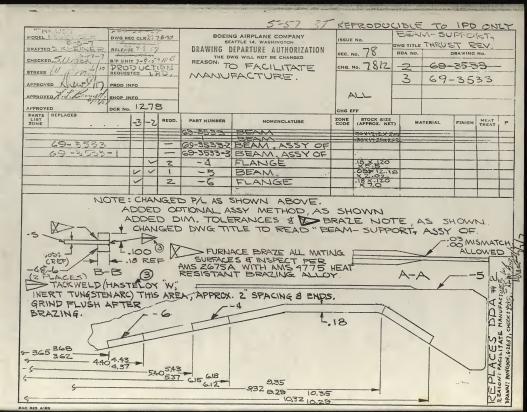
1 1 1 2 - 1						-		2-5	54	1
MODEL 707 DRAFTED R. HARDING CHECKED D. COrley 7-3-57 STRESS APPROVED PLEASEN APPROVED	77-8-7 DWG. REC. CLK 927-8-57 RELEASE 2-7-7-10- 8-19-GROUP 4-4400 REQUESTED	ADVANCE	ENG AIRPANE COMPANY DRAVING CHANGE NOTICE TO SEVARATION TO USE MATTERIAL ABLE.	L SI	SUE NO. TEM! 7822 EC. NO.		DR	UST SIAWING		
PARTS HEPLACES	REQD P	ART NUMBER		ONE	STOCK SIZE (APPROX. NET)	MATERIA	L	HEAT	FINISH	P
		-1	HOUSING		1:20X2:20 X 2:20				F-8:05	T
		-1	HOUSING		1.20X2.20X2.20		-	-	F-8.05	T
	CRES BA COMP FI OPTIONA	M, CON	ES AS BELOW S1303, PER MIL-	S-		5-67	121			

AIRP, QTY.
SEC. PER DWG, NO.
AIRPLANE SERIAL NUMBERS

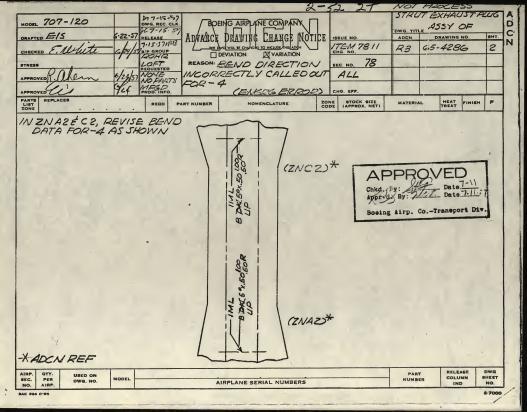
PART NUMBER COLUMN SHEET NO.
AIRPLANE SERIAL NUMBERS

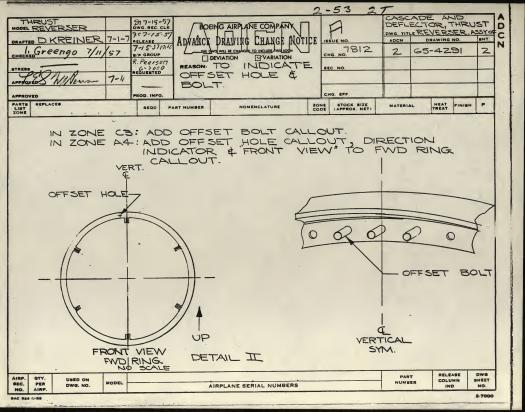




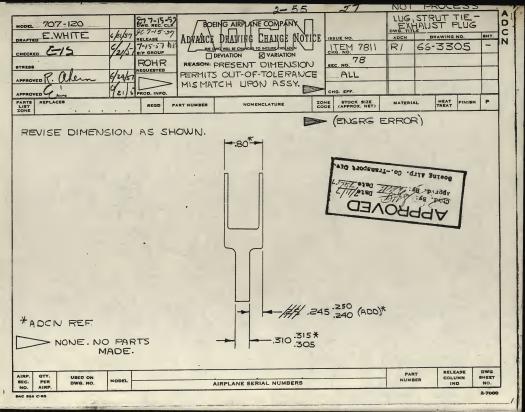


MODEL 707-120	27 7-15-57 DWG. REC. CLK.	BOEING AIRPLANE COMPANY		CLAMSE	HELL INSTL DEVERSER	?
F-15 720	57907-15-57	THE PROPERTY OF MOTHER	I ISSUE NO.	ADCN	DRAWING NO.	SHT.
C111/1-h	1 7-15-57 MB A	DVANCE DRAWING CHANGE NOTIL	17EM 78/5		5-4253	-
STRESS	ROHR R	DEVIATION AVARIATION REASON: WELD CONTINUITY	70			11
APPROVED R. alen 6/34		MITTED É DIM. INCORDEC. GLLED OUT	ALL -			\perp
APPROVED ()		(ENGRS ERRO			Test	+
PARTS REPLACES LIST ZONE	REQD PART	NUMBER NOMENCLATURE	ZONE STOCK SIZE (APPROX. NET)	MATERIAL	TREAT FINISH	P
Boeing Airp. CoT	Date 7-11-7	Annunal V V V V V V		WEDLS *		
AIRP. GTY. USED ON MODISEC. PER DWG. NO. MODI	EL .	AIRPLANE SERIAL NUMBERS		PART	RELEASE COLUMN IND	DWG SHEET ND.
NO. AIRP.						2.7000

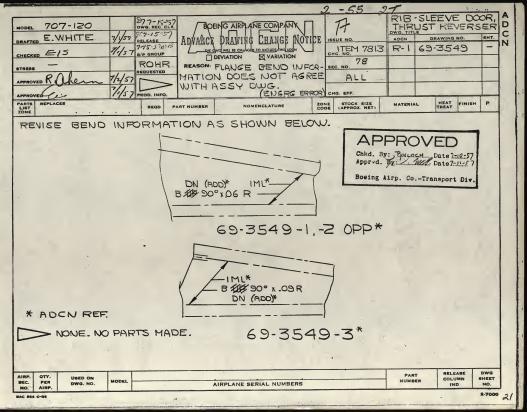


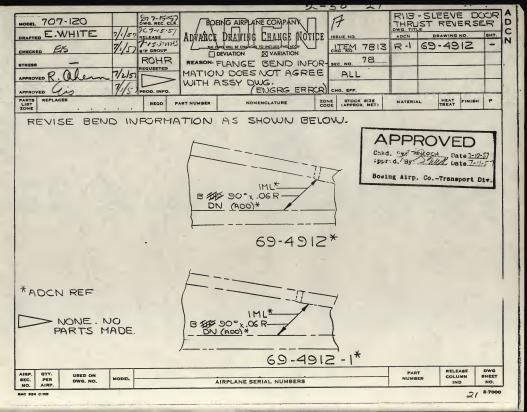


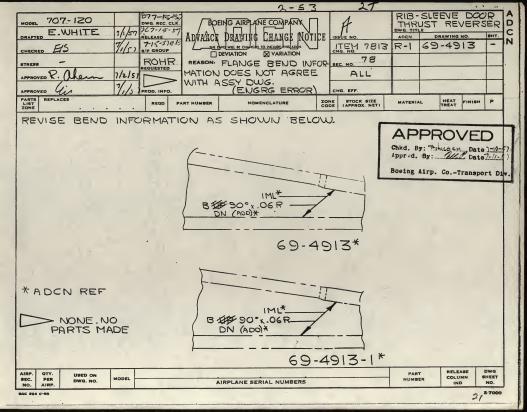
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		ERSER		90 7-15-	别 / 飞	EING AIRPLA			_				E REV	EKSER	SHT.	N
DRAFTED	DK	REINER	7-1-7	RELEASE	∠ A DAVANICI	DRAWING	CHANGE	NOTI	CE LISS	TEM 7	213	ADCN				
1. Gr	een	90 1/11/57		7-15-5717 B/P UNIT			TO INCLUDE THIS			IG. NO.			65-	6561	1,1	
CHECKED	2			R. Pearso	n	DEVIATION	VARIATI	ON		c. NO						
STRESS	10	1		C-7000 REQUESTED	REASON:	USED	ON D	WG	SE.	C. NO.						
APPROVED	31	Mallen	7-11						-							
		- //-		PROD. INFO.	NO.	INCORF	ECI		CH	IG. EFF.					-	
PARTS R	EPLACI	is .		T	PART NUMBER	NO	MENCLATURE	T	ZONE	STOCK SI	ZE	MATERIA	L H	EAT FINISH	P	
LIST				REQD	PART NUMBER		ENCERTORE		CODE	(APPROX. P	(EI)					
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SEC.	PER	USED ON DWG. NO.	MODEL			AIRPI ANE	SERIAL NU	MBERS				ן אט	MOER .	IND	NO.	
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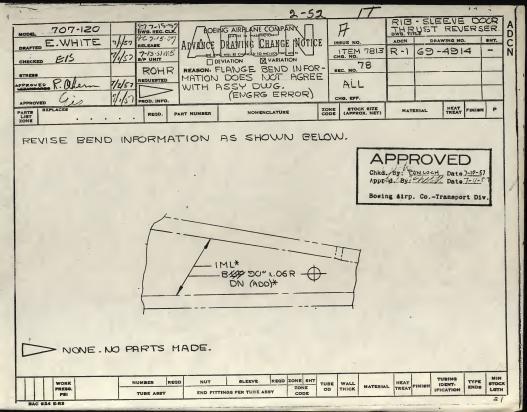


4.4	2-55 37	NOI MA		-
MODEL 707	DI 7-15-52) DWG, REC. CLK BOEING AIRPLANE COMPANY BOEING AIRPLANE COMPANY	DOOR S	TLEEVE	A D C
DRAFTED EIS 6-17-57	A DELACE DELEVING CHANGE MOTICE ISSUE NO.	ADCN D	RAWING NO.	SHT. N
CHECKED E. Whate chiefs	B/F GROUP STARTION STARTION CHG. NO.	RI 66	3-3307	
STRESS RI/ Ocabina 6-19-5)	TOOLING REASON: TO PROVIDE OPTIONAL SEC. NO.			-
APPROVED	NONE - METHOD OF FABRICATION 1-199			<u> </u>
APPROVED X, Civil 6/18/2	MFGD. (MFGFACILITY) CHG. EFF.			
PARTS REPLACES LIST ZONE	REQD PART NUMBER NOMENCLATURE ZONE CODE (APPROX. NET)	MATERIAL	TREAT FINISH	Р
*ADCN REF.	Chkd. E	PPROV By THE By HAL Airp. CoTre	Date 7-10-57 Date 7-11-57 Ansport Div.	
AIRP. QTY. USED ON SEC. PER DWG, NO. MODEL -	AIRPLANE SERIAL NUMBERS	PART	RELEASE COLUMN IND	BHEET NO.
BAG 924 C-R5				









1.53 2T REPRODUCIBLE	TO IF	3 as	12051	2
MODEL 707 DWG. REC CLK BOEING AIRPLANE COMPANY ORAFIED S. WOOD RELEASE ADVANCE DRAVING CHANGE NOTICE ISSUE NO.		DE & DER	SER	BHT
CHECKED S. H. FELD (10) 6.01.57(8) IN GROUP DEVIATION VARIATION CHG. NO.	Z	65-4	291	
STRESS (D. 1907) BENNETT REASON: TO CLARIFY DWG SEC NO. 78				
APPROVED Z. J. Bernett 4/7/5 PROD. INFO. CHG EFF. ALL				
PARTS LIST LIST NOMENCLATURE ZONE STOCK SIZE (APPROX. NET)	MATERIA	AL HEAT	FINISH	P
FURNACE BRAZE (3) (4) EXTERIOR INSPECTION SHACE (b) WITH BRAZING ALLOY APPLIED TO ADD UNDER SCORED OF THE JOINT BEFORE BRAZING, INSPECTION SHALL SHOW A COMPE BRAZE ALLOY ON BOTH SIDES OF (C) IN THE EVENT SUBSEQUENT BRAZING TO MEET REQUIRE MENTS OF (b) BRAZING IS ALLOWED; AND X-F SHALL BE EMPLOYED TO ESTABLE WITH (3)	EXTE TE LITE COMP	RIOR NE OF PLETET REG. SIDE NSPEC	D TION NCE	NT.
AIRP. GTY. USED OH MODEL AIRPLANE SERIAL NUI JERS	PAR	ER CO	EASE LUMN ND	DWG SHEET NO.

THRUST R	EVE				3-1	19 6T N	JOT P	KOCES	S	
MODEL TOT KRISTOFFERSON DRAFTED STREED STREED ADMINISTREED ADMINISTREED APPROVED A J. Lemeth	9/10/7	BIP GROUP ENNE G-700 REQUESTED	ADVANCE	DEING AIRPANE COMPANY E DRAWING CHANGE NO AND WILL WINDOWS DESIGNATION DEVIATION SYMMETRY TO COMPLY WITH	TICE IS	ISUE NO. EM 1854 MISS NO. EC. NO.	DWG. TITLE	AUST P	TION NO. SHT.	ADO BOOK OF STANKE
PARTS REPLACES LIST ZONE	. 10	AN REGO	PART NUMBER	NOMENCLATURE	ZONE	STOCK BIZE	MATERIAL	HEAT	FINISH .P	12
	,	, 4	BAC 830 8G -5-10A	BOLT						किर ह
		1 2	BAC 63086 -4-86 BAC 63086 -4C-2A	BOLI						ODOC
	:	SHT I	- BAC	E P/L AS SHOP E BOLT CALLO BBOBG-SHOP 330 BG-BC-100	27 UC	ABOVE, I S AS SH BAC 830 B	OWN	· · · · ·	4	ERP E
		SHT ?	Z: IN ZO	one's BB, BG; but as show	DS.	CHANG	e Bo	PLT		
				AC 830 BG - 40						-
AIRP. QTY. USED ON								RELEAS	F DWG	

AIRPLANE SERIAL NUMBERS

NO. AIRP. BAC 924 C-RS

MODEL

DWG. NO.

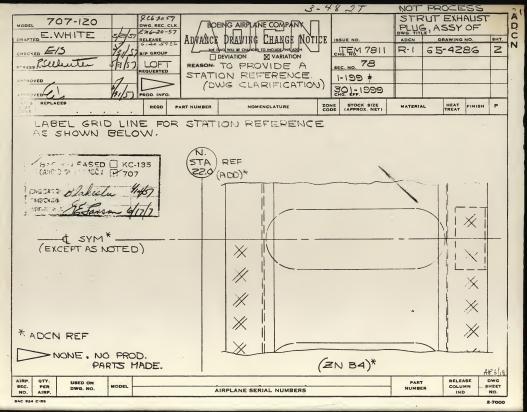
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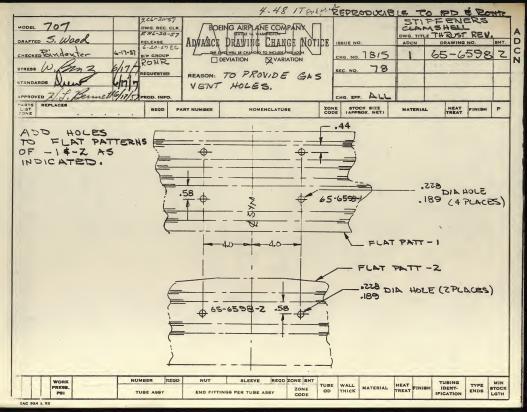
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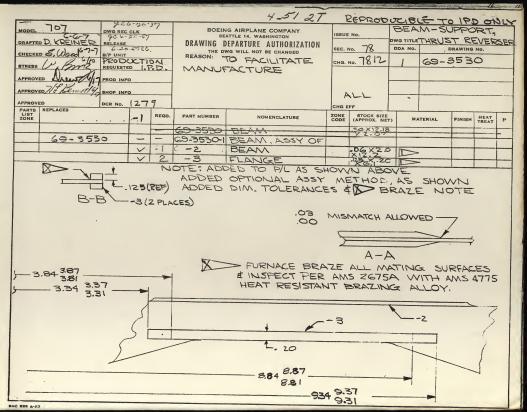
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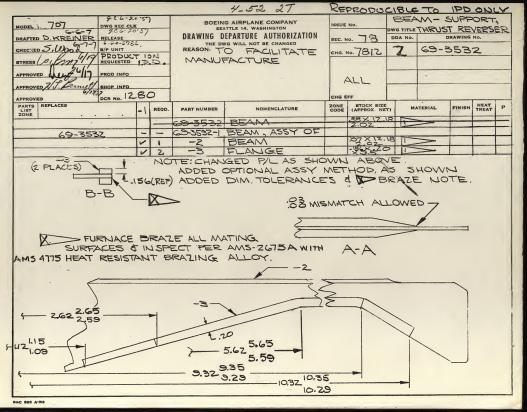
PART

NUMBER



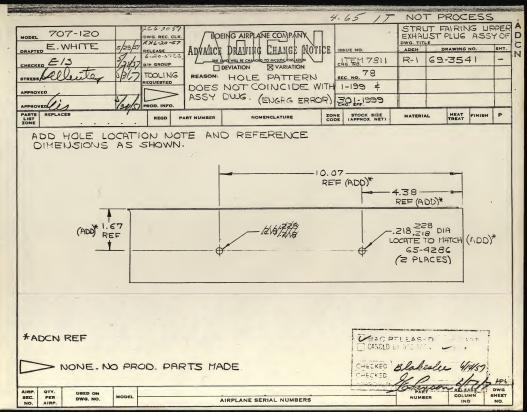


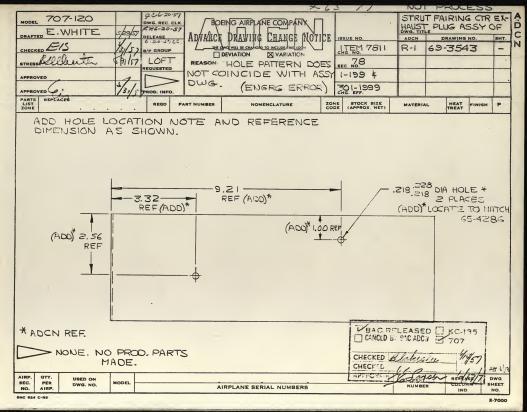


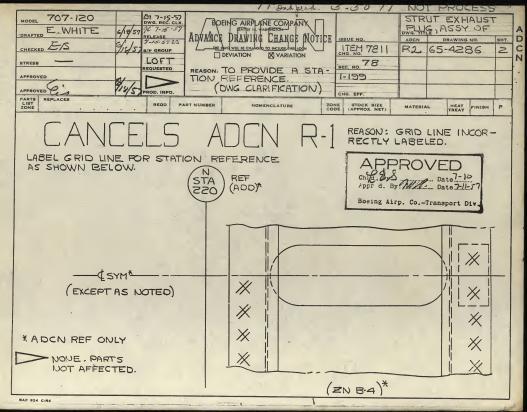


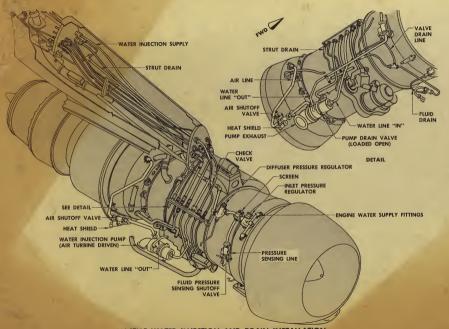
						4-52 2T	ベモド	RODU	TIBLE	70	IND	ON	-
THRUST	206-	20	-57			G AIRPLANE COMPANY			BEN	W- 5U	PPOP	272	
MODEL REVERSER	DWG REG	CLK				TTLE 14, WASHINGTON	ISSUE			THRUS			
DRAFTED D. KREINER	RELEASE		7-5*		DRAWING D	EPARTURE AUTHORIZATION		. 78	DDA No.		RAWING		
1	6.20	-578	٥.		THE DV	VG WILL NOT BE CHANGED							
CHECKED S. WOOL	B/P UNIT		a T.	15.51	REASON: TO	D FACILITATE	CHG. N	10.7812	2	69-	353	3	
STRESS W. Comto	PROT	ED	LP	D	NUMAN	FACTURE.							
APPROVED KILLY 17	PROD IN	FO					1						
192 1	1						A	1					
APPROVED A . De could	SHOP IN												
APPROVED	DCR No.	12	-12	3			CHG E	FF		<u></u>			
PARTS REPLACES LIST ZONE		-3	-2	REQD.	PART NUMBER	NOMENCLATURE	ZONE	STOCK SIZE (APPROX. NE	т) м.	TERIAL	FINISH	HEAT TREAT	P
		_			69-3533	BEAM		30×12.2×					
						BEAM		304\7.28XZ			+	-	-
69-3533						BEAM, ASSY OF							
69-3533	-1			_		BEAM, ASSY OF		10 7 150	-		-		-
			4	2	-4	FLANGE		18 x 750			-		
		V	~	1	-5	BEAM		×2.02	8				
		\neg		2	-6	FLANGE		18 X.120					
				7		-			-				
-5 SA	* *	DE D	DEL	GED GED	TIONAL ADIM. TOLE	SHOWN ABOVE. SSY METHOD, AS ERANCES & B TLE TO READ "B ACE BRAYE ALL MATI	RAZ EAM NG	E NO	TE,	ASSY	SS WI		ich D
(ZPLACES) B	-B	18	RE	6	SURFACE AMS 26757 RESISTAN	ES & INSPECT PER A WITH AMS 4775 UT BRAZING ALLO	HEAT	7	A	A		5	

BAC 925 A-93







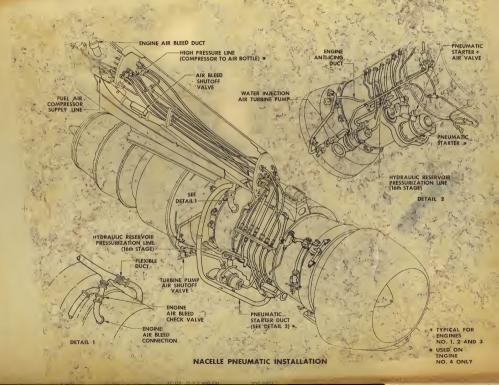


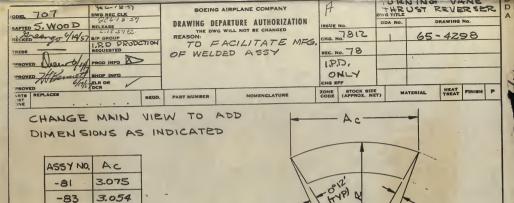
NACELLE WATER INJECTION AND DRAIN INSTALLATION

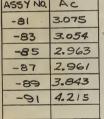
KC- 35 55-3121 AND ON 5P41 SHT 2

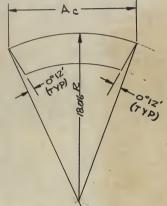
FRAME NO. 8

BLACK PLATE OF 2









FOR USE ON 65-4291-3 ASSY ONLY

MODEL 707	DWG. REC. CLK.		EING AIRPLANE COMPANY		A	TUR TAR		IERS	
CHECKED J. Stranger 9/14/	RELEASE 7 6-18-1762. 7 B/P GROUP ROHR	ADVINACE	DRATITIC CHANGE MOTIC WILL BE CHANGE TO INCLUDE THIS ADD DEVIATION SVARIATION	c	7812 HG. NO.	ADCN	65-42°		SHT.
STANDARDS THIS INTERCED	REQUESTED		TO CORRECT	-	I ASSYONY				
PARTS REPLACES	PROD. INFO.	ART NUMBER		ZONE	STOCK SIZE (APPROX. NET)	MATERIA	HEAT TREAT	FINISH	P

CHANGE DIMS. INDICATED BELOW IN ZN A4

ASSY NO	DIM"A"E.O	DIM "B"	DIM'X'	DIM"Y"
-81	3,070	3.128	.030	.035
-83	3.050	3.128	,035	,050
-85	2.957	3.128	1050	.1250
-87	2.950	3.128	.IZ50	.054
-89	3.820	3.905	.064	.025
-91	4.177	4.231	.054	.000

NO PARTS MADE - PART NUMBERS NOT CHANGED

l																		
t	T	Г	I	WORK	NUMBER	REQD	NUT	SLEEVE	REQD	ZONE SHT	TUBE	WALL		HEAT		TUBING	TYPE	MIN
ı				PRESS.	TUBE ASS	Y	END FITTIN	GS PER TUBE AS	SY	ZONE	OD	THICK	MATERIAL	TREAT	FINISH	IDENT-	ENDS	LGTH

8-68 /T REPRODUCIBLE TO IPD. & ROHR

	hl + 7-15	-57	-						****		
MODEL 707	DWG REC CLK	- /		BOEING ALL	RPLANE COMPANY				ASSEMI	364	***********
DRAFTED P. WEED 1/57			DI		TURE AUTHORIZATION	MCR-No.		DIK	ECTIONAL	- VA	LVE
DRAFTED VILLATED JOJ				TUILING DELVI	HOLLWANDING WILLIAM					KEVE	SEIC
CHECKED 27 17/1/2	7-15-57 LB			THE DWG W	LL NOT BE CHANGED	SEC No.		DDA NO.	DRAWIN	IG NO.	
CHECKEUS FEET 17				SON:		_	1837		69-3	507	
STRESS	REGUESTES ON	R.	1		HI-TEMP	TEM			2/3	201	
						17			2		
STANDARDS	PROD INFO			BEKKING	HOT						
P) 12 3/2 7-11			IVA	ALLARIE	AT THIS TIME.	-	_				
APPROVED PAR	SHOP INFO		7,70	WILL COCC	MI THIS TIME.						
						Mono					
RAPPROVED REPLACES	DCR No.	-				CHG EFF					
PARTS REPLACES	\$5	-				ZONE			79/2		1
ZONE · ·	/.	507	REQD.	PART NUMBER	NOMENCLATURE	CODE	STOCK (APP)		MATERIAL	HEAT	FINISH
			,		7						-
				RAPZMSSI	BEARING BALL		1415050	HU ROC	KNELL CORE		
		-			(BAC-BIOA -680) -	JAM=	STOWL	NY (OF BOW	(a)	
				RA3M5	BEARING BALL					2	
	(1/2	レー	1	X > 1		- 1	-AF	MIK !	BRG. Co.		
							HEM .	BRITA	W. COUP. (OE	טוטפב)
					,		-	-			
	-						HEM .	BRITA	W. Coup. (OE	עוטסב	
								-			



REMOVE NON-METALLIC SEALS & REPACK WITH SHELL 21176A SILICONE GREASE.

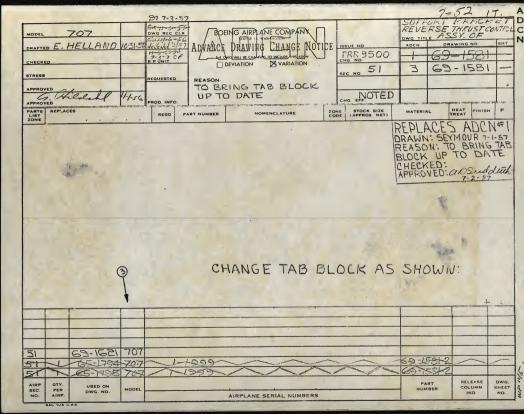
OPTIONAL: REPLACE NON METALLIC SEALS WITH TEFLON SEALS.

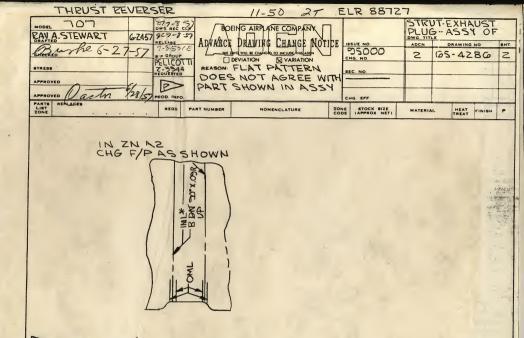


FIRST TWO UNITS MEGO BY ROHR.



FIRST FOUR LINITS MEG'D BY IPD

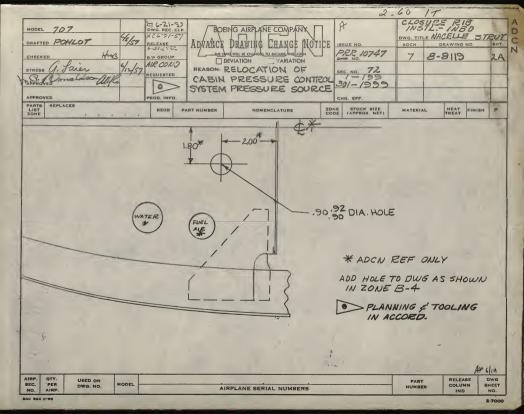


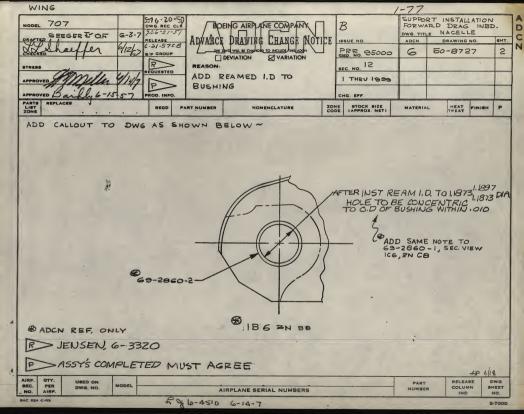


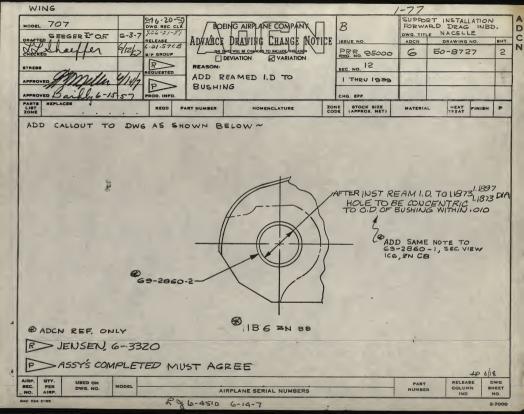
DETAIL PLNG & TOOKS -4 APPRECIED

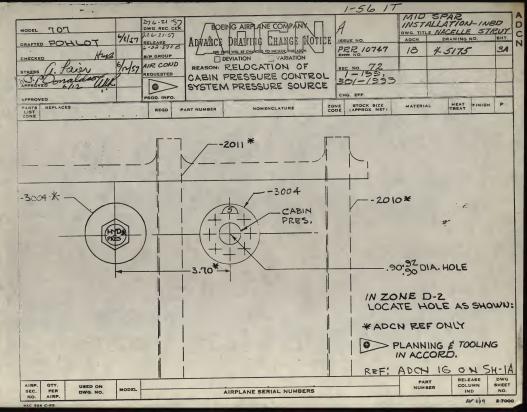
AIRP. OTY USED ON RELEASE DWG PART SEC. PER MODEL DWG. NO COLUMN SHEET AIRPLANE SERIAL NUMBERS NUMBER NO. AIRP NO.

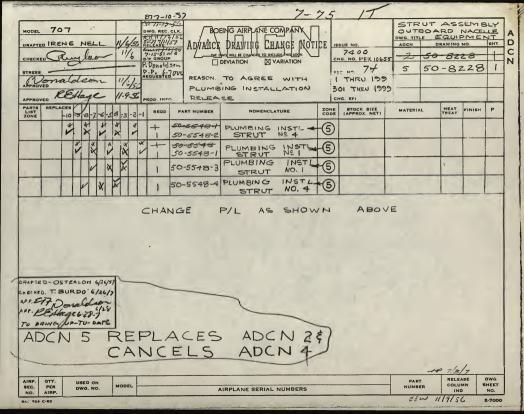
*ADCN REFONLY











		POWER	PLAN	T		-7-6	7	11	COORD 9		x 10-	93
MODEL		07		17-18- WG. REC 8W7-12	Zx Boi	EING AIRPLANE COMPANY	7		STIFFEN R.H.	STOE ST	RUT	
DRAFT	ED	2.DOWNING	012 3/ R	7-15.57	ADVANCE	DRAWING CHANGE NOT	ICE -	SUE NO.	ADCN	DRAWING !	10.	SHT.
CHECK	EDEAT	enburter	1/20.1-	P GROUP		WILL BE CHANGED TO INCLUDE THIS ADDIN		TEM 95000	2 5	-8344	7	HA
			1	G-306		DEVIATION VARIATION	[77	3 5	-884	47	IA
STRESS		7, ,	R	EQUESTED	01011	ROUNDING PROVIS		EC. NO.	1 -		• •	-
APPRO	VED	1///	11	P	SA KICAL G		_					\mathbf{H}
APPRO	VED /	All Vall	1417 .	ROD. INFO	o.		10	199 \$ 301-1995				
PARTS LIST ZONE	REPLA		-3006	REQD	PART NUMBER	NOMENCLATURE	ZONE	STOCK SIZE (APPROX. NET)	MATERIAL	HEAT TREAT	FINISH	P
1			V	11+	5-88447-2000	STIFFENER	C52A	8AC1517-497 X 81.70 LG		T6	SRF 2115	RF
	NEW	V			5-88447-3006		C5ZA					RF
	NEV	V	V	2	69-5363	BRACKET, ASSY OF	C4 2A					
	NEV	V	V	2	69-5363-1	BRACKET, ASSY OF	SZA					
	NEW	v 3	V	2	69-5363-2	BRACKET, ASSY OF	CBZ					
	NEW	1	V	1	12LHA1-02	(BUT-PIOLA-A3S)	C22A	ELASTIC ST	OP NUT COR	P. OF AM	FRICA	TO
CH	IANG	E DWG TI	TLE T	0 R	EAD AS F	FOLLOWS: "STIFFE INBD NA ASSY (OF F			OCN 1	2	
ADC	NN	ON 5	-88447 18 ON	SHT1 5-85	A 5 69-536	HTZA, ADCN 2 3 (NEW DWG), 18 ADCN 9 CAMPLETE LUB ON 5-8864-7547ZA	1	ADVANCE C REASON: TI BRACKET ELR 23 DRAFTED CHECKED: APPROVE	O ADD (1) ASSY TO 23, (CX GLENN R Rothand	69-53 DWG 10-136) 2. DOW	PER	2 2-7
CH	ANG	E TAB B				E	_	REWORK E & ASS'Y	XISTING	5 PAR	TS IN	
72	2.	5-85617	707			OI THRU 1999			5-83447-300			±ZA
72	2	5-85617	707		3	OITHR'1 1999			5 83447-20		IA	\$2A
72	2	5-85617	707		1	THRU 199			5-83447-300			124
72	2	5-85617	707		1	THRU 199			5-88447-20	20	IA	12A
AIRP. SEC. NO.	QTY. PER AIRP.	USED ON DWG. NO.	MODEL		À	IRPLANE SERIAL NUMBERS			PART NUMBER	RELEAS	N SH	WG EET NO.
BAC 924	C-RS	Desc.	1510 6-21	4-7 7	-Z-7						2	7000

THE THE PRODUCT OF TH	DRAFTED P.H. CORSER	7.0 5	D77-17 DWG. REC SX17/18/3	ST BO	EING AIRPLANE COMPANY		yew.	DWG, TIT	LE	ALLATI	
REASON: (ALLOUT SEC. NO. 76 I - 199	54 1	7/2/_	1-18-50		OWO WILL BE CHANGED TO INCLUDE THIS ADON	1 4	RR 95000	-	-		
APPROVED APPROVED APPROVED PROD. INFO. P	STRESS		-7000	REASON:	CALLOUT						
APPROVED PROD. INFO. CHO. SPEC. SOC. STOR. STO	APPROVED	7/10/57	EQUESTE	NEW	BOLT			1			
CHANGE CALLOUT IN REAR VIEW FROM G-83855 TO	APPROVED			э.		_ :	307-1999 CHG. EFF.			1	1
CHANGE CALLOUT IN REAR VIEW FROM G-P3855 TO	LIST	10650	REQD	PART NUMBER	NOMENCLATURE	CODE	STOCK SIZE	MATERI	AL	HEAT FINIS	P
CHANGE ALLOUT IN REAR VIEW FROM G-83855 TO						C7					
		CHANG	SE	AL AS	SHOWN ABOUE		2M G-P3	855	TC)	
		CHANG	SE	ALLOUT	SHOWN ABOUE IN REAR VIEW		ом 6-83	855	TC)	
		CHANG	SE	ALLOUT	SHOWN ABOUE IN REAR VIEW		pm 6-83	855	TC)	
		CHANG	SE	ALLOUT	SHOWN ABOUE IN REAR VIEW		ру 6-83	855	TC	,	
		CHANG	SE	ALLOUT	SHOWN ABOUE IN REAR VIEW		pm 6-83	855	TC)	

A 7/16/7 RELEASE DWG AIRP. QTY. PART USED ON DWG. NO. COLUMN SHEET MODEL SEC. PER AIRPLANE SERIAL NUMBERS NUMBER NO. NO. AIRP.

BAC-924 C-RS

S.R 64510 7/11/7

MODEL	WILLARD D	945	7. 7	RK 7/12 DWG. REC RN 7/12	eck. BO	EING AIRPLANE COMPANY	1	A _.	LOWE INBD			
DRAFTI	ED	- /		RELEASE	A DV ANC)	DRAWING CHANGE NOTI	ICE L	SSUE NO.	ADCN	DRAWING	NO.	SHT.
CHECK	a Fun as	1	19	m/m GROUI	. Lange	DEVIATION VARIATION		PRR-10826	12	3-310	0	12
STRESS	Ellafer	7	. ,	P. DONAL P.P. 6-7	000			EC. NO. 72				
APPROV	Donafoldon	3	14/57	REQUESTE	REASON:	TO PROVIDE SUPPO HRUST- REVERSER		1				
APPRO	At rello			PROD. INF		OL BRACKET	- 1	1-199 HG. EFF.301-1999				
PARTS LIST ZONE	REPLAČES	8.8	300	REQD	PART NUMBER	NOMENCLATURE	ZONE		MATERIA	L HEAT	FINISH	P
(R	"∂69-4279-I	V	/	1	69 - 4279-3	FAIRING SUPPORT	AB			+		
	NEW.	/	/	1	69-5434	STIFFENER	AS					
	NEW	1	1	1	69-5434-1	STIFFENER	AB				1	
(RE	F) 6E-4522	V	~	1.	66-5025-1	STIFFENER ANGLE	<i>A3</i>					
	NEW	~	/	1	-3025	DOUBLER	AB	.040 ×.85 × 4.50	3	- -	F- 8.05	P

AIRPLANE SERIAL NUMBERS

CHANGE P/L AS SHOWN ABOVE;

SCRAP GG-4522 \$ 19-4279-1

RELEASE DWG COLUMN SHEET IND NO.

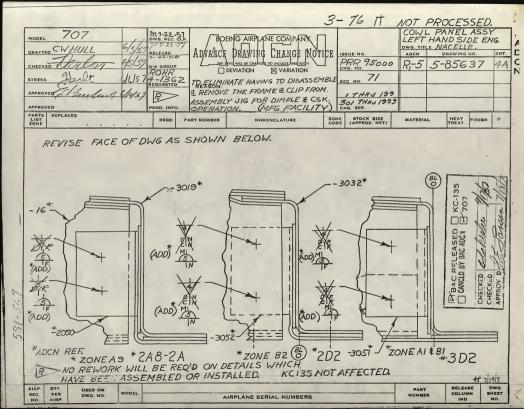
PART

NUMBER

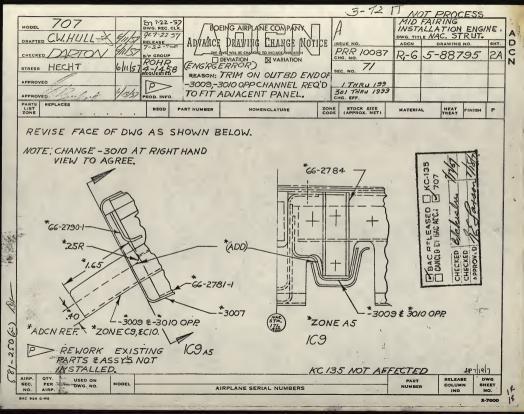
PER AIRP. USED ON

DWG. NO.

MODEL



				3-	-62 IT	NOT PR			11.15
MR. MATTESON A CHECKED A POTON	1457 B/PUNIT	ADVANCE	G AIRPLANE COMPANY STATE IT VALUESCOOL ORALVING CHANGE NOT. WILL BE CULVED TO INCLUST HISLAND VARIATION VARIATION	ICE ISSU	IE NO. EM 7130	A CANADA STATE OF THE STATE OF	E AS	NO.	OF
APPROVED APP	G/1457 ROHR 4-1390 REQUESTED	REASON: -:	3019,+3020 OPP CL EARLY DEFINED. GRG. ERROR)	-IP /	THRU 1995				
PARTS REPLACES	11901	ART NUMBER	NOMENCLATURE	ZONE	STOCK SIZE (APPROX. NET)	MATERIAL	HEAT	FINISH	P
			106	20	*\$1	ICKER V ZONE D	EW R	-1	
* ADCH REF.			2	*	- CAN	CRELEASE CLD BY BAS MIC		7/2	The second second
POREMORK EX		S & ASS	SY'S INSTALLE	D.	CHECK	(ED 060:	so-	7/18	5



						3-6211	MOTH	KOCES.	>
MODEL MATTE CHECK!	FCHT (FD)	WG REC	ADVACE REASON:	EING AIRPLANE COMPANY DRAVING CHANGE NOTIF DRAVING CHANGE NOTIF DEVIATION PART CALLOUT CHE RTS LIST BUT NOTIF ACE OF DUG. NGB FRON	5	ISSUE NO. ITEM 7455 CHG. NO. 74 ITHRU 199 301 THRU 1999 CHG. EFF.	FAIRING	NG EDGE S OUTBDA STRUT AS DRAWING NO. 3-8563	SY OF
PARTS LIST ZONE	REPLACES	REQD	PART NUMBER	NOMENCLATURE	ZON	E STOCK SIZE	MATERIAL	HEAT FIN	ISH P
			E WITHO				Blake	1707 sla 1/2	5 Contraction
1×A	DCN REF.								
	KC-135 No			T ASSEMBLED.		.// -			HF 7/10/1
AIRP.	QTY. USED ON PER DWG. NO.	MODEL	and the	AIRPLANE SERIAL NUMBERS	-		PART NUMBER	COLUMN	SHEET NO.

AIRPLANE SERIAL NUMBERS

DWG. NO.

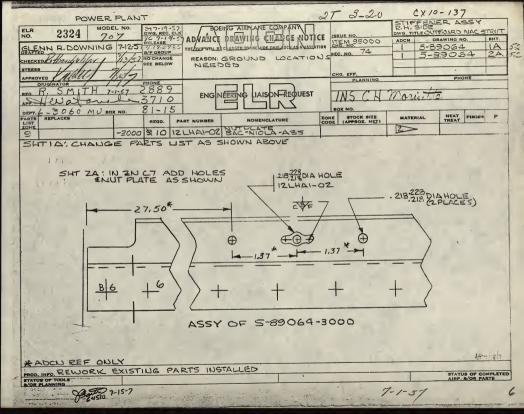
NO. AIRP

BAC 924 C-RS

1R 15-2-7000

:			2	-64	It (No	T PRO	CESS')	
DRAFTED C. ROSS & CHECKED DETON MESTRESS HECHT 6/6	8/P GROUP	ADVANCE REASON:	EING AIRPLANE COMPANY	TICE	SSUE NO.	UPPER DWG. TITLE	ET-N	SELD SELD	
PARTS LIST ZONE	REGD	PART NUMBER	NOMENCLATURE	ZONE	STOCK SIZE (APPROX. NET)	MATERIAL	HEAT F	INISH P	
1-10	1-5	-9	PAD	83	.25 X LIOX 1.0			R	1
NBN	1	-3800	PAD	C3	25X110X10			R	
(ADD) EXCEPT AS * ADCH REF D RUK EXIST	ING F	PARTS	*(AED) EXCE	TYF	P & PLAN	3800 Les J,	CONULD BY BRO AGN IC 1035	CHECKED STAKELLE 11/27	581-397
AIRP. GTY. USED ON SEC. PER DWG. NO. MODEL			RPLANE SERIAL NUMBERS			PART NUMBER	RELEASE	DWG	1
BAC 024 C-RS		- 4.7					IND	NO.	١, ٢

ADON



NO. AII

2.7000

			3-70 //
MILLARD DALE 7-12-7 MILLARD DALE 7-12-7 DATED CHECKE PRINGLES 1/12 STRESS A. Fluin 1/12/52 APPROVED 7/12/52	BOENG AIR ANE COMPANY ALLEAR ADVANCE DRAVING CHANGE NO BENEVICTOR PRODUMY AND CE FOR THE THRU ANCE FOR THE THRU ANCE FOR THE THRU PROD. INFO. PROD. INFO. PROD. INFO. PROD. INFO. PROD. INFO. CYLINDER	PRR 10749 CHG. NO. 71 SEC. NO. 1 THRU 199 301 THRU	COWL PANEL ASSY LH SIDE ENG NAC DRAWING NO BHT ACCN DRAWING NO NO 3 5-85637 100
PARTS REPLACES	REOD PART NUMBER NOMENCLATURE	ZONE STOCK SIZE	MATERIAL HEAT FINISH P
CHANGE ALL CALL	CONTOURS OF -3043 - 3090 9075 OF -3043 TO -3090 3090 3043	STICKER	NEW (4)

REWORK EXISTING PARTS

DWG RELEASE PART NUMBER QTY. USED ON DWG. NO. IND NO. AIRPLANE SERIAL NUMBERS MODEL SEC. PER AIRP.

BAC 924 C-RS

2-7000

-AIP 7/17/7

										_						8	//	-		
MODEL			300		7/1	DV	VG R	17-4 EC CL 1/18/3	K			G AIRPLANE COMPANY EPARTURE AUTHORIZ				POWE DWG TITLE	R PA	nck	. As	54.
	AFTED M. DONOUGH 7/0/2 RELEASE 2-19-57EG						LEAS	57/2				G WILL NOT BE CHANGED		ISSUE N	0.	DDA No.		DRAW	ING No.	
CHECKE	ECKED TILL 7/10/7 B/P GROUP								-		REASON:				10881	11		,	0 0	/
	DAMALISSON						Do	NAL	DSO	N	TO PRO	VIDE NECESSA	CHG. No.			50	-6	00	0	
STRESS	Mark	to.	ise	350	?/2		OD II					TS AT BAC		SEC. No.	76					
4	ED A	1/1	1			1	OP II				ON PROT	OTYPE ENGIL	DES	AIRPS						
APPROV	ED						ROR							2,3						
PARTS LIST ZONE	REPL	ACE	8	ارا	5	A	1.3	-2	-1	REQD.	PART NUMBER	NOMENCLATURE		ZONE (STOCK SIZE APPROX. NET) м/	TERIAL	HE	AT FIN	IISH F
	NE	W				V	1	V	V	10	65-6353	KIT INSTL-BRK	TS							
1	NE	w	V		V					ID	65-6353	KIT INST - BE	RETS							
	Net	N		V	1				-	20	65-6353	KIT INST- B	RKTS					-		amountaines .
	40	_				~ 1						_								***************************************

ADD TO P/L AS SHOWN ABOUG

AIRPS 1 2,3

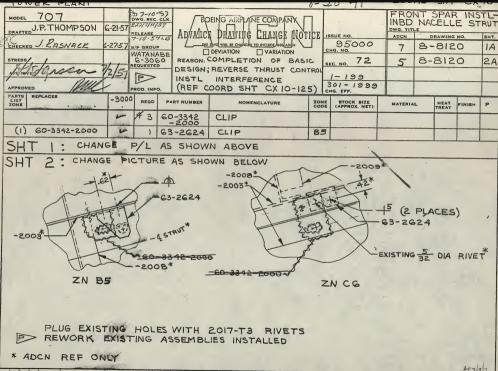
FOR INST, ON THE PROTOTYPE ENGINES.

USE FOR FLIGHT & CERTIFICATION TESTS ONLY

					_									8	· 6 /	//			
MODEL		70		7	7/	DW	77-1 G RE	C CL	K			G AIRPLANE COMPANY			POWE.	R PAI	CK . 1	4554	' .
DRAFTE	D'ILL	0,000	,,,,	, ,,	110/	RE	LEAS	E '			DRAWING D	EPARTURE AUTHORIZATION	ISSUE	No	DDA No.		DRAWING	No.	
CHECKE	CKEE 7/10/7 B/P GROUP DAMALIZSON						GRO	UP		4.1	REASON:	WIDE NECESSARY	PRR 1088 1		4	50-	68	06	
A Do	RESS PONALDSON REQUESTED PROD INFO										BRACKET	S AT BACO	SEC. N	0. 76	-				
APPROV	C	7/1	Ī			1	OP II				ON PROT	OTYPE ENGINES	AIR!						
APPROV						ELF	ROR							FF D					
PARTS LIST ZONE	REPL	ACE	8	اط	5	A	.3	-2	1-1	REQD.	PART NUMBER	NOMENCLATURE	ZONE	STOCK SIZE		TERIAL	HEAT	FINISH	P
	NE	W				V	1	V	V	10	65-6353	KIT INSTL-BRKTS					-		
	NE	w	V		V					10	65-6353	KIT INST- BOKTS					THE SALES AND ADDRESS OF THE SALES AND ADDRESS AND ADDRESS OF THE SALES		
	NEI	N		V	1				-	20	65-6353	KIT INST - BRKTS							
	400 01 40																		

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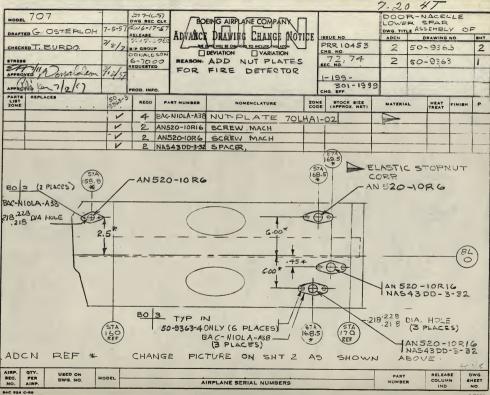
AIRPS 1 2,3
FOR INST. ON THE PROTOTYPE ENGINES.
USE FOR FLIGHT & CERTIFICATION TESTS ONLY



Lip ylaly NUMBER REQD WORK SLEEVE REOD ZONE SHT PRESS. TUBING MIN TUBE WALL HEAT TYPE ZONE MATERIAL TUBE ASSY IDENTвтоск END FITTINGS PER TURE ASEV OD THICK TREAT ENDS CODE LGTH BAC 924 E- R3

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MODEL	707-120	6-12-7	876-2 DWG. REC \$2716-2	CIE / PC	DEING AIRPLANE COMPANY			1	ET-MID FAIR NE NAC STRU	
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CHECK	Aughor		B/P GROUP		DEVIATION VARIATION	ا ا	95000	. 3	5-88795	2A
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PARTS LIST ZONE	REPLACES	-3000	REQD	PART NUMBER	NOMENCLATURE	ZONE	STOCK SIZE (APPROX. NET)	MATERIA	L HEAT FINISH	P
		-300Z -3001	+1	63-1791-1	GUSSET					
C	HANGE CALL	DUTS	AS .	FOLLOWS	ON SHT ZA					

ZONE A5 EDGE OF 66-2766 \$66-2790 CHANGED TO EDGE OF 63-1791-1 \$66-2790

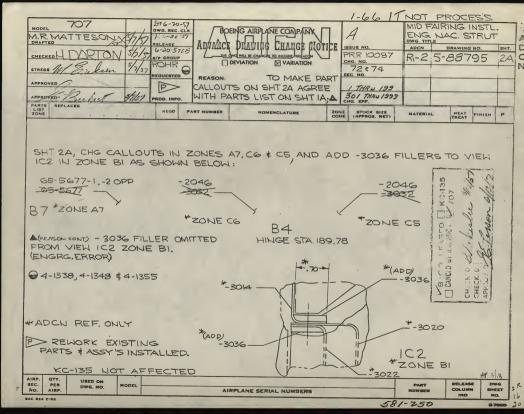
IN ZONE A5 "66-2766" CHANGED TO "63-1791-1

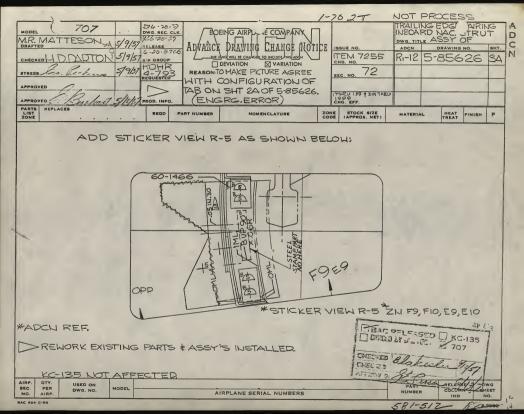
IN ZONE A6 EDGE OF 66-2766 66-2781-3"CHANGED TO EDGE OF 63-1791-1666-2781-3"

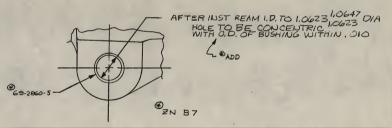
CHANGE P/L AS ABOUT ON SHT IA

* 63-1791 ALTERED TO SUIT THRUST REVERSER TUBING

						A	HP 6118
SEC. NO.	PER AIRP.	USED ON DWG. NO.	MODEL	AIRPLANE SERIAL NUMBERS	PART NUMBER	RELEASE COLUMN IND	DWG SHEET NO.



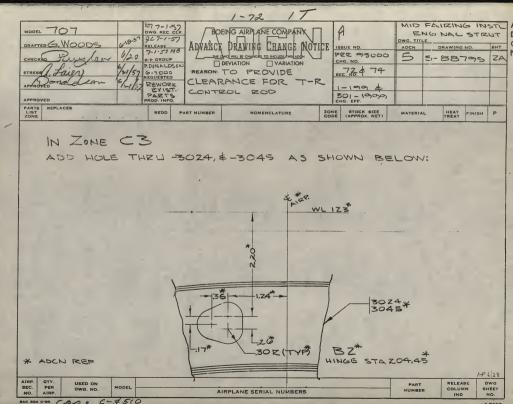




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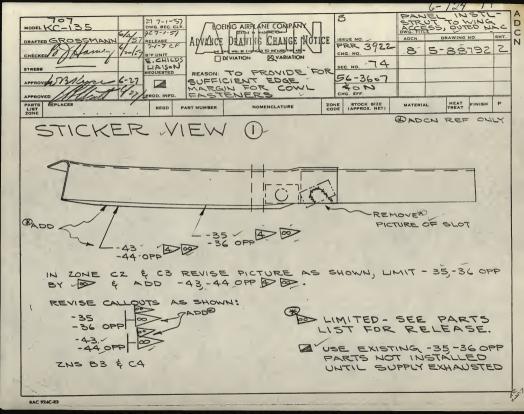
> ASSY'S COMPLETED MUST AGREE

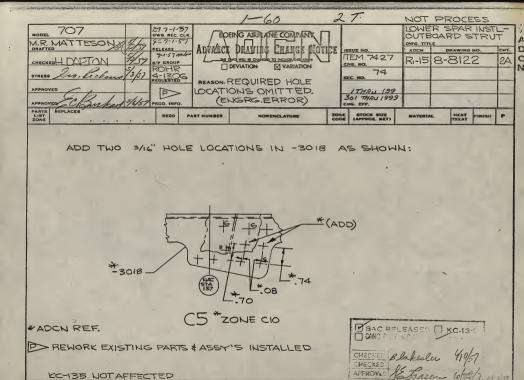
AH 5. 2 USED ON DEL EASE PART PER MODEL DWG. NO. COLUMN SHEET AIRPLANE SERIAL NUMBERS NUMBER AIRP NO £96-4510 6-14-7



2-7000

			6-110	
	G AIRPLANE COMPANY	8	SEAL INSTI	-
DRAFTEDGROSSMANN TOT RELEASE ADTIMOT	DRAWING CHANGE NOTE	CE ISSUE NO.	ADON DRAWING	
CHECKED BY Hamey 1/2/15 8/8 GROUP LINE DWG	WILL BE CHANGED TO INCLUDE THIS ADON	PRR 3922 PRR 9500	17 5-895	500
DEN	Z) TO ELIMINATE			
REQUESTED REASON DIF	FICULT FASTENERS	PRR 3022		
APPROVED My 6-27 P (PER 9500)	TO FACILITATE JUSTILL WEB-STRUT	: 56-360] & ON		
APPROVED STOWING TO WIN	To the state of th	PRR 9500		
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AN 520-DD10-RB	2 PLACES FO	R TOA	GREE WITH	
(6 PLACES)	ZONE B3	69-5	036-5,69-50 5036-7 & 69-	5036-8
ZONE B3	2012 00	,	SPECTIVELY.	
PRR 3922:			1932-BEEDE ARBACH 645	
IN ZONE BI ADD F REVISE		BI & CB. LIN		
CALLOUT:		OPP BY AD		
.136:150 DIA HOLE 7-16 0		75 69-5036		6 OPP;
-136 DIA HOLE	62-2026	7, 69-5036-8	OPP	
	69-5036 69-5036			6V.
AN 960-PD6 100	63-3036			1
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(CILACES)		20 OFP	-22	OPPL
-16007	4 1 .	9-5036-5 9-5036-6 OPP		5036-7 5036-8 CFP
-1609				3030 0011
-22 OPP 00	ZONE BI		VE C3	
69-5036-7		CN REF ONL	- ' '	7
69-5036-8 OFF		> LIMITED -		
69-5036-6 OPPL ZONE BI	9	FOR REL		
AIRP. QTY. USED ON MODEL.	The second dimension		PART RELE NUMBER COLU	MN SHEET
N AIRP. AIRS	PLANE SERIAL NUMBERS		IN	D NO.





AIRPLANE SERIAL NUMBERS

AIRP. QTY.

SEC. PER

BAC 924 C-RS

AIRP

USED ON

MODEL

DWIS SHEET NO.

RELEASE

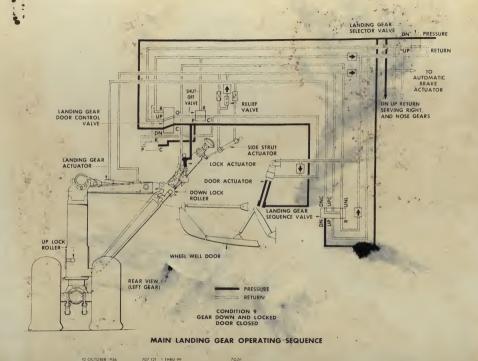
COLUMN

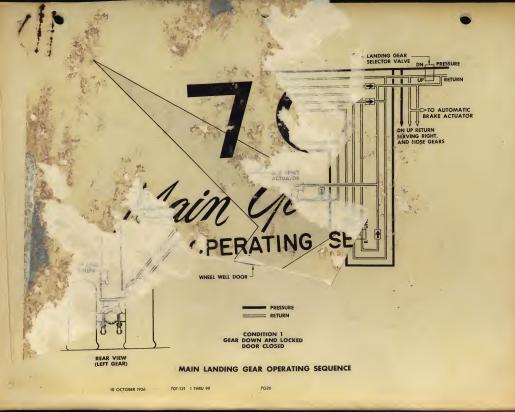
PART

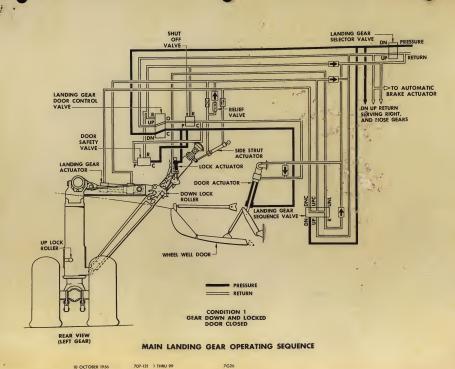
RUMBER

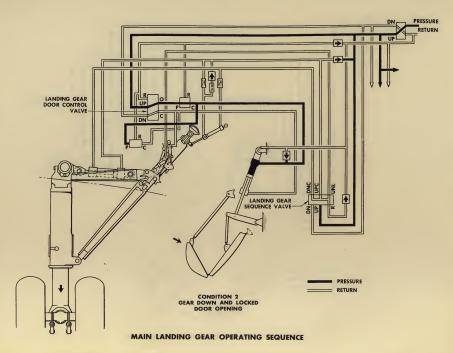
281-502

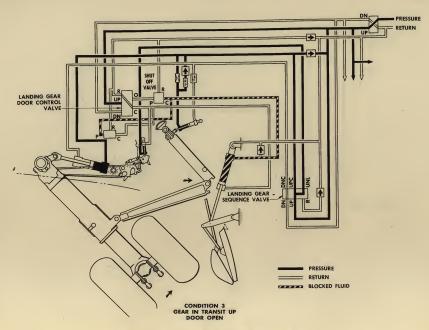
		100		1,00			Bridge Company
	PR COMPONENT	BOEIN	IL LUBRICATI	ON LIST FOR COMPANY	. 707 AIRF	LANES	PAGE NO. 59 OF PAGES MFGRS, NO. D 6-1539 DATE LAST REVISION 11/18/57 DATE APPROVED
ITEM NO.	LUBRICATION POINT	BEARING TYPE	LUBRICANT	METHOD OF APPLICATION	NO. OF APPLICATION POINTS	LUBRICATION INTERVAL	REMARKS
1	Carriages - Center	RD N	MIL-G-3278		12 8	#11 2 200	Flush Fitting (Dwg. 5-87846).
2	Carriages - End	RD N	MIL-0-3278 MIL-0-3278	Gun Gun-	24 16	#h	Flush Fitting (Dwg. 5-87847).
3	Flap & Spoiler Metering Valve Assy	-	MIL-0-5606 or Skydrol 500 (As appli- cable)	Fill	6/airplane	#h	Gear case (Dwg. 50-6875).
				σ ~ ⁴			*
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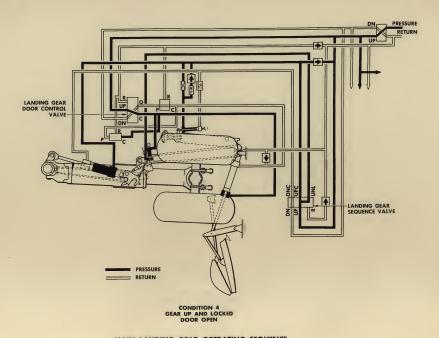




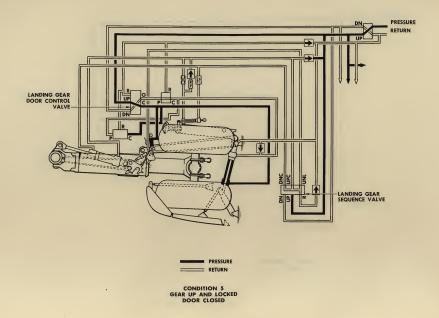


10 OCTOBER 1956

707-121 1 THRU 99

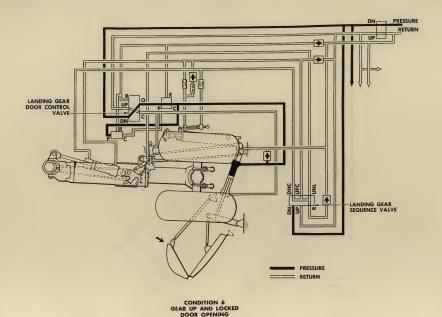


707-121 1 THRU 99



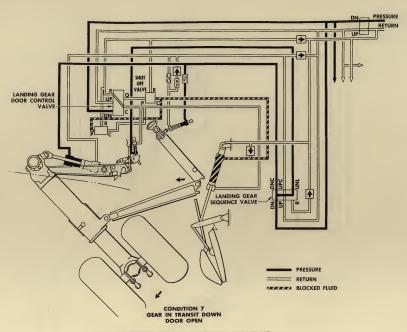
10 OCTOBER-1956

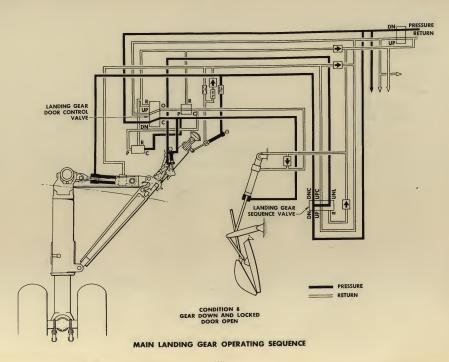
707-121 1 THRU 99



10 OCTOBER 1956

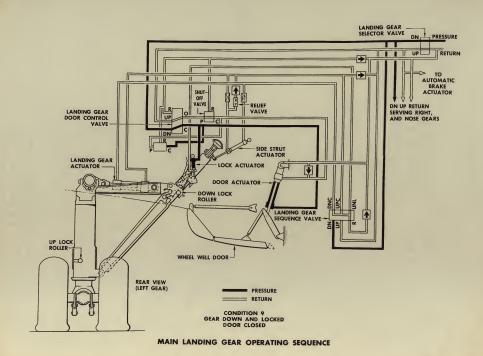
707-121 1 THRU 99





10 OCTOBER 1956

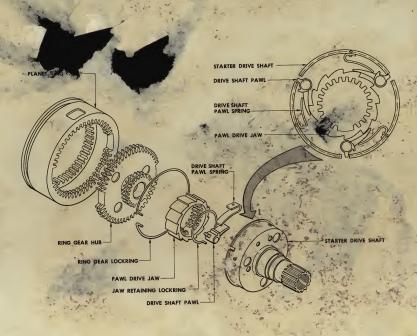
707-121 1 THRU 99



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10 OCTOBER 1956

707-121 1 THRU 99



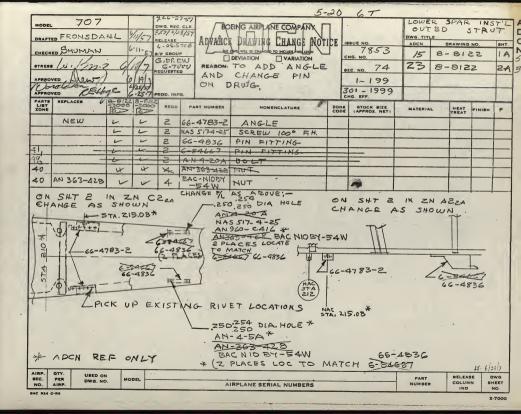
STARTER CLUTCH SCHEMATIC

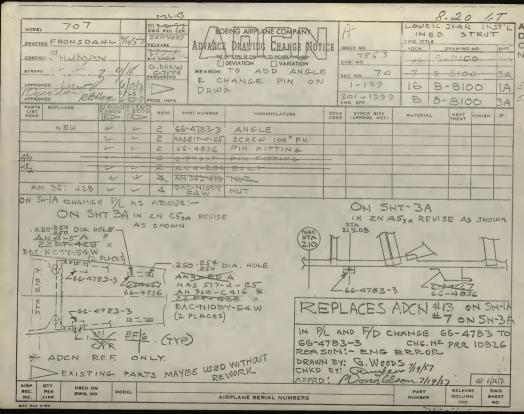
701-121 1 THRU 99 REV 14 MARCH 1957

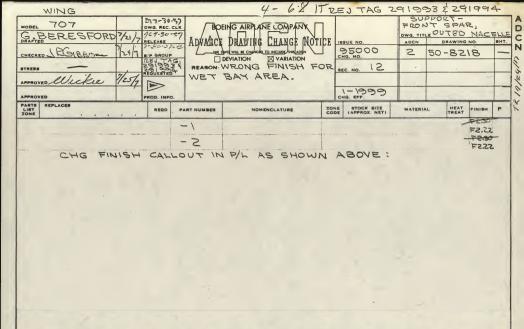
121-80-5 REV A

FRAME NO. B

BLACK PLATE OF

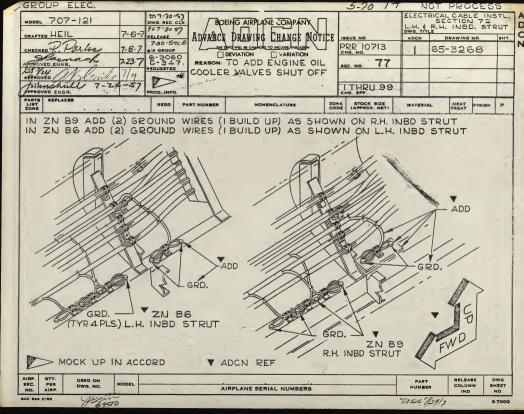


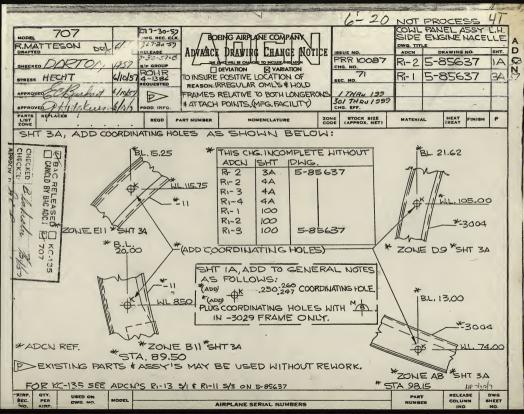


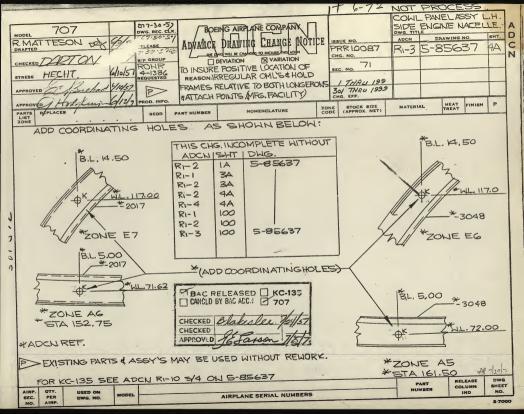


REWORK EXISTING DETAILS RY STRIPPING ALL PRIMER AIP # 1,2,3 IN ACCORD -

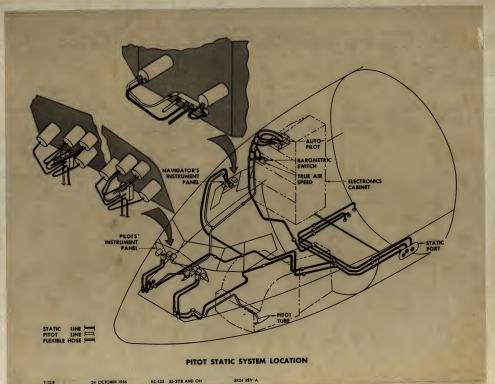
AIRP. RELEASE DWG QTY. PART USED ON SEC. PER MODEL COLUMN SHEET DWG. NO. NUMBER AIRPLANE SERIAL NUMBERS NO. AIRP BAC 984 C-RS







FIELD SERVICE REPORT BOEING AIRPLANE COMPANY OPERATIONS DEPT ENGINEERING SERVICE SECTION ENGINEERING SERVICE SECTION FAS Air Bottle Control Valve, KC-135. CLASSIFIED [UNCLASSIFIED X ROUTING: The reference advised that an improved model of the subject, P/N 38E13-8A, has failed to be a significant improvement over earlier models, P/N 38E13-3A and 840891. Service experience and number ORIGINAL of failures of each model was requested. Air Force U.R.'s and BAC Edits indicate the following valve removals: A/C Date Valve T/T Removed For 19 Hrs. Air Leak 57-2609 700 Air Leak 58-001 8/19/59 713 268 Failed Relief Valve 58-006 9/10/59 786 270 Loose Gage BASE FILE 57-2594 9/29/59 685 347 Air Leak 58-097 11/27/59 2/18/60 691 140 Gage Sticks 57-2609 Air Leak at Vent Supply records show that in the last 365 days 17 P/N 840891 valves have been issued. No P/N 38E13-3A or -8A valves have been issued. Unfortunately, this activity has had little service experience with he P/N 38E13-8A valve. Frank A. Britt Field Service Engineer FAB: ps 0106 Frank A. Britt REPORT NO BERGAFB-910-75F 21 June 60 Bergstrom AFB LOCATION Austin, Texas FAS Air Bottle Control Valve, KC-135. MODEL KC-135. 6-7171-1-12560, dated June 15, 1960 NCLOSURES FSR FSR FSR FSR FSR FSR FSR

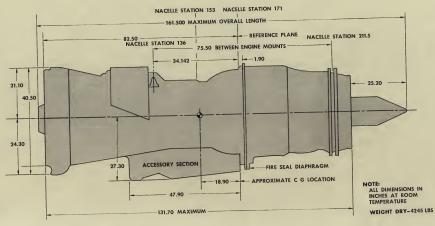


					2-63				
ELR 813 MODEL NO. 707	DWG. REC. CLK R 46-25-57	/ A \	EING AIRPLANE COMPANY	A	J SUE NO.	CONTROL -STA 600			
DRAFTED EKARA 4/5/57	V 15 57CB	" WALLET	E DRAVILIG CHANGE HOTE	ION C	G. NO. 53	ADCN 6	59 - 19		SH4.
STRESS STRESS	NO CHANGE SEE BELOW		TO PRIVIDE	SE	1-1999				7
APPROVED Bailly 6-20-5	PHONE	FICOTO	EL FINISIS	CI	IG. EFF.		РНС	ONE	
	4192	ENG	VEERING LAISON REQUEST	1	PEKASKY		3-16	9	
PARTS REPLACES	0-19 REQD. PI	RT NUMBER	NOMENCLATURE	ZONE	OX NO. 9/-90 STOCK SIZE	MATERIAL	HEAT	FINISH	Р
ZONE		-4		CODE	(APPROX. NET)) IREA!	2.1/5	
		-5						52F 2115	
	h		<u></u>					-	

CHANGE PIL AS SHOWN ABOVE

REWORK PHIETS INSTRUCE



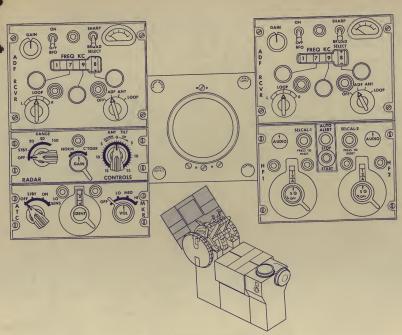


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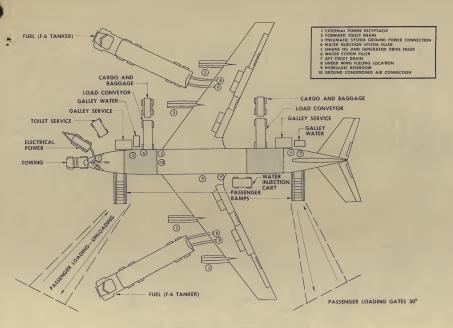
OVERALL DIMENSIONS-JT3C-4 ENGINE

9 AUGUST 1956 707-121 1 THRU 99

21-71-5



FORWARD ELECTRONIC CONTROL PANEL

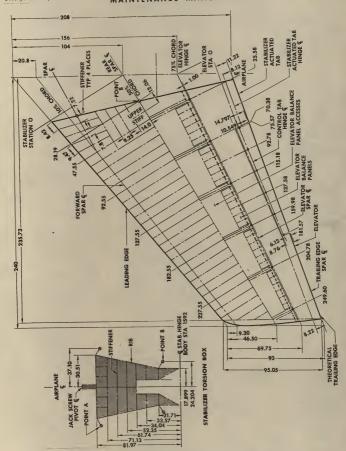


TYPICAL TERMINAL SERVICING ARRANGEMENT

REV NOV 25/57

707-121 | THRU 99

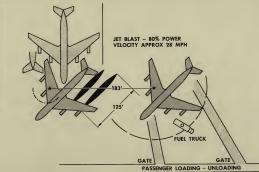
121-12-1 REV C



CANTED PARKING NOSE IN

ADVANTAGES:

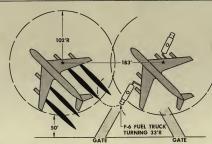
- 1 NO STARTING BLAST TO AFT AIRPLANES
- 2 PASSENGER LOADING FROM ONE GATE IF DESIRED
- 3 ADEQUATE AREA FOR REFUELING WITHOUT PASSENGER LOADING CONGESTION



CANTED PARKING NOSE OUT

ADVANTAGES:

- 1 RAPID DEPARTURE
- 2 TAXI BLAST CONFINED TO RAMP AREA OF DEPARTING AIRPLANE ONLY

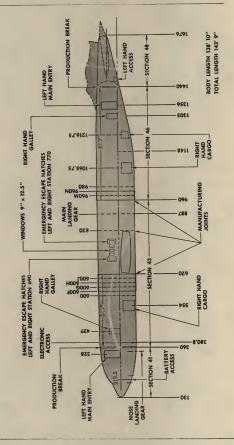


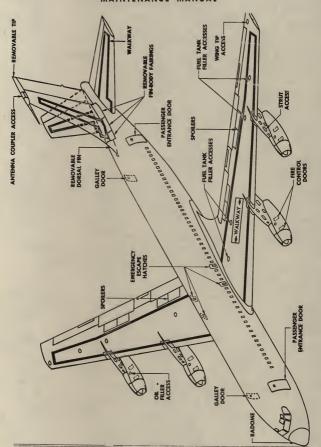
TYPICAL PARKING

9 AUGUST 1956

707-121 1 THRU 99

151-10-1

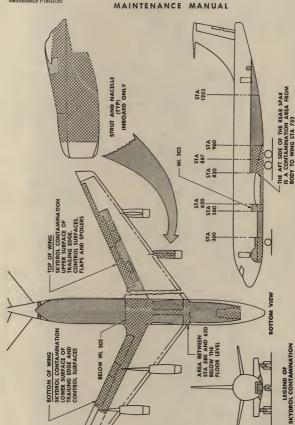




Walkways, Access Doors and Inspection Openings - Top View Figure 202

END 12-2-0 Page 203

May 20/57



Anticipated Skydrol Contamination Areas Figure 201 END 12-3-0 Page 201

INTERIOR AND EXTERIOR
INTERIOR ONLY
EXTERIOR ONLY

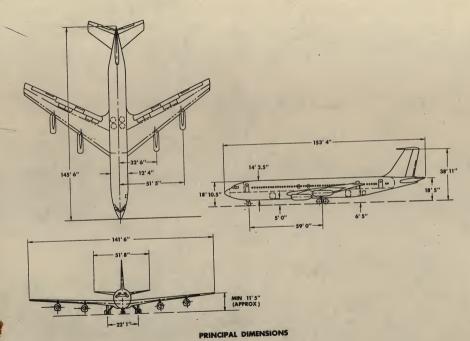


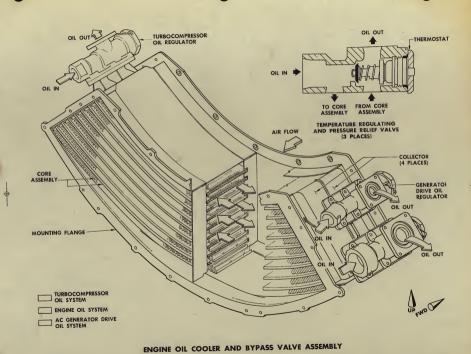
FIG. 1

9 AUGUST 1956 707-328

707-328 2101 THRU 2199

1224

10,40 T 575 5P74 10,53 T425 5P21



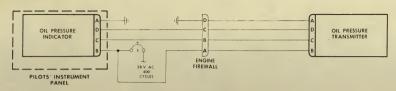
121-79-2 REV A

707-121 1 THRU 99

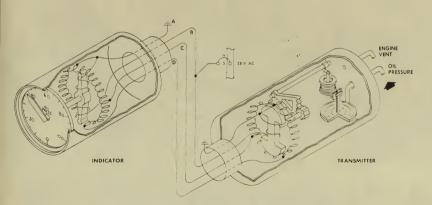
REV 22 AUGUST 1957

BLACK PLATE OF 4

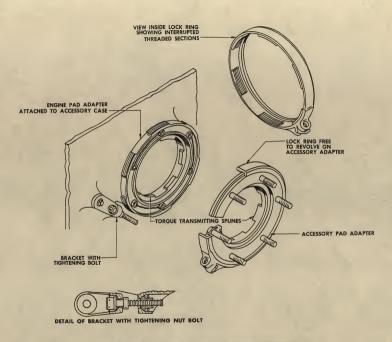
FRAME NO. B



TYPICAL-ENGINES 1, 2, 3, 4



OIL PRESSURE INDICATING SYSTEM SCHEMATIC

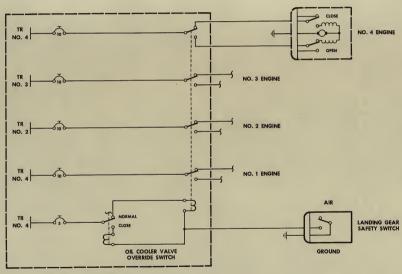


FUEL PUMP AND FUEL CONTROL QUICK-DISCONNECT

y 1957 707-121 1 THRU 99

121-73-8

10 MAY 1957



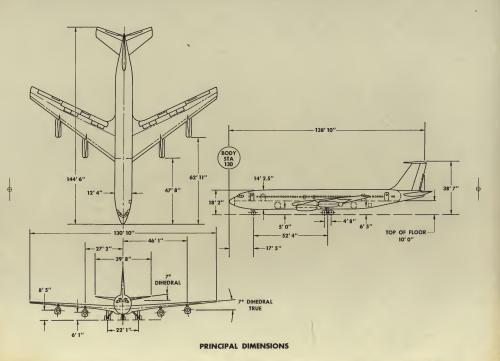
FLIGHT ENGINEER'S PANEL

OIL COOLER EJECTOR VALVE OVERRIDE

REV 29 JULY 1957

707-121 1 THRU 99

121-79-6 REV A



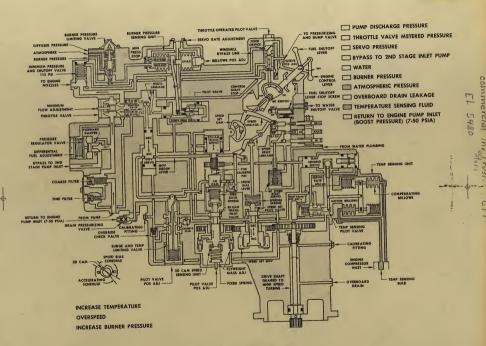
REV 14 OCTOBER 1957

707-123 101 THRU 199

123-6-1 REV A

FRAME NO. B

BLACK PLATE OF 2



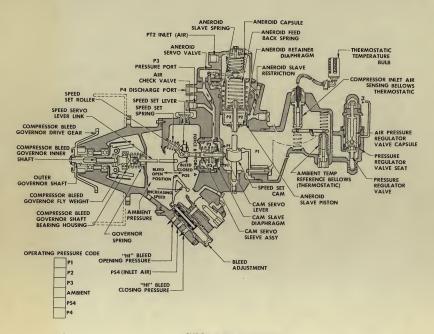
ENGINE FUEL CONTROL UNIT

707-121 1 THRU 99

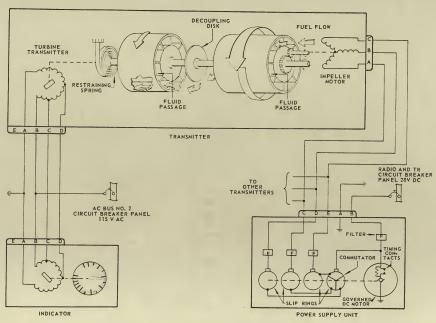
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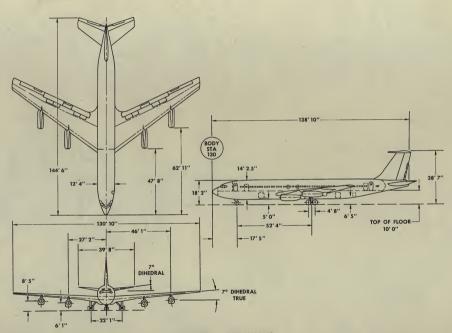
BLACK PLATE OF 5



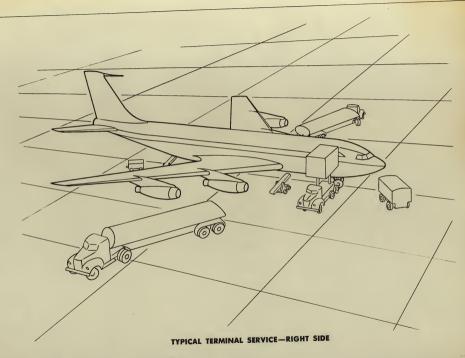
SURGE BLEED GOVERNOR



FUEL FLOW INDICATING SYSTEM SCHEMATIC



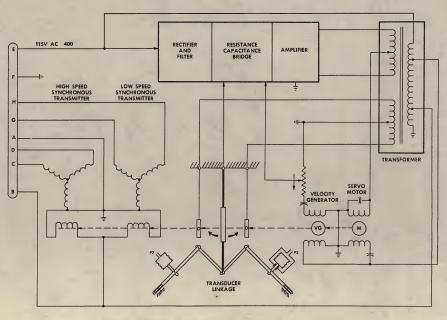
PRINCIPAL DIMENSIONS



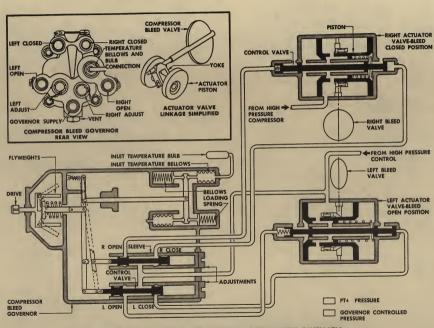
30 AUGUST 1957

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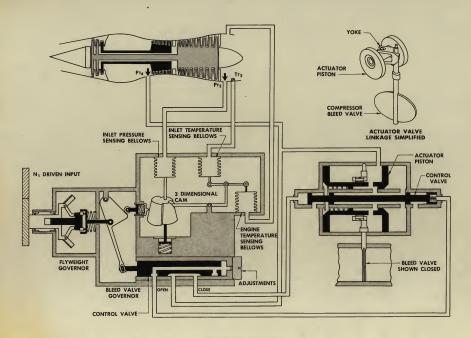
ENGINE PRESSURE RATIO TRANSDUCER OPERATIONAL SCHEMATIC



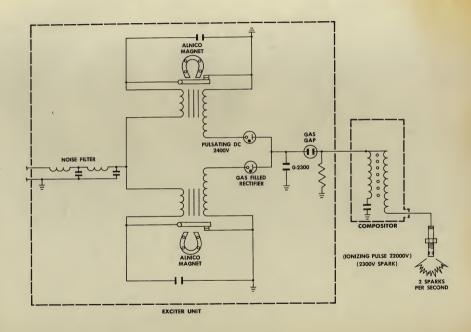
ENGINE COMPRESSOR SURGE CONTROL BLEED SYSTEM SCHEMATIC

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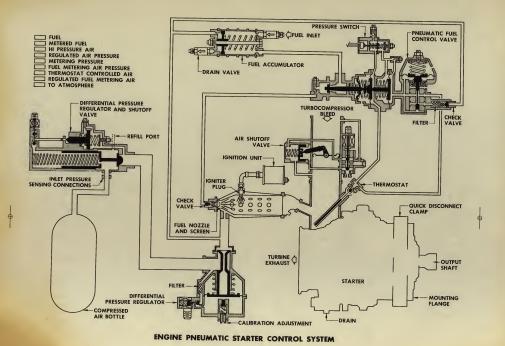
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SURGE BLEED CONTROL



ENGINE IGNITION



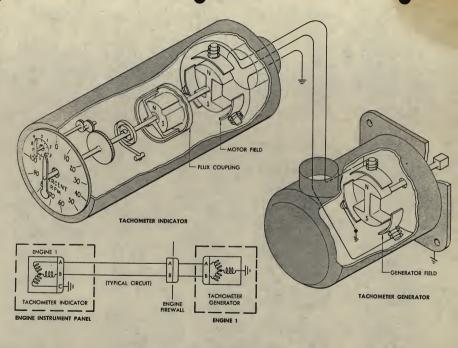
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FRAME NO. B

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17 MAY 1956

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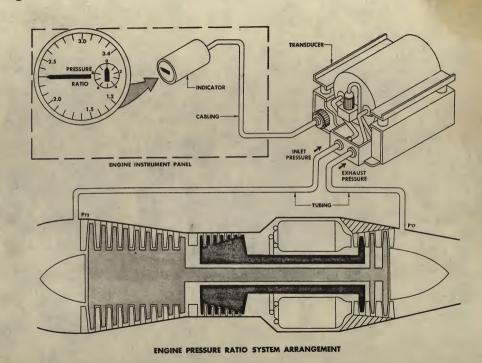
ENGINE SPEED INDICATING SYSTEM

10,32

20 OCTOBER 1955

KC-135 55-3118 AND ON

5P2



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KC-135 55-3118 AND ON

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DE RBEGUP Ø27

P 221817Z

FM AFESO BAR EAST HARTFORD CONN

TO RJWFNH/COMDR SAAMA KELLY AFB TEX
INFO RJWFNK/COMDR OCAMA TINKER AFB OKLA
RJWXBR/COMDR SAC OFFUTT AFB NEBR
RUWKBF/AFPR BAC SEATTL WASH

RJEDSQ/COMDR AMC WPAFB OHIO RJEDSQ/COMDR WADC WPAFB OHIO

RJEBKG/AFPR BAC WICHITA KAN
RBEGTDS/HAMILTON STANDARD WINDSOR LOCKS CONN

NAVY GRNC

BT

UNCLAS FROM SANEK-1-88-E FOR SANETA OCAMA/OCNUTA SAC/DM4C AMC/MCMT WADD/
WCLP X SUBJECT: REVISED MINIMUM FLOW SETTING JFC-12 FUEL CONTROL,

J-57-43W ENGINES X FOLLOWING PWA MSG IS QUOTED FOR YOUR INFO X
QUOTE. AS THE RESULT OF RECENT INSTANCES OF FLAME OUT OF J57-43W
ENGINES INSTALLED IN KC-135 ACFT ATTRIBUTED TO FROSTING OF THE
METERING VALVE, THIS CONTRACTOR IS PROCESSING A CLASS II ENGINEERING
CHANGE IN DESIGN 92150 TO INCRASE MINIMUM FUEL FLOW APPROXIMATELY
200 PPH. IT HAS BEEN DETERMINED THAT THIS INCREASE IN MINIMUM FLOW CAN



ENS. PE 3

SING THE MINIMUM FLOW STOP ON INSTALLED JFC-11 FUEL CONTROLS USING THE FOLLOWING PROCEDURE.

1. LOCATE THE THROTTLE VALVE SLEEVE JUST AFT OF THE INLET AND

THECTED IMMEDIATELY BY ADJUST

A kump B ligh

PAGE TWO RBEGUP Ø27

BY-PASS PORTS WHEN THE CONTROL IS MOUNTED ON THE ENGINE. 2. LOCATE THE MINIMUM FLOW ADJUSTMENT IN THE CENTER OF THE THROTTLE VALVE SLEEV. THIS ADJUSTMENT IS FITTED WITH AN ALLEN SOCKET AND HAS ELEVEN NOTCHES. NOTE: DO NOT DISTURB THE LOCKING PLATE ON THE OUTER PERIPHERY OF THE THROTTLE VALVE SLEEVE. 3. MARK THE SLOT ON THE THROTTLE VALVE CASTELLATED NOTCH IN WHICH THE LOCK RING IS INSTALLED. REMOVE THE LOCK RING FROM ITS SLOT AND THUS FROM ITS NOTHC IN THE MINIMUM FLOW STOP. A SUITABLE ALLEN WRENCH, ROTATE THE MINIMUM FLOW STOP COUNTERCLOCKWISE UNTIL THE NEXT NOTCH ON THE MINIMUM FLOW STOP LINES UP WITH THE MARKEDSLOT OF THE CASTELLATED NOTCH ON THE THROTTLE VALVE SLEEVE. REPLACE THE LOCKING RING IN THE SAME MARKED SLOT FROM WHICH IT WAS REMOVED. THIS ADJUSTMENT ROTATES THE MINIMUM FLOW STOP APPROXIMATELY 33 DEGREES COUNTERCLOCKWISE AND INCREASES MINIMUM FUEL FLOW 200 PLUS 6. AFTER INCORPORATING THE FOREGOING ADJUSTMENT, PAINT A 1/4 INCH WHITE DOTE ON THE FACE OF THE THROTTLE VALVE SLEEVE for -43 WB engines for-43WaWA ungin AND REIDENTIFY THE P OL 524950 CONTROL AS L-4 AND THE P/L 501157 CONTROL AS L-17. UNQUOTE. OCAMA TCTO 1C-135(KA)765 COVVERS THIS CHANGE PER AGREEMENTS AT WADC PROPULSION LAB MEETING 15- 16 JAN 59 PWA EC 92150 IS ASSIGNED THIS CHANGE X OUR REP AND PWA DID NOT AGREE IT WAS NECESSARY TO RUN ENGINE OR USE ACFT FLOW METER TO DETERMIN IF 200 LB INCREASE WAS BEING OBTAINED BY ADJUSTMENT X FLOW METER

INCREMENT BREAKDOWN NOT ADEQUATE FOR REFINED READING. REQUEST
RUNNING OF ENGINE/USE OF FLOW METERS BE DISCONTINUED IN CONNECTION
WITH THIS ADJUSTMENT IF IN EFFECT X ACCURACY OF THIS ADJUSTMENT
HAS BEEN ASSURED AT PLUS OR MINUS 15LBS ON CALIBRATED TEST BENCH
FLOW METER X BLUE DOT IS ACCEPTABLE IN LIEU OF PWA WHITE DOT X
PROD CONTROLS WILL BE INDENTIFIED BY P/T CHANGE X

PAGE THREE REEGUP Ø27

UNDER NO CIRCUMSTANCES WILL ADJUSTMENT EXCEED ONE REPEAT ONE NOTCH
ON MINIMUM FLOW STOP

BT

22/1817Z JAN RBEGUP

FIELD SERVICE REPORT BOEING AIRPLANE COMPANY
7/0
TO: ENGINEERING SERVICE DEPARTMENT SEATILE WICHITA WIC
ECT: Difficulties with Throttle Control CLASSIFIED UNCLASSIFIED
_
This report will describe an incident involving the "freezing" of the # 4 engine throttle of aipplane 3132 on May 14, 1959.
Following a wet take-off, ambient temperature +19°C, the airplane was climbed to 32000 feet altitude, ambient temperature -45°C, and remained at this altitude for the next two hours. At about 1:45 hours at 32000 feet altitude the throttles were moved to adjust engine speed without observing ambing abnormal. When trying to adjust the engines cannot be retarded below 85% rpm. The airplane was returned to Castle and prior to let-down the # 4 engine was shut-down by pulling the fire switch. After landing the throttle could be moved without difficulties.
The flight was aborted, flight time 4:20 hours. Flight time of the air plane: 829:30 hours.
During ground check on May 15, 1959 no discrepancy could be detected even after the water lines to the right hand engines was pressurized. In order to clear the airplane the AF personnel replaced the Bendix fuel control of the # 4 engine, despite advise to the contrary.
- KELLAN
Paul Rilling
Paul Ribanyi
SERVICE DIFF USER/CT FILE
A CONTRACTOR OF THE CONTRACTOR
FLE 0501 KC-135
Cham and God.
NAME Paul Ribanyi REPORT NO. CAFE-OES-727 DATE May 15,1959 ON Castle AFB LOCATION Merced, California
SUBJECT Difficulties with Throttle Control MODEL KC-135 REFERENCES None ENCLOSURES None
FSR FSR FSR FSR FSR FSR FSR
BAC 1264-R2 TOR FOR FOR FOR FOR FOR



M.S. AIR SCALE BOENIE SEATTLE WASH

8 mg PH 360

WK B Ø1 5 WUB Ø3 2 WMB Ø9 8

CONTRALT ADM

RR RUWKBF

DE RJWXBR 1 06X

R 0220457 7EX

FM CINCSAC

TO RUWKBF/AF PLANT REP BOEING APCO SEATTLE WASH

RJWFNH/SAAMA

RJWFNK/OCAMA

RBEGUP/AFESO PRATT AND WHITNEY BAR EAST HARTFORD CONN

INFO RJEBKF/2AF

RJEX DH B/ SAF

RJWBKN/15AF

RJWX BRF/ 4321ST RATWG

RJWFGM/ 41 3 25T RATWG

AFGRNC

BT

UNCLAS DM 4A 1 01 35.

ACTION AFPR BOEING - SEATTLE; SANET, SAAMA; SANEK, AFESO; CNSP, OCAMA INFO ALFA; 4321 STRAT WG; 4130 STRAT WING; 7 BOMB WG; LMSJ, AMC; B52/KC-135 OES; AFCDI-2, OTIG; 4039 STRAT W 52& AJAFSEL CONTROLS KC-135 AIRCRAFT. AFPR BOEING-

SEATTLE UNSATISFACTORY REPORT REPLY DATED 19 JAN 60 TO 2AF CONCERNING UR'S 4321 SW59-1, 4321 SW59-2, 4130 SW59-360,

59-292 ON AJA 4 FUEL CONTROLS, THE REFERENCED REPLY STATED THAT THE UR'S WERE MADE NON-PROJECT BECAUSE THE ELAPSED TIME BETWEEN

THE TIME UR WAS WRITTEN AND RECEIVED AT THE PRIME AMA WAS TOO

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abig.

PAGE TWO RUNXBR 196X

LENGTHY AND THE UR'S CONTAINED INSUFFICIENT DETAILS. THIS HEADQUARTERS DOES NOT CONCUR WITH THIS ACTION. THE AVERAGE TIME ON THESE UR'S FROM THE TIME THAT THE UR WAS SUBMITTED BY THE ACTIVITY UNTIL THE TIME THAT THE UR WAS FORWARDED TO THE AFPR FROM 2AF WAS 13 DAYS. THE SHORTEST TIME WAS 5 DAYS AND THE LONGEST TIME WAS 20 DAYS. THESE TIMES ARE CONSIDERED REASON-ABLE UNDER THE PRESENT UR SYSTEM. HOWEVER. THE PRIMARY REASON THAT THE HEADQUARTERS DOES NOT CONCUR WITH MAKING THESE UR'S NON-PROJECT IS THAT UNITS CONTINUE TO EXPERIENCE DIFFICULTY WITH FUEL CONTROL MALFUNCTIONS. IN ADDITION, THE AJA4 FUEL CONTROL IS A CRITICAL SUPPLY ITEM. THE DIFFICULTIES AS STATED IN THE REFERENCED UR'S ARE STILL PREVALENT THROUGHOUT THE COMMAND. FOR EXAMPLE. SAF NOW HAS 12 FUEL CONTROLS WHICH CANNOT BE WET-TRIMMED PROPERLY AFTER COMPLIANCE WITH T.O. 1C-135(K)A-836. AN INVESTIGATION OF TWO CONTROLS FROM RAMEY AFB SHOWS THAT THE BASIC REASON THAT THE CONTROLS COULD NOT BE WET TRIMMED WAS FAULTY FUEL CONTROLS AND NON COMPLIANCE WITH DRY-UP TRIM TECHNIQUE. THE DRY-UP TRIM REQUIREMENT ONLY REVEALED THAT THE CONTROLS WERE MALFUNCTIONING. IN VIEW OF THE ABOVE FACTS WE REQUEST THAT YOU MAKE THE ABOVE UR'S REPEATS ON AN ALREADY

ASS

PAGE THREE RJWZBR 106X

ESTABLISHED PROJECT OR THAT A PROJECT BE ESTABLISHED TO DETERMINE AJA 4 FUEL CONTROL DIFFICULTIES. THE REFERENCED LETTER ALSO STATED THAT ROUTINE UR'S SHOULD BE REPORTED BY TWX. SUCH ACTION IS INCONSISTENT WITH T.O. 80-35D-54. REQUEST THAT SAMA TAKE APPROPRIATE ACTION TO AMMEND T.O. 80-35D-54 IF DEEMED NECESSARY. IF SAAMA FINDS THE REACTION TIME UNDER THE PRESENT UR SYSTEM TOO LONG TO GAIN ACCESS TO UR EXHIBITS THEN REQUEST SAAMA SEND A FUEL CONTROL TECHNICIAN TO ONE OF THE FOLLOWING BASES TO INVESTIGATE CURRENT FUEL CONTROL PROBLEMS; (1) CRIFFIS AFB N.Y.; (2) LORING AFB ME.; (3) WESTOVER AFB MASS.

22/2116Z DE RJWXBR

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	ORDER HTM.3ER	MCGAUST	PAA-121 DC-1048	AA-123 D6-2757	CAL-124 D6-2756	TWA-131 D6-2758	UEA-136 D6-2763	CUB-139	Bir-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-2744	BCAC-436	137
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A.I.T. GRUER HUNBER	SECTION 76	PAA-121 D6-1046	AA-123 D6-2757	CAL_124 D6_2756	TWA-131 D6-2758	4EA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-2764	BOAC-436	AII-437
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A.T. ORDER	SECTION 15	PAA-121 D6-1048	AA-123 D6-2757	CAL-124, D5-27.56	TWA-131 D6-2758	38A-138 D6-2763	CUB-139	BKF-227 D6-2759	PAA-321	AF-328 56-2761	9AB-329 D6-2760	TWA-331	LUFT-130 D6-2764	BOAC-436	A11-437 D6-2762
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	ART ORDER NUMBER	SECTION 72 ENGINE	PAA-121 D6-1048	AA-123 D6-2757	CAL-124 D6-2756	Twa-131 D6-2758	QEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-2764	BOAC-L36	AII -437 D6-2762
	7,2-1	Engine Internal Arrangement	g- 🗵	829											X	
	72-2	Engine Bearing and Accessory Drive Schematic	\times													
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AAT ORDER NUMBER	SECTION 71 POWER PLANT - GENERAL	PAA-121 D6-1048	AA-123 D6-2757	CAL-12h D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2750	TWA-331	105-2764	BOAC-L36	AII-437 D6-2762
71-1	Power Plant Installation	B	300			. 🗵		X						X	
71-2	Engine Installation Equipment	X	×	X	X					100					
71-3	Engine Mount Details	A										1			
71 - ii	Engine Load Diagram	× ×			L.			Pai							
71-5	Overall Dimensions - JT3C-4 Engine	×	-	×	×			PailX				-			
-16	Engine Cowling	Pu X									1				
71-7	Engine Nose Cowl and Tab Assembly	P.u. C												1.	
71-8	Engine Load, Strut Structure and Access Diagram	A										1			
71-9	Engine Front View	× 647 5		L								-			
71-10	Engine Left Side View	Pai													
7i-11	Engine Rear View	200			1	1					1	1		1	

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ART ORDER NUMBER	SECTION 57 WINGS	PAA-121 D6-1048	AA-123 D6-2757	CAI_124 D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-2764	BOAC-Li36	AII-437 D6-2752
57-1	Wing Centerline Diagram	. X										L			
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AAT ORD ER NUMBER	SECTION 56	PAL-121 D6-1048	AA-123 D6-2757	CAL_124 D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TNA-331	LUFT-130 D6-2764	BOAC-136	AII-437 D6-2762
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56-2	Passenger Cabin Window	×					, L		L						
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AMT ORDER NUMBER	SECTION 52 Cont. DOORS	PAA-121 D6-1048	AA-123 D6-2757	CAL-124 D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BHF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-430 D6-2764	BOAC-136	AII-437 30-2762
52-12	Emergency Escape Hatch	X		× ×	A	K	K	×	S.		2	K	K	K	K
52-13	Emergency Escape Hatch Removal	×	×	×	×	X	×	K	X	Z	E	X		K	K
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ALCT ORDER NUMBER	SECTION 51 STRUCTRES - GARDAN '	PAA-121 D6-1048	M-123 D6-2757	CAL_124 D5-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BVF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-2764	BOAC-436	A11-437 D6-2762
51-1	Sectional Breakdown	B	C. C.								L		L	611	
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AAT ORDER NUMBER	SECTION 38 WATE: AND WASTE	PAA-121 D6-1048	AA-123 D6-2757	CAL_124 D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-430 D6-2764	BOAC-1/36	AII-437 D6-2762
311-1	(Typical) Cabin Water Systems	2 0	La		×			L.							
3(1-2	Forward Water System)	\boxtimes	X									L			
30-3	Aft Water System	×	×		[•					L			L	-
36-4	Toilet System	×						Ĺ						l,	
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-	AKT ORDER NUMBER	SECTION 34 (cont.) HAVEGATION	PAA-121 D6-1048	AA-123 D6-2757	CAL-124 D6-2756	TWA-131 D6-2758	2EA-138 D6-2763	CUB-139	BrF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	D6-2764	BOAC-LI36	AII-437 D6-2762
1	3112	Bendix Flight Director System -4		X	×	X	X		X	X	X		IX	X		N N
-	3h-13	Bendix Flight Director System -5		X	K		X			X				-		
-	314	Dendix Flight Director System -6		X		X										
	31-15	Rendix Flight Director System -7		X					-							
	34-10	integrated Instrument System Indicators (Sperry)	7.0 ×													
	34-17,	Kollsman KS 86	X									L				
	34-18	Captains' Integrated Instrument System	×						 							
	34-19	Captain's Air Data System (Kollsman)		-											-	
	34-20	Continental Compass Block Diagram		X		X], [+-	
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				-										1		

D6-2764 B0AC-436	AII-137 D6-2762
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ALIT ORDER NUMBER	SECTION 33	PAA-121 D6-1048	AA-123 D6-2757	CAL_121, D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-2764	BOAC-U36	AII-437 D6-2752
33-1	Retractable Landing Light	X				L		L		L				L	
33-2	Exterior Lights Location	A.													
33-3	Emergency Exit Light	X													L
33-4	Fixed Landing and Nunway Turn- Off Lights	X									E	4	L	1_	T
33 - 5	Light Location Diagram - Fain Cabin	X	×							Ч		H	Ч		4
33-6	exit and Energency Exit Light Circuit	X						F			H		L		
33-7	Miscellaneous Internal Lighting	X				Ч						H			H
33-8	Lower Mose Compartment and Wheel Well Light Circuit	X		Ļ	4			L		U	. 4	4	4	F	
33-9	Aft Cargo Compartment Lighting	×	L	L	L		L	H	4	. 4	4	-	H		H
33-10	FWD Cargo Compartment Lighting	×	4	4	H	H		4		H			L		
			-	Н	H	4	H						Ц		

A.T ORUER NUMBER	SECTION 32 (cont.) LANDING GEAR	PAA-121 D6-1046	AA-123 D6-2757	CAL_124 D6-2756	TWA-131 D6-2758	284-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-430 D6-2764	BOAC-436	AII-437 D6-2762
32-45	Main Geer Down Lock Installation	e X													
32-46	IMAIN GEAR DOOR SAFETY VALVE	\boxtimes	\boxtimes		×							L			
	LANDING GEAR POOR WARNING LIGHT CIRCUIT	X	X	X	X	X	X	X						L	
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AAT ORDER NUMBER	SECTION 32 (cent.) LANDING GEAR	PAA-121 D6-101/8	AA-123 D6-2757	CAL_124 D\$-2756	TWA-131 D6-2758	2EA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT_130 D6-2764	BOAC-136	AII-437 D6-2762
32-34	Nose Wheel Steering Mechanism (Animated)				L					L			L	L	H
32=35	Brake Hydraulic System	6. D			X						L		L		
3L -3 6	Brake Metering Valve Schematic	X	×			F							Ц	Į.,	-
32 -37	Brake Cable Control System	X		4										L	7
32-38	Anti-Skid Detector Schematic	X	Ц				-	L		L		Ч	4	L	L
32-39	Anti-Skid System	X						Ц				-		Ч	H
32-40	Main Landing Gear Actuator (Animated)					L	Ч			H		Ч	H	H	F
. 32 - 10	Nose Wheel Steering and Follow- Up Control System (Animated)	4	-	4	4	. 4				H			-	L	4
· 32=42	Steering Hydraulic System Schematic	, X		L	L	L		L	-	L	4	4	4	L	口
32-43	Anti-Skid Circuit (Animated)	Ч	L		Ч	H			H		T		4		
32 - 444	Landing Gear Control Cable System	PAX	4		4	Н	4						4	L	

	T	_		_											
AAT ORDER NUMBER	SECTION 32 Cont. LANDING GEAR	PAA-121 D6-1048	AA-123 D6-2757	CAL-124 D6-2756	TWA-131 D6-2758	QEA_138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AP-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-2764	BOAC-436	AII-437 D6-2762
32-23	Nose Gear Lock	PUA	121 A	121 8	1214	12/ 6	121 A	121 A		L					L
32-24	Nose Wheel Well Door Actuator and Linkage Installation	Pu X	121	121	121	121	121	121		Ч	4			L	
32-25	Landing Gear Control System	Pu B B				Ч		L		-			L		T
32-26	Landing Gear Control Handle Lock Circuit	es X	12/	121	121	121	121	121			H	Ч	L		*
32-27	Landing Gear Position Indica- ting Circuit	Pu A	121 A	121A	121 0	121 A	12/4	12/4	Ч	4	H	Ч	4	Ч	口
32-28	Main Gear Emergency Extension System	× ×	121	12/	121	121	12/	121	4		H	T	H		T
32-29	Nose Gear Emergency Extension System	Pu X	12/	121	121	121	121	121	121	121	,2,	121	121	121	12.1
32-30	Nose Wheel Steering Hydraulic System	PIA	= -		4	4	T	4	H	4	4		4	4	7
32-31	Nose Wheel Steering Control System	Pu X	-	4	4	4	4		4			H	H	+	T
32-32	Steering Metering Valve	X X	121	121 1	121	121	121	121	12/	121	,2/	12/	12/	121	.27
32-33	Nose Wheel Steering Follow-up Details	X N	121	121	12.1	21	2/	12/		4					4
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AUT ORDER NUMBER	SECTION 32 Cont. LANDING GEAR	PAA-121 D6-1048	AA-123 D6-2757	CAL-124 D6-2756	TWA-131 D6-2758	284-138 D6-2763	cuB-139	BNF-227 D6-2759	PAA-321	AR-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-2764	BOAC-L36	AII 437 D6-2762
32-12	Main Gear Truck Snubber	- X											-		
32-13	Main Gear Truck Centering Cylinder	B										. L		_	
32-14	Main Landing Gear Actuator Schematic	A									ļ			_	
32-15	Brake Equalizer Mechanism	c · 🗴					L_			L				L	
32 - 10	Main Landing Gear Door Actua- ting Mechanism	A				,									
32-17	Main Landing Gear Wheel Well Door Mechanism	(* X									L				
32-18	Nose Gear	r D	52°C			ĺΧ						-			
32-19	Nose Gear Structure	, B												L	
32-20	Nose Gear Ground Lock Instal- lation	×													
32-21	Nose Gear Mechanism (Animated)		, .									-			
32-22	Nose Gear Shock Absorbing Strut	×													

ALT CRDER NUMBER	SECTION 32 LANDING GEAR	PAA-121 D6-1048	AA-123 D6-2757	CAL_124 D5-2756	TWA-131 D6-2758	QEA-138 D6-2763	cms-139	BNF-227 D6-2759	PAA-321	AF-328 36-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-2764	BOAC-136	AII-437 D6-2762
32-1	Nose Gear Retracted Schematic	X				_	L	-							
32-2	Nose Gear Extended Schematic	A													
32-3	Nose Gear Operating Sequence	çu A										1.	-		
32-4	Main Landing Gear Retracted Schenatic	×			L										
32-5	Main Landing Sear Extended Schematic	2						-	1						
32-6	Main Landing Gear Operating Sequence	, A				-									
32-7	Landing Gear Mechanisms (Animated)		1. [ļ -									1	
32-8	Main Landing Gear	A	200												
32-9	Main Landing Gear Structures	X													
32-10	Main Landing Gear Location Diagram	A							L.		-				
32-11	Main Landing Gear Lock	A													

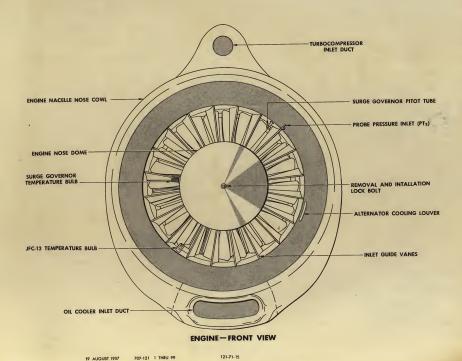
A.r.T. ORDER NUMBER	SECTION 31 Cont. INSTRUMENTS	PAA-121 D6-1048	AA-123 D6-2757	CAL_124, D6-2756	TWA-131 D6-2758	QKA-138 D6-2763	CUB-139	BNP-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-2764	BOAC-136	AII-437 D6-2762
31-12	Attendant's Panel - Forward	X													
31-13	Navigation Station Panel	X											L		H
31-14	Forward Electronic Control Panel	X													4
31-15	Aft Electronic Control Panel	X		-	L					Ч	H				
															T
				L		Ч		4	Ч	Ч	4				口
		Ц	Ч	4		Ч				4		Ч	Ч		T
		4	4	H	4	H		4	中	-4		Ч	4	4	口
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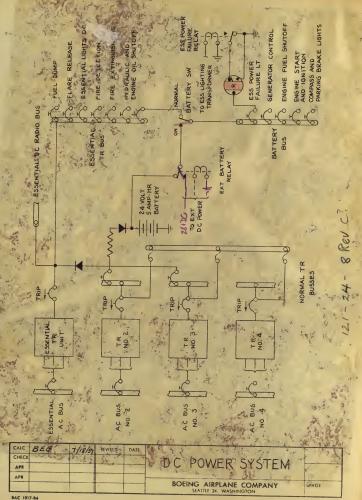
SECTION 31 INSTRUMENTS PROPERTY OF THE PROPER																
31-2 Pilot's and Copilot's Overhead Panel 31-3 Contact Stand 31-4 Flight Engineer's Instrument Panel - Lower Uppec 31-5 Flight Ancineer's Instrument Panel - Upper Lower 31-7 Pilot's Instrument Panel - Left 31-8 Pilot's Instrument Panel - Conter 31-9 Pilot's Instrument Panel - Right	AAT ORDER NUMBER		PAA-121 D6-1048	AA-123 D6-2757	CAL-124 D6-2756	TWA-131 D6-2758	JEA-138 D5-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT_130 D6-2764	BOAÇ-136	AII 4137 D6-2762
Panel 31-3 Consider Stand 31-4 Flight Engineer's Instrument Panel - tower Upp's 31-5 Flight Angineer's Instrument Panel - Uppar Lower 31-6 Pilot's Instrument Panel - Left 31-8 Pilot's Instrument Panel - Center 31-9 Pilot's Instrument Panel - Right A	31-1 200	Acta Tistrument Panel	CANCEL						Ĺ						L	L
31-4 Flight Engineer's Instrument Panel - issuer Uppe 31-5 Flight Angineer's Instrument Panel - Upper Louge 31-6 Cartain's Integrated Instrument System 31-7 Pilot's Instrument Panel - Left 31-8 Pilot's Instrument Panel - Conter 31-9 Pilot's Instrument Panel - Right	31-2		75	X										L	L	
31-5 Flight engineer's Instrument Panel - Lower Uppro 31-5 Flight engineer's Instrument Panel - Uppar Lower 31-0 Cartain's Integrated instrument System 31-7 Pilot's Instrument Panel - Left 31-8 Pilot's Instrument Fanel - Conter 31-9 Pilot's Instrument Panel - Right	31-3	constant stands										-		L	-	L
31-5 Plict's Instrument Panel - Silent received Instrument 31-7 Pilot's Instrument Panel - Left 31-8 Pilot's Instrument Panel - Contern 31-9 Pilot's Instrument Panel - Right	31-4							L		-		L				L
31-7 Pilot's Instrument Panel - Left 31-8 Pilot's Instrument Panel - Conter 31-9 Pilot's Instrument Panel - Right A	31-5		P		L									-		
31-7 Pilot's Instrument Panel - Left 31-8 Pilot's Instrument Panel - Conter 31-9 Pilot's Instrument Panel - Right	31-6	Captain's Integrated Instrument System	X	L												
31-9 Pilot's Instrument Panel - Conter 31-9 Pilot's Instrument Panel - Right	31-7		1													
31-9 Pilot's Instrument Panel - Right	31-8	Pilot's Instrument Panel -									-	-				
31-10g- 100 100 100 100 100 100 100 100 100 10	31-9			X									- [
	31-10	no de la constante de la const		Barv.EL							L					T
31-11 Attendant's Panel- Aft	31-11	Attendant's Panel- Aft											-			

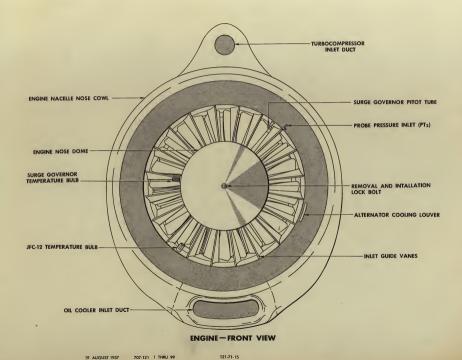
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ART ORDER NUMBER	SECTION 30 . ICE AND MAIN PROTECTION	PAA_121 D6-1048	AA-123 D6-2757	CAL-124 D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BUF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUFT-130 D6-276L	BOAC-136	AII-437 D6-2762
30-1	Tee Elimination	X X	900			. L									
30-2	Empennage Anti-Icing System	A	N /			- [
30=3	Empennage De-Icing System	A	_					L					L		
30 - 4	Wing Anti-Icing System and Equipment Location	B											L	L	
30-5	Wing Anti-Icing Control System	NB	, 🖸				L							L	L
30-6	Ice Detector Control System	CANCEL			L					- 12					
30-7	Ice Detector	X					L								
30-8	Ice Detector Control	X		L		L		L		1	-		L		
30-9	Ice and Rain Protection Equip- ment Location - Control Cabin	X						-	-4	4	4	· L	H		
30-10	Nose Dome and Cowl Anti-Icing System	X											L		-
30-11	Windshield Heat Controller- Schematic Diagram	×								L				-	4
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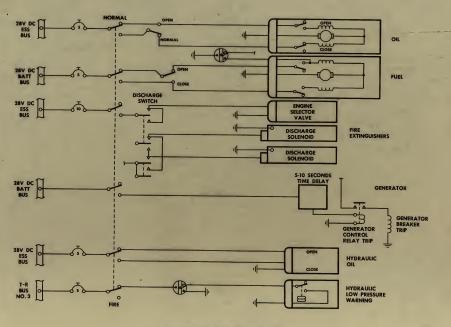
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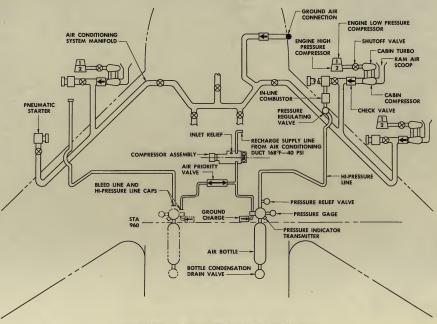






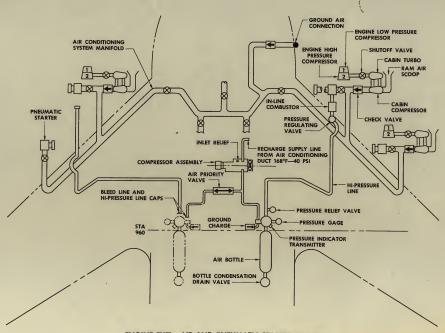


ENGINE FIRE SWITCH SCHEMATIC



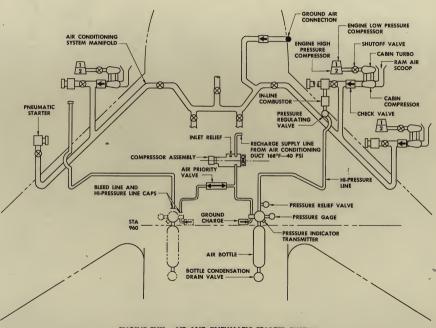
ENGINE FUEL-AIR AND PNEUMATIC STARTER SYSTEM

B

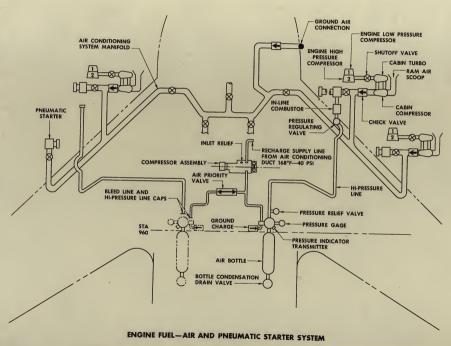


ENGINE FUEL-AIR AND PNEUMATIC STARTER SYSTEM

B



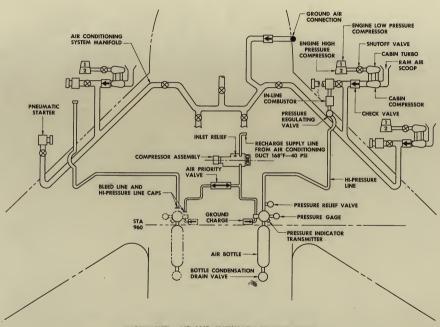
13 SEPTEMBER 1956 707-121 1 THRU 99 121-80-1 B 7913 NEWS

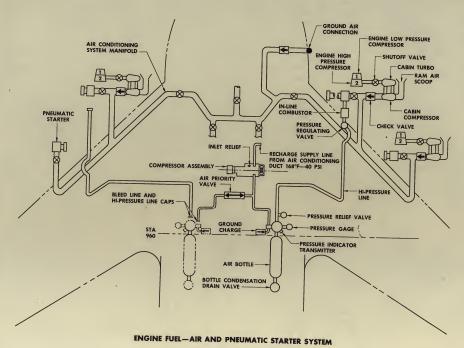


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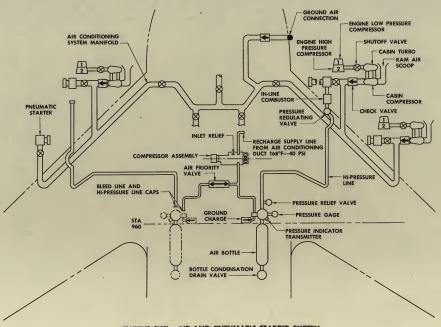


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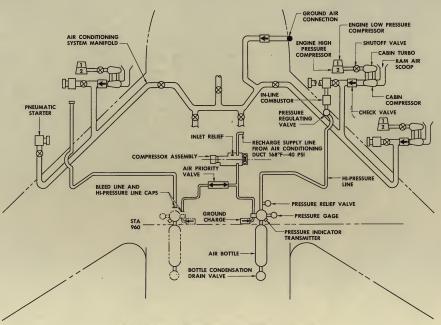
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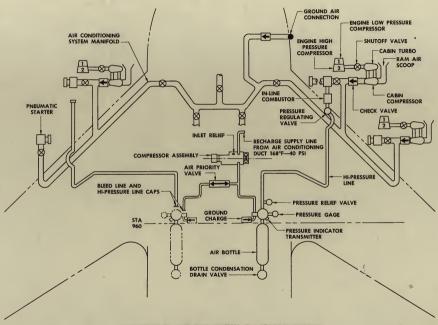
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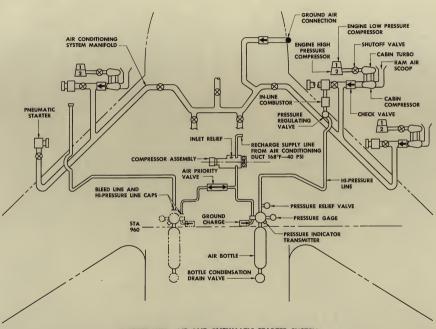
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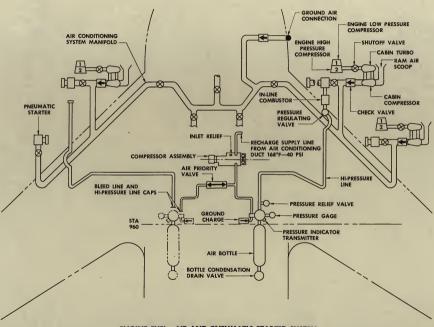


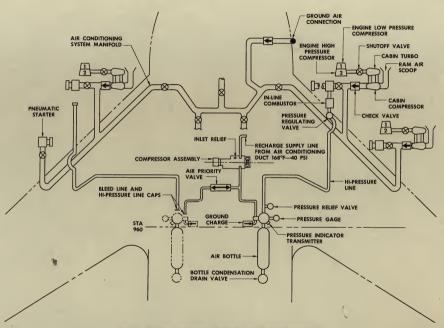
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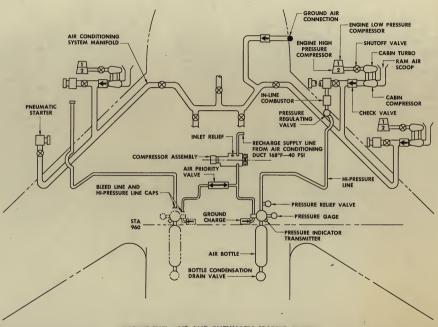


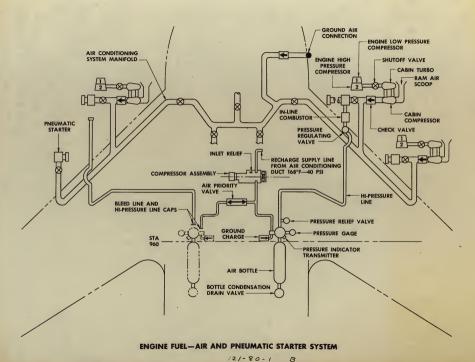






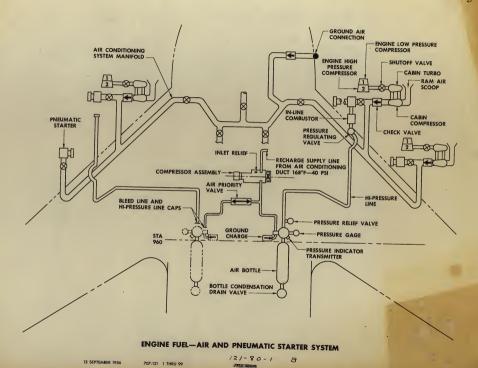


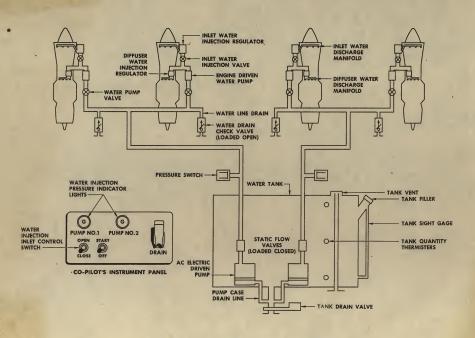




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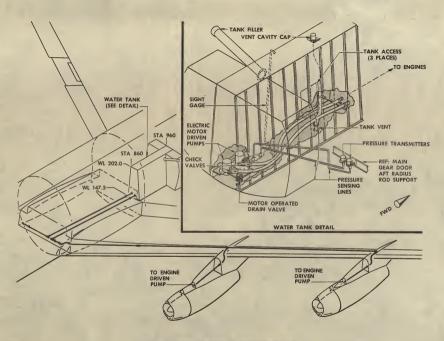


WATER INJECTION CONTROL SYSTEM SCHEMATIC

REV 22 JULY 1957

707-121 1 THRU 99

121-82-2 REV B

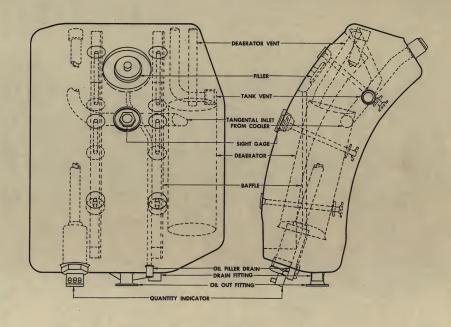


JT3C-6 ENGINE WATER INJECTION SYSTEM

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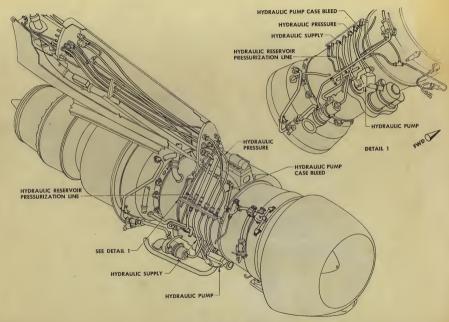
ENGINE OIL TANK

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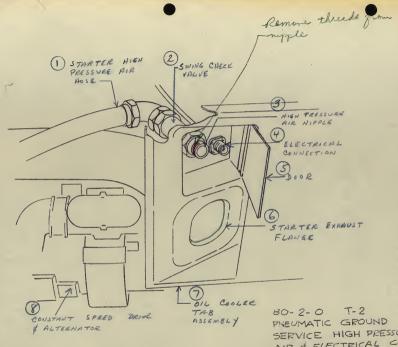
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NACELLE HYDRAULIC INSTALLATION

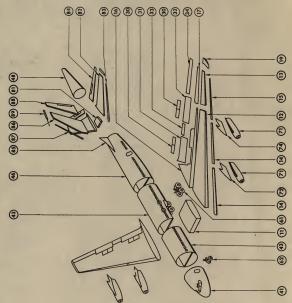
KC-135 55-3121 AND ON JP43 SHT 2 FRAME NO. B



SERVICE HIGH PRESSURE AIR & ELECTRICAL CONN. 1-28-58 G. LEAKE

STRUCTURES Structures - General Description and Operation





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HORIZONTAL STABILIZES HORIZONTAL STABILIZES NBOARD STRUT TORQUE BOX LEADING EDG ELEVATORS -DORSAL FIN

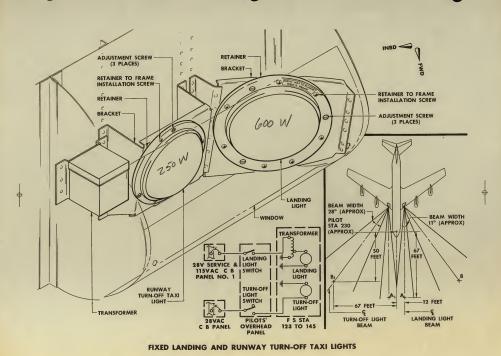
Sectional Breakdown Figure 1 D (1100

321 6.1 REV A

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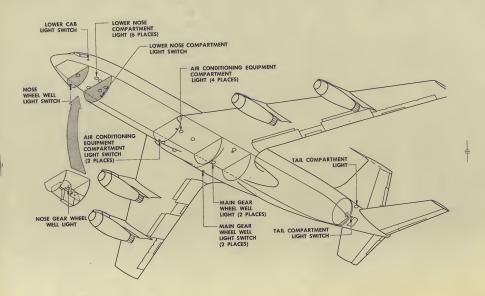


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13 MARCH 1957

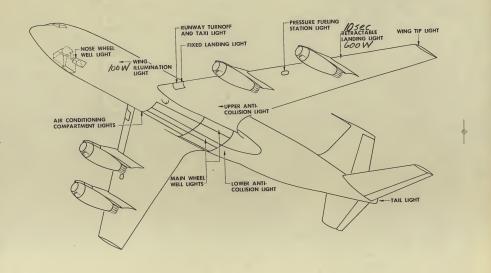
707-121 1 THRU 1999

FRAME NO. B



MISCELLANEOUS INTERNAL LIGHTING 121-33-7

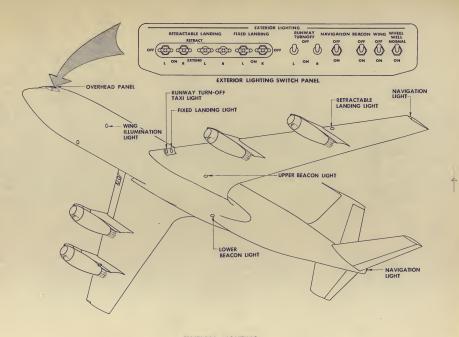
707-121 1 THRU 99



EXTERIOR LIGHTS LOCATION

707-121 1 THRU 99

121-33-2



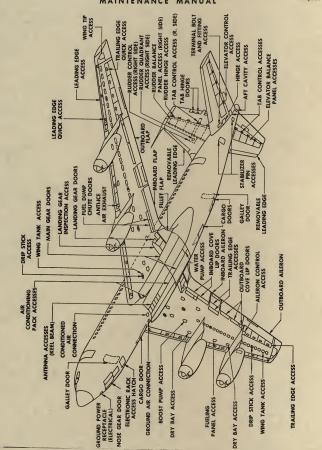
EXTERIOR LIGHTING

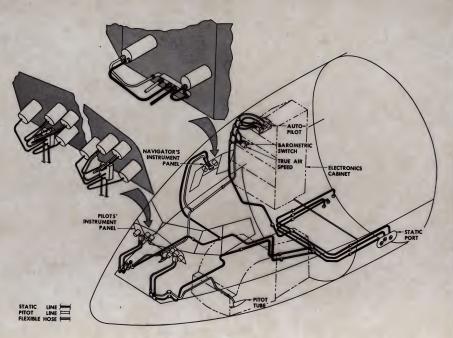
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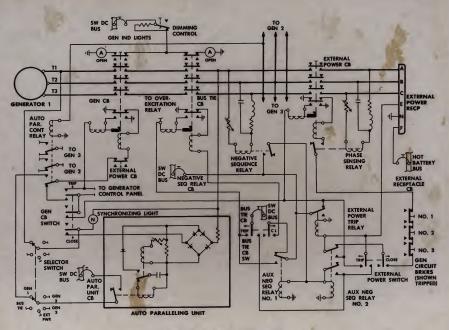
121-33-2 REV A

FRAME NO. B

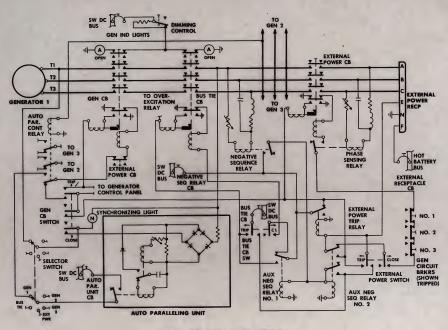




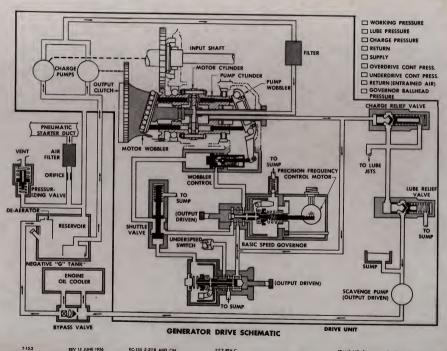
PITOT STATIC SYSTEM LOCATION



GENERATOR PARALLELING CIRCUIT



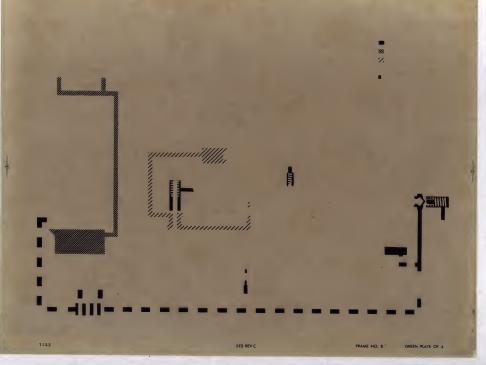
GENERATOR PARALLELING CIRCUIT

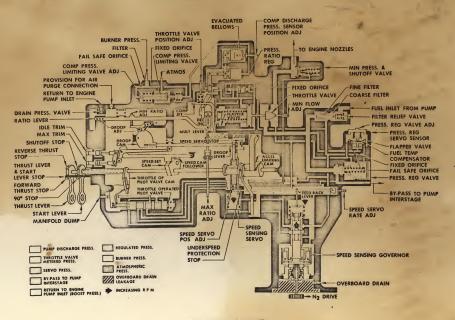


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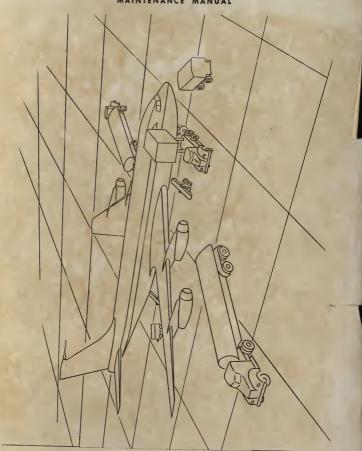


FUEL CONTROL UNIT

JUL 13/39 . 720-15 73-1 FRAME NO. 8 BLACK PLATE OF 2

SERVICING Servicing General Maintenance Practices

MAINTENANCE MANUAL



May 20/57

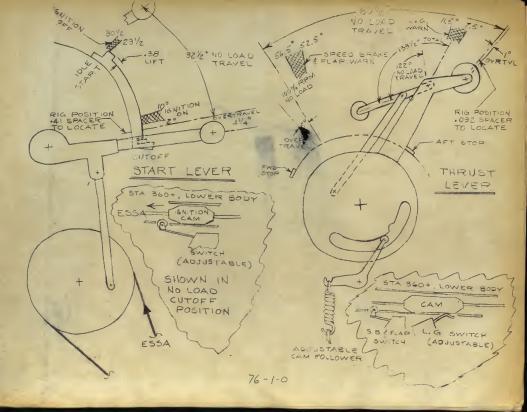
Typical Terminal Service Arrangement Figure 203

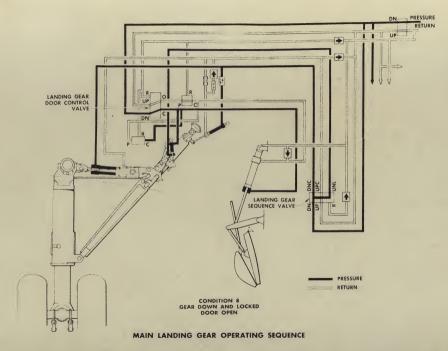
END 12-1-0 Page 205

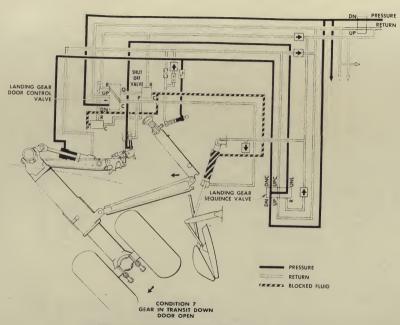
D6-1198

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ART ORDER NUMBER	SECTION 82 .	PAA-121 D6-1048	AA-123 D6-2757	CAL_124 D6-2756	TWA-131 D6-2758	QEA-138 D6-2763	CUB-139	BNF-227 D6-2759	PAA-321	AF-328 D6-2761	SAB-329 D6-2760	TWA-331	LUTT-130 D6-2764	BOAC-436	AII-437 D6-2762
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82-7	Engine Water Injection Flow Distribution	×	4			H	Ч		Ч	Ч	7	L		Ч	口
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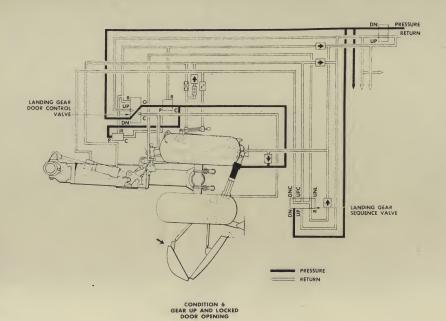
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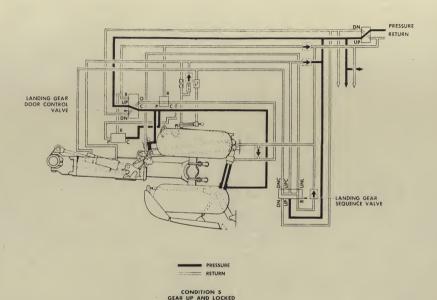


MAIN LANDING GEAR OPERATING SEQUENCE



3331 31 311113

MAIN LANDING GEAR OPERATING SEQUENCE

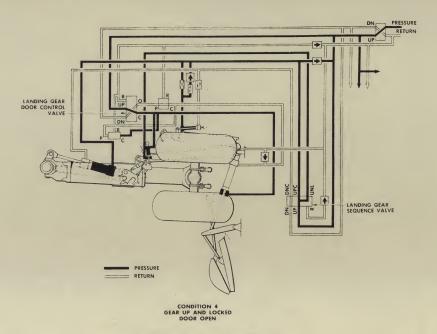


MAIN LANDING GEAR OPERATING SEQUENCE

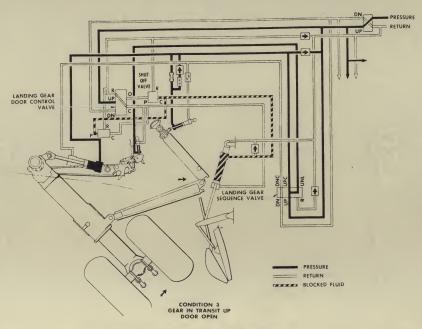
DOOR CLOSED

10 OCTOBER 1956 707-121 1 THRU 99

7G26



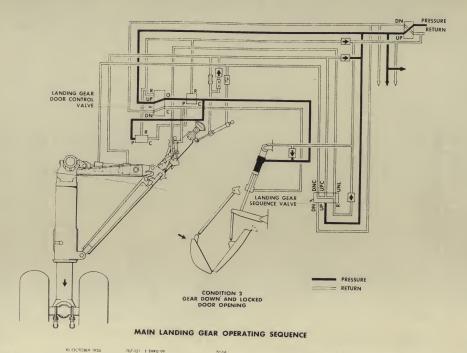
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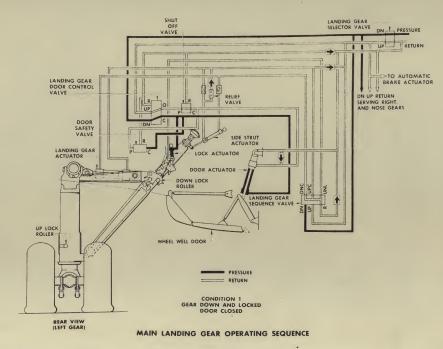


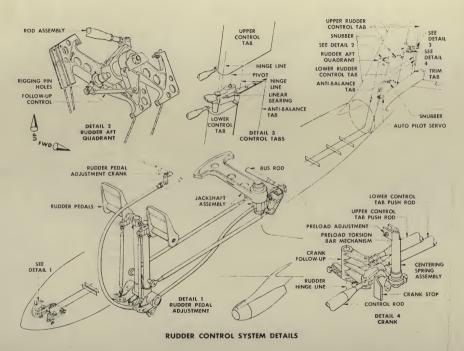
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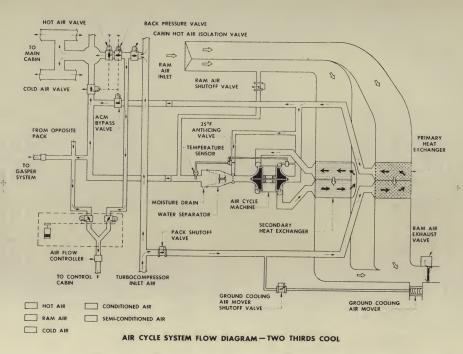
10 OCTOBER 1956 707-121 1 THRU 99

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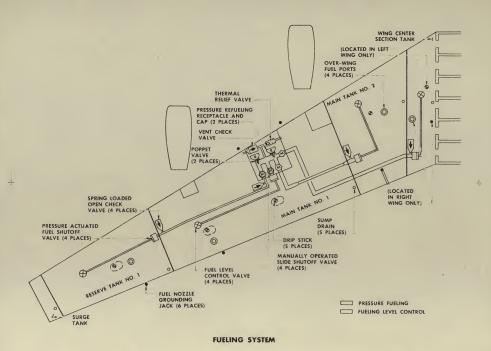


19 OCTOBER 1956 707-121 1 THRU 99

7X14

FRAME NO. B

BLACK PLATE OF 4



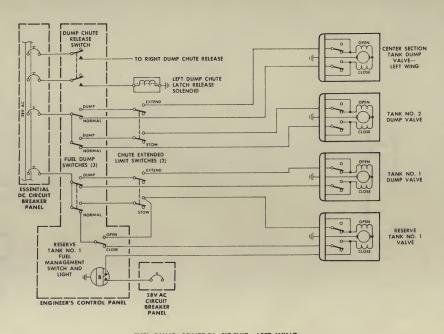
7F3 REV A

FRAME NO 8

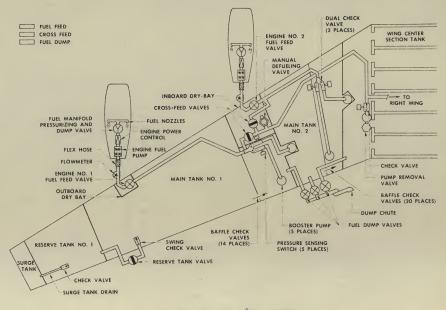
BLACK PLATE OF 2

REV 17 SEPTEMBER 1956

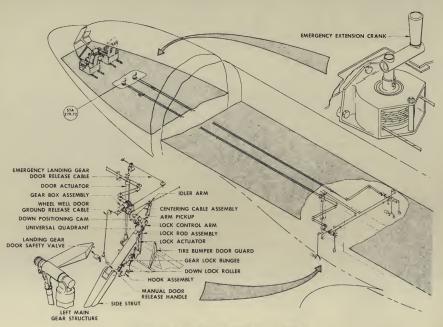
707-121 1 THRU 99



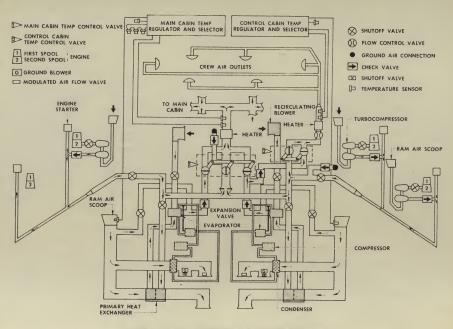
FUEL DUMP CONTROL CIRCUIT-LEFT WING 7F7



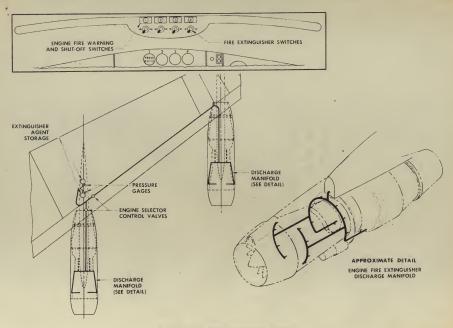
FUEL FEED AND FUEL DUMP SYSTEMS



MAIN GEAR EMERGENCY EXTENSION SYSTEM



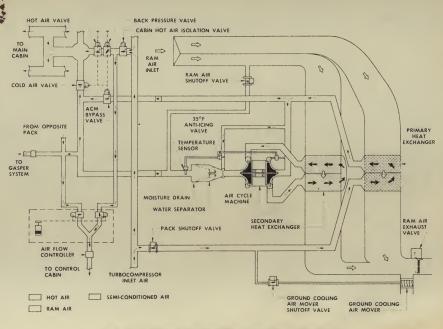
VAPOR CYCLE AIR CONDITIONING SYSTEM SCHEMATIC



ENGINE FIRE EXTINGUISHING SYSTEM

REV 3 OCTOBER 1956 707-121 1 THRU 99

7P6 REV 8



AIR CYCLE SYSTEM FLOW DIAGRAM-FULL HEAT CONDITION

19 OCTOBÉR 1956 707 121 1 FHRU 99 7X11 FRAMÉ NO. 8 BLACK PLATE OF 3

707

Main Geat OPERATING SEQUENCE

9 FRAMES



INSTRUCTION BOOK



KENT, WASH.

Technical Specifications of the ELECTRONIC TOUCH KEYER Model Mark V

Code Speed
 to 55 words per minute

2. Dot-Dash Ratio 1:3

3. Automatic Space Ratio 1 (element) : 3 (letter) : 7 (word)

4. Aural Output Speaker with level control

5. Output Method Dry Reed Relay contacts

6. Mode Control 'AUTO' for automatic spacing of character elements, characters, and words.

'SPACING OFF' for manual control of spacing of elements of each character.

'TUNE' for adjusting associated RF Transmitter.

Warning light when in manual spacing mode.

7. Integrated Circuits 17

8. Light Emitting Diodes 2 ea. LED's 1 ea. BiLED

9. Internal Operating Power 5 Vdc, Regulated

10. Power Requirements 120 V, 60 Hz, 7 W

11. Net Weight 4.5 pounds

OPERATING YOUR NEW ELECTRONIC TOUCH KEYER Model Mark V

INITIAL TEST:

- On-Off Volume control fully counterclockwise.
- Mode control switch to 'AUTO'.
- 3. 'SPEED' control fully counterclockwise.
- 4. External paddle type key in key jack. Plug line cord into 120 volt AC outlet.
- 6. Turn 'On-Off' control half turn clockwise.
 - a. Green 'SPACE' BiLED will light.
 - b. If either 'DOT' or 'DASH' light is on, touch key paddle to either 'DOT' or 'DASH' position and the light will turn off.
- 7. Close Dot contact on paddle key.
 - a. Keyer will make continuous dots which can be heard in the speaker. Adjust volume for comfortable level.

 - b. 'DOT' LED will light with each dot.
 c. 'SPACE' BiLFD will two many and the second s 'SPACE' BiLED will turn red during the space between the dots.
 - d. Release key. 'SPACE' BiLED will turn red following last dot, for lengthy period indicating word space, then return to green.
- Close dash contact on the paddle key and check action of 'DASH' LED and 'SPACE' BiLED.
- 9. Turn mode switch to 'SPACING OFF'.
 - a. 'SPACE' BiLED will turn red.
 - b. Apply Dot and Dash inputs, check operation of LEDs.
 - c. Note that 'SPACE' BiLED stays red continuously to warn that automatic spacing is not functioning.
- 10. Turn mode switch to 'TUNE'.
 - a. Continuous tone will be heard in the speaker.
 - b. 'DASH' LED will be on.
 - 'SPACE' BiLED will be green.
- d. Using an ohmmeter, check for 220 ohms resistance between the relay output terminals on the terminal board on the rear of the keyer.
- 11. Turn mode switch to 'AUTO'.
 - a. No tone can be heard from the speaker.
 - b. 'DASH' and 'DOT' LED's will be off.
 - c. 'SPACE' BiLED will be green.
- d. The ohmmeter should show infinity between the relay output terminals.
- 12. End of initial tests.

LEARNING TO USE YOUR ELECTRONIC TOUCH KEYER

Using your Electronic Touch Keyer (ETK) is very different from sending code with a 'Bug' or most other keyers. The ETK performs all the functions necessary to send perfect code with just a few directions from the user. Just a touch of the dot or dash key is all that is required for the ETK to transmit a perfect dot or dash and block the output for the duration of the word space.

Just touch the dot key and then the dash key as rapidly as possible and the ETK output will be a perfect dot, a space equal to the dot length, a perfect dash three times as long as the dot and a word space seven times the dot length.

Practice this simple operation, watching the LED indicators, particularly the space BiLED until you are familiar with this operation.

Next, rapidly touch the dot key, the dash key and the dot key again. Complete this sequence before the dash starts. The ETK will send a perfect 'R', most of it while your hand is off the key. Then instruct the ETK to send a 'K' by rapidly touching the dash key, the dot key, and then the dash key again.

Repeat these steps until you have assured yourself that just a touch of the dot or dash key is all the instruction your ETK requires to send a perfect code element. You do not need to hold either key closed to insure that your instruction to the ETK will be followed.

Next, you should learn to use the letter space. The ETK is programmed to block the output from sending a dot or dash for a period equal to seven dots following the completion of the last dot or dash entered by the key. However, it is also programmed to change this instruction and modify the word space to a period equal to three dots (a letter space) if the next dot or dash beginning the succeeding letter is entered at a certain time with respect to the previous element. This time is not <u>critical</u>. Just touch the dot or dash key at a time at least a dot period after the last element of a letter is completed but before a period equal to a dash has elapsed. This instruction just has to be given to the ETK (by touching a key) during the last 66% of the letter space time. If the key is touched too early (within one dot period) the ETK will send the element after a one dot space (normal separation between elements). If the key is touched too late (after a three dot period) the ETK will send the element after a word space. Practice instructing the ETK to provide letter spacing between dots or dashes.

Using the automatic word spacing properly requires that the first dot or dash of the next word be entered before the word space period has expired. The ETK is programmed to accept a dot or dash instruction after a letter space period has passed, between the 4th and 7th dot period of the word space, complete the word

spacing and then send the stored dot or dash. You may even enter one dot and one dash instruction during this time and the ETK will send them in the same order they were entered following the word space.

A certain amount of practice at low keying speeds is necessary so the operation of the ETK is understood thoroughly before sending at normal keying speeds. Habits developed using a 'Bug' or other code mechanisms may have to be modified to take advantage of the capabilities of the ETK. Once the user is familiar with the ETK, he will be delighted with the machinelike code from his ETK.

THEORY OF OPERATION

CLOCK CIRCUITS

The clock circuit in this keyer is very different from the usual clock or oscillator found in other keyers. It is designed to avoid several faults common to other keyers which derogate their performance. This circuit forces the keyer output to start instantly upon application of an input signal. It has a wide frequency range, allowing a keying rate of 5 to 60 wpm without switching ranges. The clock circuits are designed to minimize the long first cycle oscillation period characteristic of RC oscillators which cause the first dot or dash in other keyers to be nearly 50% longer than succeeding elements. The first dot from this keyer is within 5% of the correct length, a slight amount which cannot be detected by ear.

The clock circuit begins with a pulse generator operating at 10 times the keying speed, or generates 10 pulses in order to form a dot or a space between elements and 30 pulses to form a dash. The output of the pulse generator is counted down by a divide by 10 counter to obtain the correct time period for these elements.

The pulse generator, counter, inverter, gate, and flip-flop act to begin the output signal instantly when an input signal is applied, and reduce the effect of the long first cycle of the clock. When the keyer is not operated, the flip-flop resets the counter to a nine count. The pulse generator is stopped by a signal on its reset input, which holds the output in a low condition. The inverter transforms this to a high at the input to the counter. When a dot or dash input signal is applied, the reset signal is removed, the pulse generator output goes high, the counter input goes low, causing the counter to advance to zero and the output of the counter sets the dot flip-flop, forcing the keyer output to transmit the start of the output signal. At the 10th pulse from the pulse generator, the counter output resets the dot flip-flop, ending a dot period. The effect of any long first cycle period in the pulse counter is reduced by a factor of 10 by the counter, thereby insuring that the first dot or dash are nearly of the correct length.

The gate in the clock circuit removes the reset 9 signal as soon as the counter is set at nine. If this were not done until the pulse generator reset signal was removed, the counter would not respond to the first high output from the pulse generator as transmit time in the internal reset circuits of the counter is longer than the transit time in the pulse generator and inverter. This would cause a 1/10 dot period delay in the output of the keyer for all signals.

SPACING CIRCUITS

There are four flip-flops and a space decoder in the spacing circuits. One FF acts as a gate to turn on and off the pulse generator or clock. The other three FF's provide the letter and word spacing and control the main enabling signal to allow dots and dashes at the correct times. The enabling signal forces the keyer to send as though it were driven by a synchronous clock.

The space gate is reset when a dot or dash input signal is entered and turns on the clock circuits. The space gate FF can only be set by a signal from the 7 space FF when there are no dot or dash signals stored in the memory circuits. The space gate forces the clock to run until all the memories are cleared and 70 additional pulses are generated.

The 1, 3, and 7 space FF's and the space decoder control the main enabling signal so dots and dashes are sent at the correct times. If the memories do not contain signals to be sent, the spacing system blocks the keyer output for a time period equal to a letter space (3 dots). If a dot or dash is entered during the last 66% of the letter space, it will be sent after the letter space is completed. If an input signal is entered after the letter space is completed, the spacing system will block the keyer output until a total time period equal to a word space (7 dots) has elapsed since the previous dot or dash was completed. The keyer is then allowed to send the signal contained in the memory. If no signal is contained in the memory, the 7 space FF will set the space gate, shutting off the pulse generator. Once the first dot or dash is entered the spacing circuit controls the timing of the keyer so all subsequent elements of a message are referenced to the start time of the first signal and occur synchronized to this time. In effect, the asynchronous clock is made to operate in a synchronous mode until the message is completed if the user enters the information at a slightly faster rate than the kever speed.

The automatic letter and word spacing function may be switched off, and the spacing controlled by the operator. However, the spacing system will continue to control the clock circuits and force the pulse generator to furnish 70 pulses after any element. If the operator does not exceed the normal word space time between elements all dots and dashes will be synchronized with the first element sent although the letter and word spacing may not be correct if the operator's sending is inaccurate.

DOT-DASH MEMORY AND PROCESSING CIRCUITS

The dot-dash memory and processing circuits perform many functions. They accept the input signals from the external key mechanism and eliminate the contact bounce associated with mechanical switches. It resets the space gate, turning the pulse generator on. It generates the main (dot) and secondary (dash) enabling signals. It remembers which of the two input signals were entered first and forces the keyer to transmit the corresponding dot or dash first. While directing the keyer to transmit one signal, it will accept and hold the other input signal until it can be sent in the correct time frame. It removes the input signal from the memory after the corresponding element has been sent. It will allow multiple dots or dashes to

be transmitted by holding the external key closed while accepting and holding an input signal of the opposite element for transmission after the sequence is completed.

These functions are accomplished by six FF's and 8 gates arranged in two interconnected channels. The dot-dash gate detects an input signal, generates the main enabling signal and resets the space gate. A memory FF accepts the input signal, eliminating the contact bounce, and sends it to the acceptance FF when the lockout gate is not disabled by the other channel. The acceptance FF seeks to set the reset FF through the response gate and disables the lockout gate in the other channel. This gate will allow the passage of the trigger to the reset FF when the dot or dash FF associated with it is set. The reset FF arms the reset gate. The reset gate sends a reset pulse to the memory FF and resets it at the end of the transmitted dot or dash. The memory FF resets the acceptance FF which in turn arms the lockout gate in the other channel.

DOT-DASH GENERATOR

The dot-dash generator forms the dot and dash signals sent to the indicator and output circuits of the keyer. It also provides the correct spacing between elements. The generator consists of two Ff's. The first FF forms the dot signal. A dash is formed by causing the first FF to set the second FF when the dot signal is completed. Then the dot FF is set again and both FF's are reset to end the dash. Operation of these FF's is triggered by the clock.

The main enabling signal controlled by the spacing circuits is applied to the dot FF so it can respond to the clock signal from the counter. A secondary enabling signal, controlled by the dash acceptance FF in the dash memory and processing circuits is sent to the dash FF when a dash signal is to be formed.

The outputs of the dot and dash FF's are combined in a gate. The output of this gate controls the keyer output relay.

INDICATOR CIRCUITS

The keyer has a sidetone oscillator and speaker to monitor the dot-dash output. There are three LED indicators which indicate the processes occurring in the internal circuits. These LED's are labeled 'SPACE', 'DOT', and 'DASH'.

The 'DOT' LED is red and lights during the time a dot is being transmitted by the keyer.

The 'DASH' LED is red and lights during the time a dash is being transmitted by the keyer. It also lights when the mode switch is in the 'TUNE' position, indicating that the output relay contacts are closed and the keyer is transmitting a long dash.

The 'SPACE' BiLED is a dual color LED, green and red. One of the two colors is always lighted when the keyer is on. When the color is green, it indicates that

an input signal will be accepted and sent instantly or that a dot or dash is being transmitted. When the BiLED changes from green to red, it indicates a space between elements, a letter space or a word space is occurring and any input signal entered will be accepted but held until the space period is completed.

While the 'DOT' and 'DASH' LED's continue to indicate when these elements are being transmitted with the mode switch in the 'SPACING OFF' position, the 'SPACE' BILED will be red as a reminder that the user is responsible for the proper letter and word spacing.

YOUR ELECTRONIC TOUCH KEYER WARRANTY Model Mark V

The Electronic Touch Keyer is a state of the art device and is the product of the latest and most up-to-date engineering and production experience. It will give you years of satisfactory service if operated in accordance with the simple instructions furnished.

During the first six months of ownership by original purchaser, if any repairs should be necessary through no fault of yours, the factory will repair free of charge and will also pay return shipping charges.

CUSTOMER SERVICE

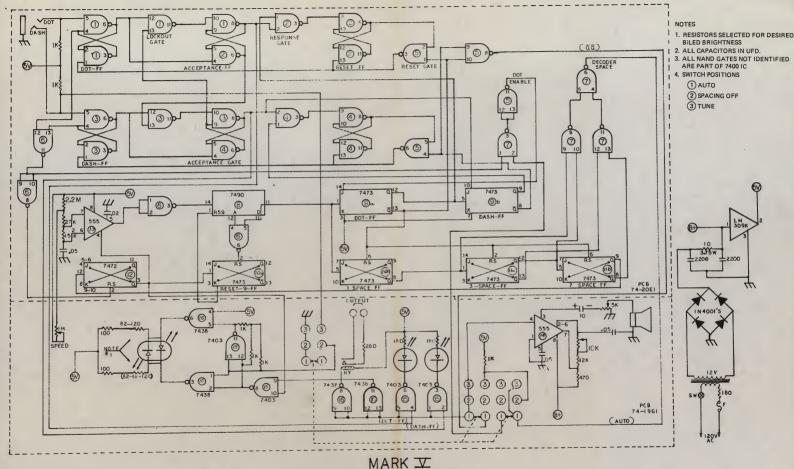
If during your first six months of ownership you require service, write to the factory and include:

Your name and address The serial number of your Electronic Touch Keyer A description of the problem or difficulty

After receipt of your letter, the factory will ship the necessary part or authorize shipping the keyer back to the factory for repair.

After six months, if factory repairs are necessary, our service department will repair the keyer for a \$10.00 service charge plus parts and return shipping costs.

CRS Company P.O. Box 1125 Kent, Washington 98031



MARK IN ELECTRONIC KEYER